

Myren Consulting, Inc.

United States
Environmental Protection Agency
Woodheater Certification Program
Woodheater Certification Test Report

Kuma Stove and Iron Works
Kuma Scott HT-1
Noncatalytic Woodstove

September 15, 1996

Myren Consulting, Inc.

Office:

512 Williams Lake Road

Colville, WA 99114

509-684-1154

509-685-2262 Fax

Laboratory:

Suite 106

12810 NE 178 th St.

Woodinville, WA 98072

206-483-7997

206-485-1677 Fax

* * * * *

CONFIDENTIAL

* * * * *

The data and information in this test report is confidential, proprietary information and is not to be released to and/or discussed with any party who is not authorized by the manufacturer or the testing laboratory to receive such data.

* * * * *

CONFIDENTIAL

* * * * *

TABLE OF CONTENTS

	<u>Section(s)</u>	<u>Page(s)</u>
Introduction		
Title Page	Introduction	i
Confidentiality Statement		ii
Table of Contents		iii
Field Observation Checklist		v
Report Certification		vi
Test Report (Data) Page Number Index		vii
Individual Test Run Page Number Index		x
Statement of Confidentiality		xi
Test Series Information and Discussion		xii
Summary and Discussion of Results		
Weighted Average Calc Sheets	Data Summary	1-3
Cap Graph		4
Data Summary		5-7
Stove/Cat Aging Data	Aging	vari
Individual Test Runs (Raw Data)		
See Introduction, Individual Test Run	<0.8 kg/Hr	vari
Page Index for a complete, sequential list	0.8-1.25 kg/Hr	vari
of the data and data sequence in the	1.26-1.90 kg/Hr	vari
individual test runs	>1.90 kg/Hr	vari
Calibration Data	Cal Data	vari
See Test Report (Data) Page Number Index,		
Item 14, for a complete, sequential listing		
of the data in this section.		
Stove QC		
Wood Heater Description/Stove QC	Stove QC	1-2
Useable Firebox Volume Dimensions and Calculations		3
Primary Air Inlet Dimensions and Settings		5
Secondary Air Inlet Dimensions and Settings		5
Blueprints		
Promotional (Sales) Brochure	Blueprints	vari
Laboratory verified blueprints		vari
Manual		
Manufacturer's Written Test Instructions	Manual	1-2
Manufacturer's Operators Manual		vari
Storage		
Storage Location	Storage	1
Sealing Information		1

FIELD OBSERVATION CHECKLIST

Unit Name: kuma Scott HT-1 Date: 9/15/96

Manufacturer Name: KUMA Store and Iron Works

Manufacturer Address: 450 Old Highway 95
Rathdrum, Id 83858

Manufacturer Phone: (208) 762-8002

Observers & Affiliation: _____

Myren Consulting's Field Team:
Supervisor: BEN Myren

Other Members: RON Schenck

Test Location: Suite 106 12810 NE 178TH St., Woodinville, WA 98072

Phone (206) 483-7997, Fax: (206)485-1677

Test Site Elevation: 30 feet

Lab
Suite 106
12810 NE 178th St.
Woodinville, WA 98072
(206) 483-7997
(206) 485-1677 Fax

Office
512 Williams Lake Road,
Colville, WA 99114
(509) 684-1154
(509) 685-2262 Fax

Photos

This section contains two photographs of the fuel load for each test run and two color photographs (side and front view) of the wood heater tested and any other photographs pertinent to testing the unit.

Photos

vari

Appendicies:

A - Example Calculations

B - Installation Description and Operating Instructions

REPORT CERTIFICATION

The sampling and analysis for the woodstove described in this report was carried out under my direction and supervision.

Date 9/15/96 Signature Albert V. Myer Jr.

Date _____ Signature _____

I have reviewed all of the testing data and results found in this test report and hereby certify that the test report is authentic and accurate.

Date 9/15/96 Signature Albert V. Myer Jr.

PAGE NUMBER INDEX

	<u>Section</u>	<u>Location</u>
1. Summary Table of Burn Rate and Emission Rate Results	Data Summary	Weight Avg Calc Sheet, pp.1-4
2. Summary Table of Other Data	Data Summary	Data Summary Sheets, pp 5-7
3. Wood Heater Description	Stove QC	Wood Heater Description, p.1 (vari)
4. Manufacturer's Testing Instructions	Operators Manual	P.1 of Section
5. Test Chamber Installation Description	Installation Description	P. 1
6. Wood Heater/Catalyst Aging Documentation	Stove/Cat Aging	
7. Wood Heater Dimensions and Useable Firebox Volume	Stove QC	
8. Pretest Burn Procedures	Individual Test Runs	Data Sheets #9,9A,9A-1,9A-2,13
9. Pretest Facility Measurements	Individual Test Runs	Data Sheets #8,16
10. Test Fuel Measurements		
A. Load Wt.	Individual Test Runs	Data Sheet #8
B. Load Moisture	Individual Test Runs	Data Sheet #10
C. Wood Density	Individual Test Runs	Data Sheet #11
11. Test Fuel Crib Description	Photographs	
A. Photographs	Individual Test Run	Data Sheet #9A,9A-1, or 9A-2
B. Wood Type and Line Drawing	Individual Test Run	Data Sheets #9,9A,9A-1,9A-2,13
12. Test Run Heater Operation and Air Supply Settings		
13. Calibrations		
A. Platform Scale		
1. Initial	Cal Data P. 1	
2. Semi Annual	Cal Data P. 2	
3. Pre and Post Test	Individual Test Run	Data Sheet #16

B. Analytical Balance			
1. Initial	Cal Data	P. 3	
2. Semi Annual	Cal Data	P. 4	
3. Pre Weighing Check	Individual Test Run	Data Sheet #4	
C. Temperature			
1. Thermocouples	Cal Data	P. 5	
2. Thermocouple Readout			
a. Semi annual	Cal Data	P. 6	
b. Daily Check	Individual Test Run	Data Sheet #16	
3. Dry Gas Meter	Cal Data	P. 7	
D. Anemometer	Cal Data	P. 11	
E. Barometer	Cal Data	P. 12	
F. Draft Gauge	Cal Data	P. 13	
G. Humidity Gauge Calibration (Sling Psychrometer)			
H. Dry Gas Meter			
1. Initial	Cal Data	P. 14	
2. Semi Annual	Cal Data	P. 15	
3. Post Certification Test	Cal Data	P. 16	
4. Transfer Standard Calibration	Cal Data	P. 17	
5. Wet Test Meter Calibration	Cal Data	P. 18	
J. Combustion Gas (CO ₂ , O ₂ , CO) Train Response Check	Cal Data	P. 20	
L. CO Analyzer			
1. Calibration	Cal Data	P. 22	
2. Zero/Span Control Chart	Cal Data	P. 23	
3. Pre and Post Test Zero/Span	Individual Test Run	Data Sheet #15-3	
M. CO ₂ Analyzer			
1. Calibration	Cal Data	P. 24	
2. Zero/Span Control Chart	Cal Data	P. 25	
3. Pre and Post Test Zero/Span	Individual Test Run	Data Sheet #15-1	
N. O ₂ Analyzer (Optional)			
1. Calibration	Cal Data	P. 26	
2. Zero/Span Control Chart	Cal Data	P. 27	
3. Pre and Post Test Zero/Span	Individual Test Run	Data Sheet #15-2	
P. Calibration Gas Certificates of Analysis			
1. The Pre and Post Test Zero/Span Audits	Individual Test Runs	Data Sheets #15-1, 15-2, 15-3, 15-4	

2. Method 3 Verification of Analysis (CO₂, O₂, CO, N₂) Cal Data
14. Quality Checks
- A. Leak Checks
 - 1. Particulate Sampling Train Individual Test Runs
 - 2. Combustion Gas (CO₂, O₂, CO) (CEM) Train Individual Test Runs
 - B. Proportional Checks Individual Test Runs
15. Sample Calculations
- A. Weighed Average Emission Rate Data Summary
 - B. Dry Burn Rate Individual Test Runs
16. Raw Test Data Individual Test Runs
17. Analytical Data
- A. Filter and Beaker Tares Data Sheets #4-1, 4-2
 - B. Solvent Blanks Data Sheet #4-3, 5-3
 - C. Particulate Catches
 - 1. Gross Data Sheets #5-1, 5-2
 - 2. Blanks Data Sheets #5-3
 - 3. Net Data Sheet #6
 - D. Constant Weight Weighings Data Sheet #4-3
- P. 1 of Data Sheet #2
Data Sheet #16
Table 1
Computer Printout
- Weighted Average Calc
Sheets, pp. 1-3
Data Sheet #8
Computer Printout
- Data Sheets 1 - 16

M5G-1 INDIVIDUAL TEST RUN PAGE INDEX
The Data Sheets in the Individual Test Runs
Are Organized in the Following Sequence

A. Computer Printouts		
Table 1	Field Data - Sampling Interval Data	
Table 1	Field Data	
Table 1	Field Data Averages	
Table 1	Calculations	
Table 1	Proportional Rate Variation	
B. Raw Data Sheets		
Data Sheet #2	Meterbox Data Sheets	No. of Pages variable
Data Sheet #4	Scale Sheets	
#4-1	Initial Filter Weights	variable
#4-2	Initial Beaker Weights	variable
#4-3	Constant Weights	variable
#4-4	Scale QA Checks	variable
Data Sheet #5	Particulate Catch Processing Sheet	
#5-1	Front and Back Half Catch	1
#5-3	Blank Catch	1
Data Sheet #6	Net Particulate Catch Calc Sheet	1
Data Sheet #8	Miscellaneous Test Data	1
Data Sheet #9	Stove Operating Data	1
Data Sheet #9A	1-4 Stove Operating Data	variable
Data Sheet #10	Fuel Moisture	1
Data Sheet #11	Wood Density	1
Data Sheet #12	Burn Rate and Flue Gas Data	variable
Data Sheet #13	Pre Burn Data	variable
Data Sheet #14	Temperature Data	variable
Data Sheet #15	Pre and Post Test Zero/Span Audits	
#15-1	CO ₂	1
#15-2	O ₂	1
#15-3	CO	1
Data Sheet #16	Quality Checks	1

STATEMENT OF CONFIDENTIALITY

As a condition of being allowed to visit the woodstove testing facility and/or observe a woodstove test(s) at Myren Consulting, Inc.'s testing laboratory located at Suite 106, 12810 NE 178th St., Woodinville, WA 98072, I hereby agree not to release or divulge any information about the design engineering principals used at Myren Consulting, the testing facility, the testing personnel or the testing procedures (other than the information found in the Standard Method for Measuring the Emissions and Efficiencies of Residential Woodstoves promulgated by the Oregon Department of Environmental Quality (DEQ) and/or Methods 28, 28A, 5G and 5H promulgated by the United States Environmental Protection Agency (EPA) to any other individual or firm unless specifically authorized to do so by an authorized person from Myren Consulting.

SIGNED: _____
Name

SIGNED: _____
Name

Title

Title

Affiliation

Affiliation

Date

Date

TEST SERIES INFORMATION AND DISCUSSION

Unit: Kuma Scott HT-1
Model #: Scott HT-1
Manufacturer: Kuma Stove and Iron Works
Date Received: 7/5/96 Date(s) Aged: 8/2, 14 & 15/96
Test Dates: 8/28, 29, 9/5, 6 and 9/96
Sampling Methods Used: M28, M5G-1 Number of Test Runs: 5

The Kuma Scott HT-1 Noncatalytic Woodstove
manufactured by Kuma Stove and Iron Works
of Rathdrum, Id was tested
by Myren Consulting, Inc. using the United States Environmental
Protection Agency's (EPA) Method 28, "Certification and Auditing of
Wood Heaters", Method 5G-1, "Determination of Particulate Emissions
from Wood Heaters from a Dilution Tunnel Location." And, if
applicable, Method 28A, "Measurement of Air to Fuel Ratio and Minimum
Achievable Burn Rates for Wood Fired Appliances". (See the Federal
Register/ Vol. 53, No. 38/ Friday, February 26, 1988/ pp.5860-5926.)
The Particulate Matter (PM) emission data, if present, was calculated
as specified in the Wood Heater New Source Performance Standard (NSPS).

If computed and reported, Oregon Overall Efficiency (%OE) for
each run was calculated using the computer program supplied by the
State of Oregon's Department of Environmental Quality (DEQ) as part of
the "Standard Method for Measuring the Emissions and Efficiency of
Residential Woodstoves". The weighted average overall efficiency was
calculated using the overall efficiency data for each run and the EPA
Burn Rate Probabilities for calculating weighted averages.

All events pertinent to the test data and test results are
recorded on the data sheets in the individual test runs, particularly
on pp. 9, 9A, 9A-1, 9A-2 and 12.

Any deviations made or noted from the promulgated methods other
than those which were accepted and certified by the EPA and/or the DEQ
during the laboratory accreditation process are listed and discussed
below.

The following pages contain (1) a diagram showing the height and
location of the stack components and sampling ports (2) copies of the
certification test notifications and cancellations sent to EPA and
(3) a discussion of test results.

↑

A brief note about the particulate samples is necessary to help understand the net catch values. During initial lab shakedown testing it was discovered that the portion of the filters left on the frits in the M5G-1 filter housing apparatus were full of static electricity and when removed to a plastic petri dish quickly adhered to the dish. Trying to recapture this material during weighing caused it to disintegrate making accurate weights difficult. Thus, it was decided to place this material in with the material captured with the acetone wash, where it shows up as catch. Some of the filter material was already following this flow anyway.

Thus, there may be negative filter weight catches that are used during the particulate emission rate calculation process. This accounts for the filter material that ended up in the acetone catch.

○

The Kuma Scott HT-1 is a true outside air unit in that all air entering the combustion chamber first must pass through the pedestal. It was a good performer in that all test runs took off as expected. The higher emissions for the medium low, medium high and fan confirmation tests were due to unfortunate wood falls which blocked the air wash air flow through the coal bed. If these falls had not occurred the weighted average for the unit will have been considerably lower.

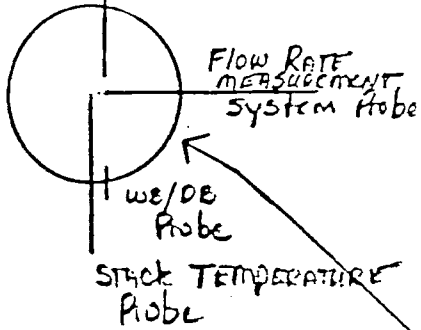
Please note that the data sheets list the unit as the Kuma Scott HT-1 (its true name) and the Scott Kuma HT-1. This mix up with the names reversed was not caught until testing was complete. Thus, it was thought it would be easier to deal with it via an explanation in the introduction rather than change all the data sheets.

Stack Ht. 15' 6"
15.0 ± 1 ft. (M28, 4.1.1)

Particulate Sampling probe

SO₂ Sampling Probe Ht. N/A
13.5 ft. ± 0.5 ft (MSH, 5.1.5.2)

Dp VILK!
DETAIL



Stack Measurements And Sampling Port Locations

STEEL Flue Pipe Ht 8' 4"
8.5 ± 0.5 ft (M28, 4.1.1)

SO₂ Injection Probe Ht. N/A
9.5 ft ± 0.5 ft (MSH, 5.1.5.1)

WET BULB/Dry Bulb Probe Ht 7' 8"
(NO SPECIFICATIONS GIVEN)

Particulate Sampling Probe N/A
Ht. 8.0 ± 0.5 ft (MSH, 5.1.2)

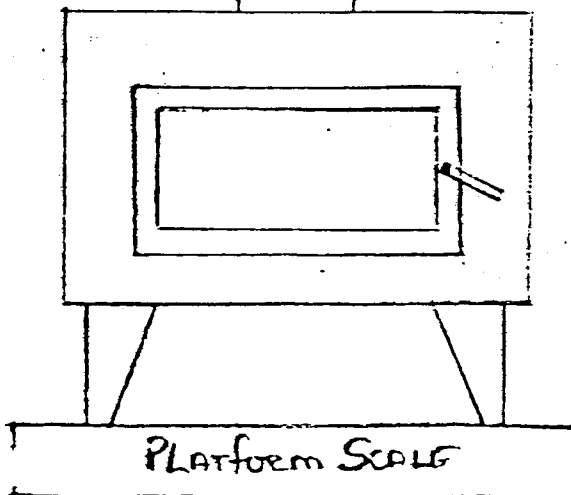
Stack Temperature Probe Ht.
8.5 ± 0.5 ft (DEQ, 3.3.1)
8' 1"

Flow Rate Measurement System Probe
Ht. 7' 8" 7.5 ± 1.0 ft (MSH, 5.1.6)

CUTAWAY DETAIL ON
Barometric Oil SEAL

Static Pressure Probe Ht 9"
< 1.0 ft above flue connector (M28, 6.2.3)

Stove Ht at the flue collar



Unit Kuma Scott HT-1
Date 8/28/96
Technician A.T. Myren

FAXED 6/13/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrom, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

7 / 15 / 196 and ending on about 7 / 21 / 196

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is 7/22-28/96

Sincerely,

Ben

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96
Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

7/15/96 and ending on about 7/21/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

FAXED 6/13/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: Kuma Scott Model #: HJ-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

7/22/96 and ending on about 7/28/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is 7/29 - 8/4/96

Sincerely,

Ben
Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled • or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

8/7/22/96 and ending on about 7/28/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated 6/13/96

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is 7/29-8/4/96

Sincerely,

Ben Myren

Ben Myren

epa not

FAXED 6/13/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

7/29/96 and ending on about 8/4/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is 8/5 - 11/96

Sincerely,

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id. 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
7/29/96 and ending on about 8/4/96

or has scheduled additional runs on the above unit starting on
_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated 6/13/96

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is 8/5 - 11/96

Sincerely,

Ben Myren

Ben Myren

epa not

FAXED 6/13/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, ID 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
8/5/96 and ending on about 8/11/96

or has scheduled additional runs on the above unit starting on _____
and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____.

Sincerely,


Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/9/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
8/5/96 and ending on about 8/11/96

or has scheduled additional runs on the above unit starting on
_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated 6/13/96
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is 8/12-18/96

Sincerely,
Ben Myren

Ben Myren

epa not

7/6/96
FAXED 7/6/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stone & Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
8/12/96 and ending on about 8/18/96

or has scheduled additional runs on the above unit starting on
_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____.

Sincerely,



Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96

Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

8/12/96 and ending on about 8/18/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

8/15/96 and ending on about 8/21/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated 6/13/96

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is 8/22-28/96

Sincerely,

Ben Myren

Ben Myren

epa not

7/6/96
FAXED 7/6/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove & Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: KUMA SCOTT Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
8/19/96 and ending on about 8/25/96

or has scheduled additional runs on the above unit starting on
_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____.

Sincerely,



Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96

Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

8/19/96 and ending on about 8/25/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____

Sincerely,

Ben Myren

Ben Myren

epa not

7/6/96
FAXED 7/6/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rothelm, ID 83858

Contact Person: Mark Fullman


Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: KUMS SCOT Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
8/26/96 and ending on about 9/1/96

or has scheduled additional runs on the above unit starting on _____
and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____

Sincerely,

Ben Myren

epa not

7/6/96

FAXED 7/6/96

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Mr. Robert Marshall
Woodheater Certification Program
Federal Programs Section
Stationary Sources Compliance Division
U. S. EPA
Mail Drop EN 341 W
2800 Crystal Road, 8th Floor
Arlington, VA 22202

Dear Mr. Marshall:

RE: WODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: KUMA Stone and Iron Works

Address: 450 old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 962-8002 has scheduled X or cancelled _____ the

Unit Name: KUMA Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
9/2/96 and ending on about 9/8/96

or has scheduled additional runs on the above unit starting on _____
and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____

Sincerely,

BM

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

8/9/96 and ending on about 9/15/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

9/16/96 and ending on about 9/22/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96
Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

9/16/96 and ending on about 9/22/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/9/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
9/23/96 and ending on about 9/29/96

or has scheduled additional runs on the above unit starting on
_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____.

Sincerely,
Ben Myren
Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96
Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on
9/23/96 and ending on about 9/29/96

or has scheduled additional runs on the above unit starting on
_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____
and is only for the dates shown. All other current notifications are still in effect. The next scheduled test
period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address: 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

9/30/96 and ending on about 10/6/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96
Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

9/30/96 and ending on about 10/6/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

10/7/96 and ending on about 10/13/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96
Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

10/7/96 and ending on about 10/13/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 9/15/96

Faxed: 9/15/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95

Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled _____ or cancelled X the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

10/14/96 and ending on about 10/20/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____

Sincerely,

Ben Myren

Ben Myren

epa not

MYREN CONSULTING
Suite 106
12810 NE 178 th St.
Woodinville, WA 98072

Date: 8/8/96
Faxed: 8/8/96

Mr. Robert Marshall
Woodheater Certification Program
Manufacturing, Energy and Transportation Division (2223A)
Office of Compliance
U. S. EPA
1200 Pennsylvania Ave. NW
Washington, D.C. 20044

Dear Mr. Marshall:

RE: WOODHEATER CERTIFICATION TEST NOTIFICATION

This letter is to notify EPA that

Name: Kuma Stove and Iron Works

Address 450 Old Highway 95
Rathdrum, Id 83858

Contact Person: Mark Freeman

Phone: (208) 762-8002 has scheduled X or cancelled _____ the

Unit Name: Kuma Scott Model #: HT-1

for certification testing at Myren Consulting's Woodinville, WA lab starting on

10/14/96 and ending on about 10/20/96

or has scheduled additional runs on the above unit starting on

_____ and ending on _____

NOTE: If this is a cancellation notice, the cancellation is for the notification dated _____

and is only for the dates shown. All other current notifications are still in effect. The next scheduled test

period for this unit is _____.

Sincerely,

Ben Myren

Ben Myren

epa not

III. EPA CUMULATIVE PROBABILITY CALCULATIONS

$$P_n = \frac{[\text{Hi Prob.} - \text{Low Prob.}][\text{Act. Dry Burn Rate} - \text{Low Dry Burn Rate}]}{.05} + \text{Low Prob.} = P_n$$

$P_1 = \frac{[.380 - .328][.973 - .950]}{.05} + .328 = .3519$ ✓

$P_2 = \frac{[.490 - .460][1.104 - 1.100]}{.05} + .460 = .4624$ ✓

$P_3 = \frac{[.857 - .840][1.739 - 1.700]}{.05} + .840 = .8533$ ✓

$P_4 = \frac{[.964 - .959][2.475 - 2.450]}{.05} + .959 = .9615$ ✓

$P_5 = \frac{[- -]}{.05} + =$

$P_6 = \frac{[- -]}{.05} + =$

$P_7 = \frac{[- -]}{.05} + =$

$P_8 = \frac{[- -]}{.05} + =$

$P_9 = \frac{[- -]}{.05} + =$

$P_{10} = \frac{[- -]}{.05} + =$

$P_{11} = \frac{[- -]}{.05} + =$

$P_{12} = \frac{[- -]}{.05} + =$

$P_{13} = \frac{[- -]}{.05} + =$

$P_{14} = \frac{[- -]}{.05} + =$

$P_{15} = \frac{[- -]}{.05} + =$

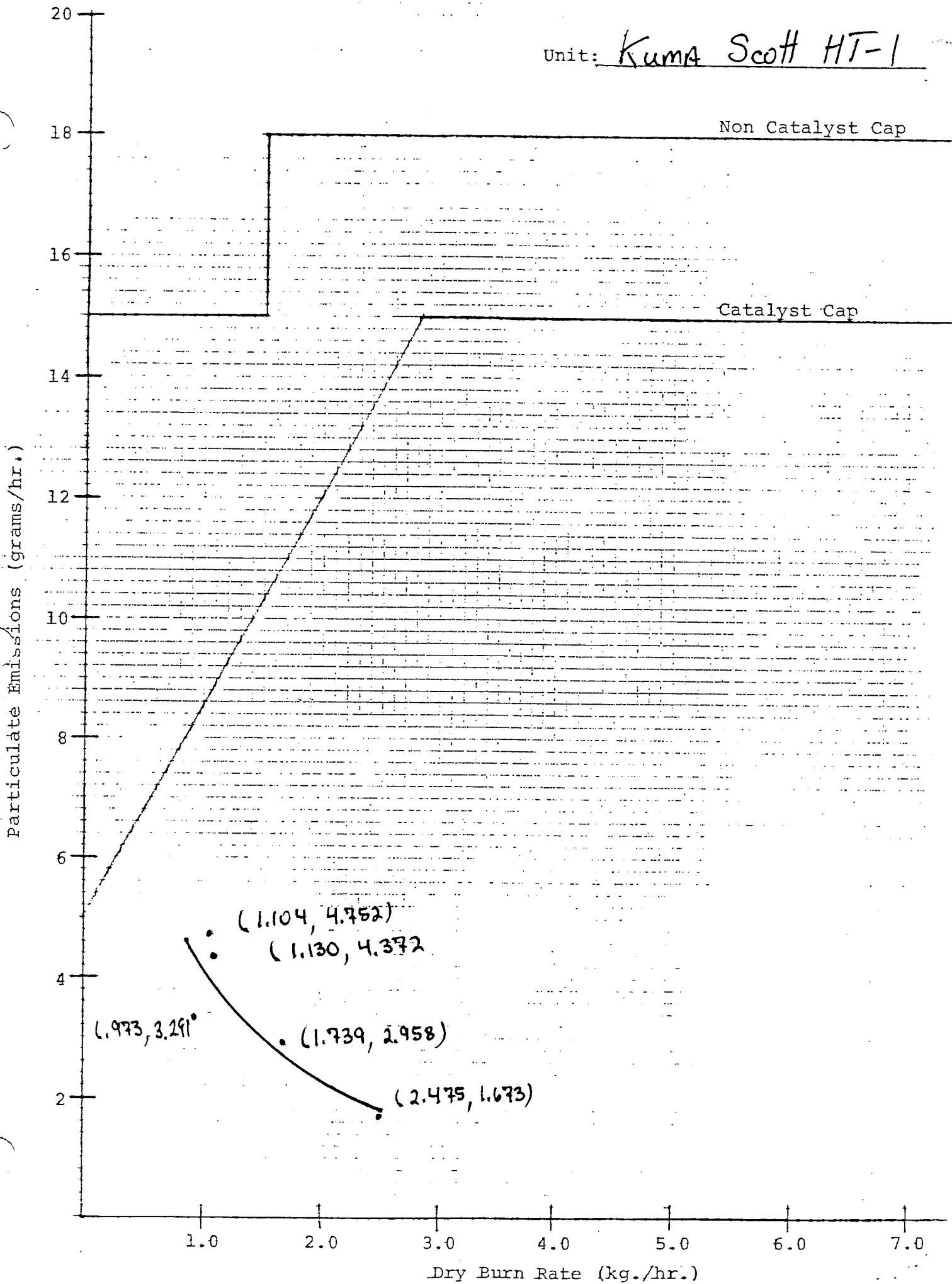
$K_1 = P_2 - P_0 =$	<u>.4624</u>	-	<u>.000</u>	=	<u>.4624</u>
$K_2 = P_3 - P_1 =$	<u>.8533</u>	-	<u>.3519</u>	=	<u>.5014</u>
$K_3 = P_4 - P_2 =$	<u>.9615</u>	-	<u>.4624</u>	=	<u>.4991</u>
$K_4 = P_5 - P_3 =$	<u>1.0000</u>	-	<u>.8533</u>	=	<u>.1467</u>
$K_5 = P_6 - P_4 =$	_____	-	_____	=	_____
$K_6 = P_7 - P_5 =$	_____	-	_____	=	_____
$K_7 = P_8 - P_6 =$	_____	-	_____	=	_____
$K_8 = P_9 - P_7 =$	_____	-	_____	=	_____
$K_9 = P_{10} - P_8 =$	_____	-	_____	=	_____
$K_{10} = P_{11} - P_9 =$	_____	-	_____	=	_____
$K_{11} = P_{12} - P_{10} =$	_____	-	_____	=	_____
$K_{12} = P_{13} - P_{11} =$	_____	-	_____	=	_____
$K_{13} = P_{14} - P_{12} =$	_____	-	_____	=	_____
$K_{14} = P_{15} - P_{13} =$	_____	-	_____	=	_____
$K_{15} = P_{16} - P_{14} =$	_____	-	_____	=	_____

IV. EPA WEIGHTED AVERAGES CALCULATIONS

The following formula is the one set out in Equation 28-1, Section 8.1, Method 28 and is to be used to calculate both the weighted average particulate emission rate (PM) and the weighted average overall efficiency (OE) as shown below. The formula uses interpolated probabilities for a given heat output demand calculated from the values listed in Table 28-1(2) in Method 28.

$$\overline{PM} = \frac{K_1 PM_1 + K_2 PM_2 + K_3 PM_3 + \dots + K_n PM_n}{K_1 + K_2 + K_3 \dots + K_n}$$

Unit: Kuma Scott HT-1



Woodstove Data Summary

FCT

Run #	2	1	3	4	5
Particulate Emissions:					
Concentration: grains/dscf:					
grams/m ³ :					
Emission Rate: grams/hr:	<u>3.291</u>	<u>4.752</u>	<u>2.958</u>	<u>1.673</u>	<u>4.372</u>
Emission Factor: gms/kg: (dry fuel weight basis)					
Front Half Catch: % of total					
Total Mass Captured:					
Frt & Bck Halves:	<u>28.6</u>	<u>29.0</u>	<u>14.1</u>	<u>4.9</u>	<u>33.5</u>
Efficiency Valves:					
Overall Appliance Efficiency					
Combustion Efficiency					
Heat Transfer Efficiency					

Heat Output:
 Avg. BTU/hr for test cycle 11,727 13,310 20,973 29,845 13,621 BTU/h

Fuel Burn Rates:
 Avg Kg/hr for test cycle
 (Wet basis) 1.167 1.848 2.119 3.028 1.380 Kg/hr
 Avg Kg/hr for test cycle
 (Dry basis) 0.973 1.104 1.739 2.475 1.190 Kg/hr

FCT
 5

RUN # 2 1 3 4

Average Temperatures:

Stack Gas	254	261	380	479	283	OF
Primary Combustion Chamber Gas	750	830	967	1032	778	OF
Secondary Combustion Chamber Gas	876	953	1123	1158	773	OF
Catalytic Combustor Exit Gas	N/A	N/A	N/A	N/A	N/A	OF
Stove Top	392	433	539	596	431	OF
Stove Left Sidewall	406	444	511	542	415	OF
Stove Back	146	157	181	159	266	OF
Stove Right Sidewall	383	391	490	521	408	OF
Stove Bottom	373	412	465	411	370	OF
Stove Temperature Change	-874	-70.8	-44.2	-33.4	-63.0	OF

Test Chamber Environment:

Avg. Barometric Pressure	29.88	29.95	29.92	29.95	29.95	in Hg
Avg. Temperature	74	82	73	70	71	OF
Avg. % Ambient Moisture	1.80	1.90	1.625	1.40	1.55	% H ₂ O
Avg. % Relative Humidity	63.5	51.5	54.5	53.5	56.5	%RH
Avg. Air Velocity	0	0	0	0	0	m/sec
Avg. Dilution Tunnel Draft (If Applicable)	0	0	0	0	0	in/H ₂ O

Test Fuel Weight and Burn Time:

Density (Dry basis)	.4673	.5195	.4703	.4867	.5091	gm/cm ³
Coal Bed Weight	2.7	2.5	2.5	2.3	2.5	lbs.
Pre Test Fuel Wt (Inc Kindling)	29.9	38.1	39.2	40.2	38.8	lbs.
Test Fuel Load Weight	10.9	10.9	10.9	10.9	10.9	lbs.
Total Test Cycle Burn Time	250	220	140	98	215	min.

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS
3/31/96

File Name: CKUMAR2

Stove Manufacturer: KUMA

Model Number: SCOTT HT-1

Lab Name: MYREN

Test Date: 8/29/96

Run Number: 2

Meter Box Y Factor: 1.012

Barometric pressure (in): 29.88

Gas meter temp (ave): 105.65
delta H(ave): 0.877

Gas meter initial reading: 786.9

Gas meter final reading: 910.872

Front catch (acetone) mg: 2.9

first filter catch (mg): 25.7

second filter catch (mg): 0

tunnel flow (ave cfm): 137.71

Emission Rate(g/hr): 2.04

Emission Rate(M5H): 3.29

vs/VmTs: 0.01
vs ave: 763.64

Tunnel average temp (°f): 90.81

Test time(min): 250

Fuel Load(lb. wet): 10.9

Wood moisture(%wet): 18.038

Burn rate(dry kg/hr): 0.973

Samp vo(scF): 116.931

front filter number: 131

back filter number: 130

acetone beaker number: 9

PRELIMINARY RESULTS

FINAL RESULTS

X

SCOTT HT-1

2

8/29/96

0.973

2.041

3.291

GPH UNADJ

:ADJ

RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.036	89	786.900	75	0.900	772.80		
10	0.035	96	791.785	80	0.860	766.84	103.1	4.836
20	0.035	94	796.780	85	0.870	765.46	104.9	4.899
30	0.034	99	801.725	91	0.870	757.84	103.8	4.797
40	0.035	99	806.645	95	0.870	768.90	103.6	4.739
50	0.035	98	811.560	99	0.870	768.22	101.1	4.700
60	0.035	96	816.530	101	0.870	766.84	101.6	4.736
70	0.035	94	821.395	104	0.870	765.46	98.7	4.611
80	0.036	92	826.330	105	0.870	774.91	99.8	4.669
90	0.036	90	831.265	106	0.880	773.51	98.1	4.661
100	0.035	89	836.210	108	0.880	762.00	97.9	4.654
110	0.035	89	841.178	109	0.880	762.00	99.7	4.667
120	0.035	89	846.150	109	0.880	762.00	99.8	4.671
130	0.034	90	851.120	111	0.870	751.71	99.5	4.653
140	0.035	89	856.075	111	0.880	762.00	100.4	4.639
150	0.035	88	861.045	112	0.880	761.30	99.0	4.645
160	0.036	88	866.000	113	0.880	772.10	98.6	4.623
170	0.035	88	870.990	113	0.890	761.30	97.9	4.655
180	0.035	89	875.915	113	0.890	762.00	98.2	4.595
190	0.035	88	880.910	114	0.880	761.30	99.2	4.652
200	0.035	88	885.870	115	0.870	761.30	98.4	4.611
210	0.034	88	890.911	115	0.870	750.35	100.0	4.686
220	0.035	88	895.875	115	0.880	761.30	99.9	4.615
230	0.035	88	900.825	116	0.880	761.30	98.0	4.594
240	0.035	88	905.840	116	0.880	761.30	99.3	4.654
250	0.035	87	910.872	116	0.880	760.61	99.5	4.670
260						0.00	0.0	0.000
270						0.00	0.0	0.000
280						0.00	0.0	0.000
290						0.00	0.0	0.000
300						0.00	0.0	0.000
310						0.00	0.0	0.000
320						0.00	0.0	0.000
330						0.00	0.0	0.000
340						0.00	0.0	0.000
350						0.00	0.0	0.000

DATA SUMMARY

MODEL:

RUN:

DATE:

DBR:

GPH UNADJ

:ADJ

METHOD 5G-1

PARTICULATE SAMPLING DATA

Kura

LAB-1

DATE 8/29/96

PAGE 1 OF 2

MODEL # Scott

RUN # 2

METER BOX # 45G-P

METER Y 1.012

HT-1

FILTER # (F) 131 (R) 130

PRE TEST LEAK RATE = .002 CFM @ -23.75 IN. HG

FILTER SIZE: 110mm

POST TEST LEAK RATE = .000 CFM @ -11.25 IN. HG

PROBE LENGTH 24" g600

TIME		METER READING CU. FT.	PITOT dp	INL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1215	00	786.900	-036	89	75	0.90	0	N-1	0.5"	-028	93
25	10	791.785	-035	96	80	.86	0	2	1.5"	-042	92
35	20	796.780	-035	94	85	.87	0	3	4.5"	-040	92
45	30	801.725	-034	99	91	.87	0	4	5.5"	-080	92
55	40	806.645	-035	99	95	.87	0	W-1	0.5"	-026	91
1305	50	811.560	-035	98	99	.87	0	2	1.5"	-039	90
5	60	816.530	-035	96	101	.87	0	3	4.5"	-041	90
25	70	821.395	-035	94	104	.87	0	4	5.5"	-035	89
35	80	826.330	-036	92	105	.87	0	Avg. -0351			91.125
45	90	831.265	-036	90	106	.88	0	Pitot Leak Check			551.125
55	100	836.210	-035	89	108	.88	0	Pre <u>OK</u> Post <u>OK</u>			
1405	10	841.178	-035	89	109	.88	0	Cp = <u>0.99</u>			
15	20	846.150	-035	89	109	.88	0	N ↓ → W 1 2 3 4 3 4 ↑			
25	30	851.120	-034	90	111	.87	0	* = point of Avg. delta p			
35	40	856.075	-035	89	111	.88	0	Qs = $\left(\frac{\sqrt{(\Delta P \times BP)}}{T(^{\circ}R)}\right) \times 3167.2 =$			
45	50	861.045	-035	88	112	.88	0	<u>138.213</u> cfm			
55	60	866.000	-036	88	113	.88	0	BP = <u>Start</u> 29.88 in Hg			
1505	70	870.990	-035	88	113	.89	0	60 min <u>29.83</u>			
15	80	875.915	-035	89	113	.89	0	120 min <u>29.98</u>			
25	90	880.910	-035	88	114	.88	0	180 min <u>29.96</u>			

$\bar{X} = 29.88$ "Hg

METHOD 5G -1

PARTICULATE SAMPLING DATA

kuma

LAB-1

DATE 8/29/96

PAGE 2 OF 2

MODEL # Scott

RUN # 2

METER BOX # 45G-P

METER Y 1.012

HT-1

FILTER # (F) 131 (R) 130

PRE TEST LEAK RATE = .002 CFM @ -23.75 IN. HG

FILTER SIZE: 110 MM

POST TEST LEAK RATE = .000 CFM @ -11.25 IN. HG

PROBE LENGTH 24" glass

TIME		METER READING CU.FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1535	200	885.870	-035	88	115	.87	0	N-1	0.5"	-028	93
45	10	890.911	-034	88	115	.87	0	2	1.5"	-042	92
55	20	895.875	-035	88	115	.88	0	3	4.5"	-040	92
1605	30	900.825	-035	88	116	.88	0	4	5.5"	-030	92
15	40	905.840	-035	88	116	.88	0	W-1	0.5"	-026	91
25	50	910.872	-035	87	116	.88	0	2	1.5"	-039	90
	60							3	4.5"	-041	90
	70							4	5.5"	-035	89
	80							Avg. -0351			91.125
	90							Pilot Leak Check			851.125
	00							Pre OK			Post OK
	10							Cp = 0.99			N
	20							→ W 1 2 3 4			*
	30										3
	40										4
	50							*=point of Avg. delta p			
	60							Qs = (√(ΔP x BP)) x 3167.2 =			
	70							138.213			cfm
	80							BP = 240 min 29.88			in Hg
	90							250 min 29.88			

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

4th Round

Into Dessicator: Date: 6/27/96 Time: 1200 By: A.J. Kuma

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4824	8/9/96	1446	ATM	65.4819	8/9/96	1105	RLS				
2	66.1488	7/25/96	1217	RLS	66.1484	8/1/96	0958	ATM				
3	67.8548	8/8/96	1553	ATM	67.8542	8/9/96	1103	RLS	67.8544	8/14/96	11:30	ATM
4	67.5870	8/8/96	14124	ATM	67.5865	8/9/96	1130	RLS	KUMA	#1		
5	67.2054	8/8/96	1618	ATM	67.2050	8/9/96	1058	RLS	KUMA	5		
6	67.4250	7/3/96	1403	RLS	67.4244	7/10/96	1059	ATM	67.4250	7/25/96	1155	RLS
7	65.5422	8/8/96	1533	ATM	65.5423	8/9/96	1110	RLS	KUMA	4		
8	66.0183	7/10/96	1100	ATM	66.0187	7/25/96	1055	RLS				
9	66.9280	7/6/96	1312	ATM	66.9276	8/9/96	1120	RLS	KUMA	#2	✓	
10	66.0862	7/10/96	1111	ATM	66.0860	7/25/96	0933	RLS				
11	65.6989	7/10/96	1108	ATM	65.6989	7/25/96	1020	RLS				
12	Broken											

KUMA
BLANK 8/10/96

Checked By: _____ Date: _____ Time: _____

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	ZRH	Date	Time	By
58	70	47	7/13/96	0953	ATM
60	72	49	7/10/96	1006	ATM
57.5	69	48	8/1/96	0948	ATM
66	79	49	8/8/96	1235	ATM
60	72	49	8/9/96	0745	ATM
64	77	49	8/14/96	1116	ATM

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Dates From 6/29/96
Through 9/10/96

Scale Metric
Model AE100
SN K04827

TROEMNER CLASS 5 WTS.

100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Tech	Date	Time	Dry Bulb	Wet Bulb	% RH
100.0003	10.0000	1.0000	.1000	.0199	PLS	6/20/96	1625	61	74	47
100.0000	10.0000	1.0000	.1000	.0200	ATM	6/21/96	1259	61	74	47
100.0005	10.0001	1.0001	.1001	.0201	ATM	6/25/96	1410	63	76	48
99.9997	10.0000	1.0000	.1000	.0201	ATM	6/26/96	1558	64	78	46
99.9996	10.0000	1.0000	.1000	.0200	ATM	6/27/96	1718	65	78	49
99.9995	10.0000	1.0000	.1000	.0200	ATM	6/28/96	1254	58	70	49
100.0001	10.0000	1.0000	.1000	.0200	ATM	7/1/96	1504	65	78	49
99.9997	10.0000	1.0000	.1000	.0200	ATM	7/2/96	1816	64	77	49
99.9998	10.0000	1.0000	.1000	.0200	ATM	7/5/96	953	58	70	49
99.9999	10.0000	1.0000	.1000	.0201	ATM	7/8/96	1727	57	63	42
99.9996	10.0000	1.0000	.1000	.0200	ATM	7/9/96	1456	60	70 high	49
99.9998	10.0000	1.0000	.1000	.0201	ATM	7/10/96	1006	59	71	48
99.9998	10.0000	1.0000	.1000	.0200	ATM	7/11/96	0918	59	71	48
100.0000	10.0001	1.0001	.1001	.0201	ATM	7/12/96	842	59	71	48
100.0003	10.0003	1.0003	.1003	.0201	ATM	7/16/96	1233	62	75	49
99.9996	9.9998	.9998	.0998	.0198	ATM	7/17/96	1605	63	74	54
99.9999	10.0000	1.0000	.1000	.0200	ATM	7/18/96	0753	68	56	49
99.9999	10.0000	1.0000	.1000	.0200	ATM	7/19/96	0740	71	59	48
99.9999	10.0000	1.0000	.1000	.0200	ATM	7/20/96	1445	82	68	48
99.9996	10.0001	1.0001	.1001	.0201	ATM	7/23/96	1513	80	66	47
99.9999	10.0000	1.0000	.1000	.0200	ATM	7/24/96	0757	59	71	48
99.9999	10.0001	1.0001	.1001	.0201	ATM	7/24/96	1617	71	86	47
100.0002	10.0002	1.0002	.1002	.0201	ATM	7/25/96	0814	67	73	49
99.9995	10.0000	1.0000	.1000	.0202	ATM	7/27/96	2035	65	79	47
100.0000	10.0000	1.0000	.1000	.0202	ATM	8/1/96	0905	69	57.5	48
100.0000	10.0001	1.0001	.1001	.0202	ATM	8/1/96	1950	60	72	49
99.9998	10.0000	1.0000	.1000	.0202	ATM	8/2/96	801	59	71	49
100.0001	10.0000	1.0000	.1000	.0199	ATM	8/3/96	1235	66	79	49
99.9996	10.0000	1.0000	.1000	.0201	ATM	8/9/96	0154	60	72	49
100.0003	10.0001	1.0001	.1001	.0200	ATM	8/14/96	1176	64	77	49
99.9999	10.0001	1.0001	.1001	.0201	ATM	8/15/96	1908	66	79	49
100.0002	10.0000	1.0000	.1000	.0201	ATM	8/28/96	1611	70	85	49
99.9995	10.0000	1.0000	.1000	.0200	ATM	8/29/96	1008	67	77	49
99.9996	10.0000	1.0000	.1000	.0200	ATM	8/30/96	1005	61	73	48
99.9996	10.0000	1.0000	.1000	.0200	ATM	9/5/96	0954	59	71	48
99.9996	10.0000	1.0000	.1000	.0200	ATM	9/6/96	1030	72	80	49
100.0000	10.0000	1.0000	.1000	.0200	ATM	9/9/96	1806	76	83	48
100.0005	10.0002	1.0002	.1002	.0200	ATM	9/10/96	1726	77	84	48

R R R

R R R

R R

R R

R R

Unit: Kuma Scott HT-1
 Run: 2
 Date: 8/29/96
 Technicians: ATM RLS
 WST20, Form 5

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 EPA M5G-1

Filters

Filter # 131 (F) Beaker # 9 Final Wt. 66.9305 g ✓
 Final Wt .7670 g ✓ Ml 35 Tare Wt. 66.9276 g ✓
 Tare Wt .7414 g ✓ Desc. Acetone Net Wt. .0029 g ✓
 Net Wt .0256 g

Filter # 130 (R) Beaker # _____ Final Wt. _____ g
 Final Wt .7304 g ✓ Ml _____ Tare Wt. _____ g
 Tare Wt .7304 g ✓ Desc. _____ Net Wt. _____ g
 Net Wt .0000 g ✓

Acetone Blank Calculation: Blank done 8/8/96

Blank Beaker # 6 Final Wt 67.4251 g.
 Ml 140 Tare Wt 67.4250 g.
 Desc Acetone Net Wt .0001 g.
.0001 g ÷ 140 ml = .0000007 g/ml

Particulate Catch Calculation

Filter: .0257 g ✓
 Filter: .0000 g ✓
 Beakers: .0029 g - (.0000007)(35) = .0029 g ✓
 Total Catch g/Ml of Acetone
 Blank Value/Ml of Acetone
 Total Catch = .0286 g ✓

Unit SCOTT KUMA HT-1
 Run # 1
 Date 8/29/96
 Technician ATM, PLS.
 WST6-Form1, Rev11/89

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 1.716 ft³

Dilution Tunnel Draft (If applicable): Start 0 Stop 0

Test Chamber Air Velocity: Start: 0 Stop: 0 Avg: 0

Wet Bulb/ Start: WB: 64 °F DB: 71 °F 1.8 % Amb Moisture 68 %RH

Dry Bulb Stop: WB: 67 °F DB: 77 °F 1.8 % Amb Moisture 59 %RH

$\bar{X} = 1.8$ % Ambient Moisture $\bar{X} = 63.5$ % Relative Humidity (RH)

Empty

Stove Wt: 343.1 lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 433.1 lbs. Dry: 432.8 lbs.

Empty

Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Paper: 0.3 lbs. Wood: 4.0 lbs.

Pre Burn Fuel Wt. 11.2 + 11.5 + 12.9 Total: 35.6 lbs.

Total Kindling and Pre Burn Fuel Wt 39.9 lbs.

Coal Bed Wt-lbs: Range (2.7 - 2.2) 435.5 - 435.0 lbs. Actual: 2.7 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range $\frac{435.5}{\text{Upper Wt.}} + \frac{435.0}{\text{Lower Wt.}} 12 \times .25 = \underline{0.6}$ lbs.

Test Fuel Wt-lbs: Ideal 12.0 lbs. Range: 10.9 - 13.2 lbs. Actual: 10.9 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 14 Pcs.

2 x 4's x 14.5/16 " 3 Pcs 6.9 lbs. 63.3 %

4 x 4's x 14.5/16 " 1 Pcs 4.0 lbs. 36.7 %

Est. Dry Burn Rate (Kg/Hr.) $\frac{10.9}{2.2025} - \frac{(10.9 \times .18038)}{46} \times \frac{60}{350} = \underline{.9726}$ ✓
 Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO_E) (19,140) X $\frac{63}{100} \times .9726 = \underline{11,727}$ ✓
 (Avg BTU's/Hr) Est Heat Output (HO_E) BTU's/Hr

Comments:

STOVE OPERATING DATA
WOODSTOVE TEST DATA SHEET #9

Unit: Kenn Scott HT-1
Run: 2
Date: 8/29/96
Technician(s): ATM RLS
WST3-Form 1 Rev 9/90

Fire Started: 0815 PDST

Warm up and Preburn: Primary Air: Wide open from ignition until the start of the preburn when the primary air control(s) was (were) adjusted to the run setting of 3/8" open max. At the run setting until the start of the test.

3/8" open on arc = stop

Secondary Air:

No controls, Naturally drafted

Secondary Burn/~~By~~ Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge.

Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 25 seconds.

Test: Door Wide Open during loading _____ min 32 sec, then closed.

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 3/8" open max between 4:55 and 5:00. At the run setting of 3/8" open on arc at 5:00 into the run.

Secondary Air:

No Controls, Naturally drafted.

Secondary Burn/~~By~~ Bypass: N/A

Fan: Off during warm up. On high during the preburn, off at the start of the test. Off for 1st 30 minutes of test. On high at 30 minutes. On high for rest of test.

Test Run Anomalies:

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (11.2 lbs) added at 0832 .
 2nd Warm up/Pre Burn Fuel charge (11.5 lbs) added at 0938 .
 3rd Warm up/Pre Burn Fuel charge (12.9 lbs) added at 1028 .
 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____ .
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____ .
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____ .
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____ .
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____ .

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 0.3 lbs.

All pre burn/warm up fuel pieces were either 14 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 14 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 14 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 14 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

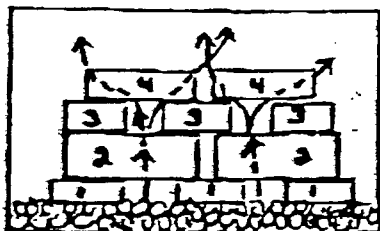
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

Unit: SCOTT KUHA HT-1
Run # 2
Date 8/29/96
Technician ATH, RLS
Page 2 of 3
WST7-Form2-A, Rev 6/90

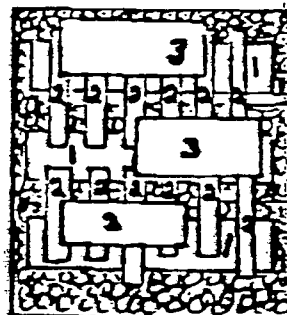
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP

surface temperature(s) and the peak value(s) obtained were 930 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 3/8" open on arc 3.0 lbs above the upper charcoal bed weight.

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit SCOTT KUMA HT-1
Run # 2
Date 8/29/96
Technician ATM, RLS
Page 3 of 3
WST5-Form2-Rev11/89

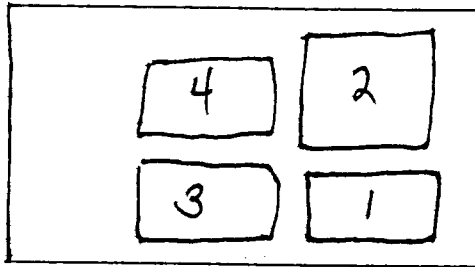
Additional Comments:

Test Start Sequence: (1) Turn Fan off. (2)

Opened primary air control wide open (3) Open door (4) loaded test fuel charge into the stove (5) Photo (6) Closed the door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



FRONT of stove view
4 X 4's: 2
2 X 4's: 1, 3 & 4
Loading Sequence: 1, 2, 3 & 4
Driest Pcs in Load 3

Loaded the test fuel charge on an essentially level, large-medium sized, hot coal bed (in appearance, color and temperature for a low burn rate. Load 0:32, Ignition 0:30, Vertical column of flame (VC) to Griddle 2:00, Secondaries igniting 2:15 at top of VC 3:00 Middle tube igniting. 3:30 Front Tube igniting 4:00 Secondaries all across the top of the fuel load under the Griddle. 5:00 Primary Air → run setting. Flames decreased. Maintained Hot pocket under pc 3, VC on left, in center and right (sm) w/ 2nds at top of L & Center VC's. Never bot gas balance. Max CO 0.53%. 11:35 top of pc 2 ignited. Flames steadily increasing big hole burnt out under pc 3. Btm spacer gone. 10:10 CO ↑ to 0.66%. 20:13 CO ↓ to 0.37% Front tube igniting 59:00. Rt stack broke down and slid forward into air wash. CO ↑. Very Lt. Smoke.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: SCOTT KUMYA HT-1
Run: 2
Date: 8/29/96
Technician: ATH, PLS.
WST1-Form7-Rev11/89

Room Temperature: 70 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture

Uncor Values are corrected for temperature: Yes No

Time Test Fuel Moisture Readings taken at: 1040

Calibration Checks: X Y 12.5 12.4 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x	K	8.0	8.4	8.0	8.4	8.0	8.4	8.400
2									
3									
4									
5	2x4x8'	P	18.0	19.2	18.0	19.2	18.5	19.8	19.400
6	"	P	18.5	19.8	18.0	19.2	18.0	19.2	19.400
7	"	P	19.5	20.9	19.0	20.3	19.5	20.9	20.700
8									59.500
9									
10									
11	2x4x14 5/16"	T	20.5	22.0	20.5	22.0	20.0	21.4	21.800
12	"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
13	"	T	22.5	24.3	22.0	23.7	21.0	22.6	23.533
14									
15	4x4x14 5/16"	T	21.5	23.1	22.5	24.3	21.5	23.1	23.500
16									88.033
17									
18									
19	FEET	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
20									OUT SPACERS

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.400%	19.833%	22.008%
% Moisture - Wet Basis:	7.749%	16.551%	18.038%

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: SCOTT KUMA HT-1
Run#: 2
Date: 8/29/96
Technician: ATH RLS
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): IN. 1.545 cm 3.9243 ✓
Width (W): IN. 3.576 cm 9.0830 ✓
Length (L): 3.555 cm
3.535 cm
3.565 cm
3.563 cm
Length \bar{X} = IN. 3.555 ✓ cm 9.0297 ✓
Volume: 321.860 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 70 °F Correction Factor: 0

Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	<u>22.5</u>	<u>24.3</u>	<u>24.3</u>
Bottom:	<u>22.5</u>	<u>24.3</u>	<u>24.3</u>
Side:	<u>22.5</u>	<u>24.3</u>	<u>24.3</u>
\bar{X} :		<u>24.300</u>	<u>24.3</u>

Avg % Moisture (Dry) 24.300 % ✓

Aug % Moisture (Wet) 19.549 % ✓

Scale: Leveled In Out

Zeroed: In Out

Wet Weight: 196.4 g Dry Weight: 150.4 g

% Moisture Dried Basis: 21.421 % ✓
[1 - (Dry Wt - Wet Wt)] X 100

Into Dryer 8/29/96 1015 215 °F
Out of Dryer 9/9/96 1715 220 °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 150.4 g ÷ 321.860 cm³ = 4673 g/cm³ ✓
(dry wt) (volume)

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g

Wet Wt: _____ g - _____ g = _____ g

Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.

Dry Wt: _____ g - _____ g = _____ g

Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: _____ %

[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Minute Time	Scale Wt	lbs left	Burn Rate	1		2		3		T/C(1)T/C(2)		T/C(3)		4	Static Press.	Comments
				V.	%CO ₂	V.	%O ₂	V.	%CO	Bal	Wet Bulb	Dry Bulb	% H ₂ O			
120	437.4	1.9	1.2	26.7	6.54	53.8	13.4	1.07	6.4	87	98	4.0	110	243	-0.41	Flow
125	437.3	1.8	1.1	26.6	6.64	53.4	13.3	0.97	7.2	86	97	3.8	109	247	-0.41	S0 ₂ 1.5
130	437.1	1.6	1.2	27.9	6.96	57.5	12.8	0.89	7.8	86	97	3.8	109	250	-0.41	CO 1.5
135	437.0	1.5	1.1	28.2	7.04	57.2	12.8	0.92	7.6	85	95	3.7	108	248	-0.41	CO 1.5
140	436.9	1.4	1.1	21.3	5.33	56.8	14.2	1.61	3.3	84	90	3.7	106	229	-0.38	CO 1.5
145	436.8	1.3	1.1	20.2	5.06	57.4	14.3	1.71	3.0	83	87	3.7	105	218	-0.36	
150	436.7	1.2	1.1	19.6	4.91	58.0	14.5	1.68	2.9	82	85	3.5	104	210	-0.35	
155	436.6	1.1	1.1	20.3	5.08	57.5	14.3	1.69	3.0	81	87	3.4	103	206	-0.34	
160	436.6	1.1	0	19.4	4.86	58.2	14.5	1.88	2.6	81	88	3.4	103	200	-0.33	
165	436.5	1.0	1.1	20.0	5.01	57.6	14.4	1.85	2.7	81	88	3.4	102	197	-0.32	
170	436.5	1.0	0	19.7	4.94	57.7	14.4	1.88	2.6	81	89	3.3	100	194	-0.31	
175	436.4	0.9	1.1	19.3	4.84	58.0	14.5	1.88	2.6	81	89	3.3	101	192	-0.30	Flow
180	436.4	0.9	0	18.9	4.74	58.4	14.6	1.92	2.5	82	91	3.4	100	191	-0.30	S0 ₂ 1.5
185	436.3	0.8	1.1	19.3	4.84	58.1	14.5	1.90	2.5	82	91	3.4	101	188	-0.29	CO 1.5
190	436.2	0.7	1.1	18.9	4.74	58.1	14.5	2.06	2.3	82	92	3.4	100	186	-0.29	CO 1.5
195	436.2	0.7	0	18.7	4.69	58.4	14.6	2.11	2.2	82	92	3.4	100	185	-0.28	CO 1.5
200	436.1	0.6	1.1	20.3	5.08	57.5	14.3	1.84	2.8	82	92	3.4	100	184	-0.28	
205	436.0	0.5	1.1	20.7	5.18	57.2	14.3	1.79	2.9	82	93	3.3	100	184	-0.28	
210	436.0	0.5	0	21.3	5.33	56.6	14.1	1.78	3.0	83	93	3.4	100	184	-0.27	
215	435.9	0.4	1.1	21.0	5.26	57.0	14.2	1.70	3.1	83	93	3.4	99	183	-0.27	
220	435.8	0.3	1.1	21.3	5.33	56.6	14.1	1.72	3.1	82	95	3.1	99	182	-0.27	
225	435.8	0.3	0	21.9	5.48	56.2	14.0	1.68	3.3	82	97	3.1	99	182	-0.27	
230	435.7	0.2	1.1	19.9	4.98	58.5	14.6	1.54	3.2	81	98	3.1	99	180	-0.26	
235	435.7	0.2	0	18.1	4.57	59.7		1.83	2.5	81	99	3.0	98	177	-0.26	
240														2206	-0.33	Flow
245																4840

BURNER AND FLUE GAS DATA
 WOODS BURNER DATA SHEET #12
 WST2-Form 14 Rev 1/88

Site: SCOTT KUMHA HT-1 Date: 8/29/96
 Technician(s): ATH, KLS.
 Page: 3 of 3

Minute Time	Scale Wt	lbs left	Burn Rate	1		2		3			T/C(1)/T/C(2)			T/C(3)		Stack	SO ₂ v.	PPM	Static Press.	Comments
				CO ₂ v.	%CO ₂	O ₂ v.	%O ₂	TeI	CO v.	%CO	BaI	Wet Bulb	Dry Bulb	% H ₂ O	CaIc W/B					
240	435.6	1.1	1.1	1.81	4.54	59.8	14.9				1.78	2.6	81	99	3.0	98	177		7.026	Flow
245	435.6	1.1	0	1.79	4.49	60.2	15.0				1.74	2.6	81	99	3.0	98	176		7.026	SO ₂ 1.5
250	435.5	0	1.1	1.70	4.27	61.0	15.2				1.72	2.5	81	99	3.0	98	176		7.026	SO ₂ 1.5
255																			1.078	SO ₂ 1.5
260																			1.190	SO ₂ 1.5
265																			2.190	SO ₂ 1.5
270																			2.190	SO ₂ 1.5
275																			2.190	SO ₂ 1.5
280																			2.190	SO ₂ 1.5
285																			2.190	SO ₂ 1.5
290																			2.190	SO ₂ 1.5
295																			2.190	SO ₂ 1.5
300																			2.190	SO ₂ 1.5
305																			2.190	SO ₂ 1.5
310																			2.190	SO ₂ 1.5
315																			2.190	SO ₂ 1.5
320																			2.190	SO ₂ 1.5
325																			2.190	SO ₂ 1.5
330																			2.190	SO ₂ 1.5
335																			2.190	SO ₂ 1.5
340																			2.190	SO ₂ 1.5
345																			2.190	SO ₂ 1.5
350																			2.190	SO ₂ 1.5
355																			2.190	SO ₂ 1.5

x

TEMPERATURES
RECORD SHEET #14
WST2-Form14 Rev7/96

U: SCOTT KUMA HT-1 Date: 8/29/96
R: 2 Technician(s): ATH, R.
Page: 1 of 3

T/C#	Minute Time	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
		Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Gas	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
0	15	369	461	144	442	450	802	776	71	89	248	36	75	35		
5	20	363	447	186	431	417	760	1115	74	103	247	37	75	35		
10	25	493	434	215	418	429	707	798	70	96	247	37	76	35		
15	30	533	424	227	407	424	704	841	70	95	248	37	76	35		
20	35	535	416	233	396	412	714	879	70	94	248	37	76	36		
25	40	586	409	234	388	402	741	886	70	96	248	37	76	36		
30	45	641	404	234	383	393	801	1074	70	99	248	37	76	35		
35	50	680	418	176	389	389	830	1099	70	99	248	37	77	35		
40	55	684	426	149	395	384	867	1241	72	99	248	37	77	35		
45	00	696	433	140	401	377	880	1239	72	100	248	37	77	35		
50	05	639	439	137	409	375	883	1253	71	98	248	37	77	35		
55	10	592	441	135	412	374	883	1265	72	97	247	37	77	35		
60	15	681	575	2210	487	4826	9572	12,466	852							
60	15	558	443	134	416	375	898	1199	71	96	247	37	77	35		
65	20	536	446	134	417	379	906	1178	72	95	247	37	77	35		
70	25	520	447	135	421	380	892	1103	71	94	247	37	78	35		
75	30	480	448	136	422	382	867	982	72	93	248	38	78	35		
80	35	442	445	136	420	383	842	926	72	92	248	38	78	35		
85	40	418	440	137	416	381	822	914	71	91	248	38	77	35		
90	45	393	434	137	414	379	818	908	72	90	248	38	77	35		
95	50	377	429	137	410	377	796	897	73	90	247	37	77	36		
100	55	360	422	137	404	373	804	884	73	89	248	37	77	35		
105	00	353	417	137	400	370	788	904	73	89	247	37	77	35		
110	05	357	413	138	395	367	784	917	74	89	248	37	77	35		
116	10	352	410	138	392	362	793	912	74	89	248	37	77	35		
120	15	5140	5794	1626	4922	4508	10,010	11,724	868							
125	20	11,957	19,346	3846	9798	9334	19,582	24,190	1720							

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute/Time	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalyst	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
120	358	406	139	389	360	748	881	74	89	248	37	77	35		
125	365	403	138	388	358	757	871	75	90	248	36	76	35		
130	371	399	136	388	360	767	893	75	90	248	36	76	35		
135	375	396	135	388	362	810	912	75	90	248	36	76	35		
140	360	395	134	387	365	793	838	75	89	248	36	77	35		
145	339	395	134	383	368	778	834	75	89	247	36	77	35		
150	325	396	132	377	370	764	816	76	88	247	36	77	35		
155	316	396	132	377	368	757	807	76	88	247	36	77	35		
160	307	395	132	364	367	778	759	76	88	248	36	77	36		
165	295	397	131	361	368	773	743	77	87	248	36	77	35		
170	294	396	131	356	369	775	737	77	88	248	36	77	36		
175	290	398	131	355	366	702	726	77	88	248	36	77	36		
180	3995	4772	1605	4508	4381	9036	9817	908							
180	285	398	132	353	364	688	717	77	89	247	37	77	36		
185	282	396	132	350	362	675	717	77	89	247	37	77	36		
190	278	393	132	347	360	667	708	77	88	247	37	77	36		
195	276	388	132	347	359	665	709	77	88	248	38	77	36		
200	273	384	133	346	356	661	718	77	88	248	38	77	36		
205	272	381	133	346	357	655	721	77	88	248	38	77	36		
210	272	376	133	346	356	658	731	77	88	248	38	77	36		
215	273	373	133	347	354	654	734	77	89	247	38	77	36		
220	271	371	133	348	355	652	731	77	88	247	37	77	36		
225	272	368	134	348	353	654	734	77	88	247	37	77	36		
230	269	365	134	349	352	627	715	77	88	248	37	77	36		
235	266	361	134	348	350	612	696	77	88	248	36	78	36		
240	3289	4554	1595	4175	4478	7868	8631	924							

7284 9326 3200 8683 8659 16904 18448 1832

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 8/29/96 Analyte: CO₂

Source: Kuma Scott HT-1 Run #: 2

Zero Cyl #: 4-36919 Conc. 00.0 % CO₂ Cyl Press: 2025 psi

Certified by: Cascade Air Gas Date: 4/24/96

Span Cyl #: W 260 657 Conc. 10.1 % CO₂ Cyl Press: 970 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: A.T. Myren Time: 1100 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	10.1	.404	10.1	40.0	.401	9.977	-.1230	-1.22

Comments:

Post Run Audit: By: A.T. Myren Time: 1655 Temp: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.1	.404	10.1	40.1	.402	10.007	-.0983	-0.97

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Differece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 3/29/96 Analyte: O₂

Source: Kurra Scott HT-1 Run #: 2

Zero Cyl #: 4-36919 Conc. 00.0 % O₂ Cyl Press: 2025 psi

Certified by: Cascade Air Gas Date: 4/24/96

Span Cyl #: W260657 Conc. 12.5 % O₂ Cyl Press: 970 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: A.T. Myren Time: 1100 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.4	00.2	.0552	.0552	+0.22
Span	12.5	50.0	12.5	12.55	49.8	12.475	-0.025	-0.66

Comments:

Post Run Audit: By: A.T. Myren Time: 1655 Temp.: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.4	00.2	.0552	.0552	+0.22
Span	12.5	50.0	12.5	12.55	49.8	12.475	-0.025	-0.66

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 3/29/96 Analyte: CO

Source: Kuma Scott HT-1 Run #: 2

Zero Cyl #: 4-36919 Conc. 00.0 % CO Cyl Press: 2025 psi

Certified by: Cascade Air Gas Date: 4/24/96

Span Cyl #: W260 657 Conc. 2.47 % CO Cyl Press: 970 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 1100 Temp: 78 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.3	-0062	-0062	-0.12
Span	2.47	49.4	2.47	2.49	49.5	24004	-0696	-2.82

Comments:

Post Run Audit: By: A.T. Myren Time: 1655 Temp.: 75 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.2	-0013	-0013	-0.03
Span	2.47	49.4	2.47	2.46	49.0	2376	-0938	-3.80

Comments:

+ Conc. Difference = Act % - Exp (Std) %
 Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: SCOTT KUMHA HT-1
 Run: 2
 Date: 8/29/96
 Technicians: ATH, RLS
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 69 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 69.0 °F; T/C#2: 69.0 °F;
 T/C #3: 69.0 °F; T/C #4: 69.0 °F; T/C #5: 69.0 °F;
 T/C #6: 68.8 °F; T/C #7: 68.8 °F; T/C #8: 68.8 °F;
 T/C #9: 69.0 °F; T/C #10: 69.0 °F; T/C #11: 68.8 °F;
 T/C #12: 68.8 °F; T/C #13: 69.0 °F; T/C #14: 69.0 °F;
 T/C #15: 69.0 °F; T/C #16: 69.0 °F; T/C #17: _____ °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: _____

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : -0.4 °F Adj to: 0.0 °F Post Test Check Zero (0°F): 0.4 °F % Difference +0.02
 Span (2000°F): 1999.6 °F Adj to: 2000.0 °F Span (2000°F): 2000.6 °F +0.03
 (Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check

0°F = 0.0 °F; 200°F = 202.0 °F; 400°F = 398.8 °F;
 600°F = 601.4 °F; 800°F = 801.0 °F; 1000°F = 1000.8 °F;
 1200°F = 1198.8 °F; 1400°F = 1399.6 °F; 1600°F = 1599.0 °F
 1800°F = 1799.6 °F; 2000°F = 2000.0 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre OK Post OK
 Draft (Static) Gauge Zero Check: Pre OK Post OK

Scale Check Pre (Wt, #'s): 433.1 - 438.1 5.0 lbs, OK (RLS)
 Post (Wt, #'s): 435.3 - 440.3 5.0 lbs, OK (RLS)

Stack cleaned prior to the run: Yes _____ No ✓
 Tunnel cleaned prior to the run: Yes _____ No ✓

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS
3/31/96

File Name:	CKUMAR1	RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
Stove Manufacturer:	KUMA	0	0.038	96	630.000	80	0.900	798.09		
Model Number:	SCOTT HT-1	10	0.035	100	635.305	85	0.900	768.69	108.4	5.216
Lab Name:	MYREN	20	0.035	103	640.320	90	0.890	770.75	106.0	4.886
Test Date:	8/28/96	30	0.034	104	645.275	96	0.880	760.33	103.5	4.775
Run Number:	1	40	0.035	104	650.165	101	0.880	771.43	102.7	4.670
Meter Box Y Factor:	1.012	50	0.036	102	655.080	105	0.880	780.99	100.6	4.661
Barometric pressure (in):	29.95	60	0.036	100	660.038	111	0.880	779.60	98.8	4.652
Gas meter temp (ave):	110.57	70	0.035	99	664.940	110	0.880	768.01	97.9	4.608
delta H(ave):	0.886	80	0.035	94	669.890	112	0.870	764.56	99.1	4.637
Gas meter initial reading:	630.3	90	0.035	97	674.865	113	0.880	766.63	100.4	4.652
Gas meter final reading:	739.887	100	0.036	97	679.850	115	0.880	777.50	100.0	4.645
Front catch (acetone) mg:	5.9	110	0.035	96	684.855	116	0.880	765.94	98.6	4.656
first filter catch (mg):	33.1	120	0.036	95	689.770	117	0.890	776.11	98.2	4.572
second filter catch (mg):	0	130	0.035	95	694.740	117	0.890	765.25	97.8	4.615
tunnel flow (ave cfm):	138.10	140	0.036	93	699.720	118	0.890	774.71	98.8	4.617
Emission Rate(g/hr):	3.178	150	0.036	94	704.660	118	0.890	775.41	97.0	4.580
Emission Rate(M5H) :	4.752	160	0.036	93	709.695	119	0.890	774.71	98.5	4.660
vs/VmTs:	0.01	170	0.035	93	714.735	119	0.890	763.87	98.6	4.664
vs ave:	771.90	180	0.035	93	719.765	119	0.890	763.87	99.8	4.655
Tunnel average temp (°f):	96.48	190	0.036	93	724.785	120	0.890	774.71	99.5	4.638
Test time(min):	220	200	0.036	93	729.810	120	0.890	774.71	98.2	4.642
Fuel Load(lb. wet):	10.9	210	0.036	93	734.845	121	0.880	774.71	98.2	4.643
Wood moisture(%wet):	18.139	220	0.035	92	739.887	121	0.880	763.18	98.2	4.650
Burn rate(dry kg/hr):	1.104	230						0.00	0.0	0.000
Samp vol(scf):	102.994	240						0.00	0.0	0.000
front filter number	127	250						0.00	0.0	0.000
back filter number	126	260						0.00	0.0	0.000
acetone beaker number	4	270						0.00	0.0	0.000
PRELIMINARY RESULTS		280						0.00	0.0	0.000
FINAL RESULTS	X	290						0.00	0.0	0.000
DATA SUMMARY		300						0.00	0.0	0.000
MODEL :	SCOTT HT-1	310						0.00	0.0	0.000
RUN:	1	320						0.00	0.0	0.000
DATE:	8/28/96	330						0.00	0.0	0.000
DBR:	1.104	340						0.00	0.0	0.000
GPH UNADJ	3.178	350						0.00	0.0	0.000
ADJ	4.752							0.00	0.0	0.000

METHOD 5G-1

PARTICULATE SAMPLING DATA

Kuma
Scott

LAB-1

DATE 8/28/96

PAGE 1 OF 2

MODEL # HT-1

RUN # 1

METER BOX # 45G-P

METER Y 1.012

FILTER # (F) 127 (R) 126

PRE TEST LEAK RATE = .0005 CFM @ -15.5 IN. HG

FILTER SIZE: 110 mm

POST TEST LEAK RATE = .001 CFM @ -8.5 IN. HG

PROBE LENGTH 24" glass

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1235	00	630.300	-038	96	80	0.90	0	N-1	0.5"	-032	99
45	10	635.305	-035	100	85	.90	0	2	1.5"	-042	98
55	20	640.320	-035	103	90	.89	0	3	4.5"	-042	98
1305	30	645.275	-034	104	96	.88	0	4	5.5"	-031	98
15	40	650.165	-035	104	101	0.88	0	W-1	0.5"	-027	97
25	50	655.080	-036	102	105	.88	0	2	1.5"	-041	97
35	60	660.038	-036	100	111	.88	0	3	4.5"	-043	97
45	70	664.940	-035	99	110	.88	0	4	5.5"	-033	96
55	80	669.890	-035	94	112	.87	0	Avg. -0364			97.5
1405	90	674.865	-035	97	113	.88	0	Pilot Leak Check			557.5
15	100	679.850	-036	97	115	.88	0	Pre <u>OK</u> Post <u>OK</u>			
25	10	684.855	-035	96	116	.88	0	Cp = 0.99			
35	20	689.770	-036	95	117	.89	0	→ W 1 2 3 4			
45	30	694.740	-035	95	117	.89	0	3			
55	40	699.720	-036	93	118	.89	0	4			
1505	50	704.660	-036	94	118	.89	0	↑			
15	60	709.695	-036	93	119	.89	0	* = point of Avg. delta p			
25	70	714.735	-035	93	119	.89	0	Qs = (√(ΔP x BP) / T(°R)) x 3167.2 =			
35	80	719.765	-035	93	119	.89	0	N <u>140.008</u> cfm			
45	90	724.785	-036	93	120	.89	0	BP = Street <u>29.95</u> in Hg			

60 29.95
 120 29.95
 180 29.95
 Stop 29.95
X = 29.95

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 6/1/96 Time 1532 By ATM Front Half _____ Back Half _____

Manufacturer: S&S Size: 110 mm Lot.No.: 75941 Grade: #250105

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
126	.7451	6/3/96	1111	ATM	.7449	6/5/96	1853	RLS				
127	.7364	"	1110	ATM	.7360	6/5/96	1852	RLS				
128	.7419	"	1109	ATM	.7416	6/5/96	1851	RLS				
129	.7422	"	1108	ATM	.7420	6/5/96	1850	RLS				
130	.7306	"	1107	ATM	.7304	6/5/96	1849	RLS				
131	.7420	"	1106	ATM	.7413	6/5/96	1848	RLS	.7414	6/6/96	11:35	ATM
132	.7394	"	1102	ATM	.7371	6/5/96	1848	RLS				
133	.7391	"	1102	ATM	.7369	6/5/96	1847	RLS				
134	.7404	"	1101	ATM	.7403	6/5/96	1846	RLS				
135	.7390	"	1101	ATM	.7389	6/5/96	1845	RLS				
136	.7388	"	1100	ATM	.7386	6/5/96	1844	RLS				
137	.7395	"	1059	ATM	.7392	6/5/96	1843	RLS				
138	.7394	"	1056	ATM	.7392	6/5/96	1843	RLS				
139	.7435	"	1058	ATM	.7433	6/5/96	1842	RLS				
140	.7395	"	1059	ATM	.7393	6/5/96	1840	RLS				
141	.7486	"	1059	ATM	.7477	6/5/96	1839	RLS	.7476	6/6/96	1133	ATM
142	.7265	6/5/96	1838	RLS	.7264	6/6/96	11:32	ATM				
143	.7258	6/5/96	1837	RLS	.7258	6/6/96	11:31	ATM				
144	.7254	6/5/96	1836	RLS	.7254	6/6/96	11:30	ATM				
145	.7375	"	1056	ATM	.7372	6/5/96	1830	RLS	.7376	6/6/96	6:58	ATM
146	.7513	"	1056	ATM	.7510	"	1832	RLS				
147	.7465	"	1055	ATM	.7462	"	1833	RLS				
148	.7450	"	1054	ATM	.7448	"	1834	RLS				
149	.7474	"	1054	ATM	.7471	"	1835	RLS				
150	.7415	"	1053	ATM	.7413	"	1835	RLS				

Checked by A.T. M... Date: 6/6/96 Time 11:41

QA REWEIGH

Filter #	WT	Date	Time	By
136	.7386	6/6/96	11:34	ATM
129	.7412	6/6/96	11:36	ATM
149	.7472	6/6/96	11:39	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
59	72	45	6/3/96	1005	ATM
57	73	49	6/5/96	1825	RLS
51	73	49	6/6/96	1035	ATM

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

4th Round

Into Dessicator: Date: 6/27/96 Time: 1200 By: A.J. Mason

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4824	8/8/96	1446	ATM	65.4819	8/9/96	1125	RLS				
2	66.1488	7/25/96	1217	RLS	66.1484	8/1/96	0958	ATM				
3	67.8548	8/8/96	1553	ATM	67.8542	8/9/96	1103	RLS	67.8544	8/14/96	1130	ATM
4	67.5870	8/8/96	14124	ATM	67.5865	8/9/96	1130	RLS	KUMA #1			
5	67.2054	8/8/96	1618	ATM	67.2050	8/9/96	1058	RLS	KUMIA 5			
6	67.4250	7/3/96	1403	RLS	67.4241	7/10/96	1059	ATM	67.4250	7/25/96	1155	RLS
7	65.5422	8/8/96	1533	ATM	65.5433	8/9/96	1110	RLS	KUMA 4			
8	66.0183	7/10/96	1100	ATM	66.0187	7/25/96	1055	RLS				
9	66.9280	7/8/96	1312	ATM	66.9276	8/9/96	1120	RLS	KUMA #2			
10	66.0862	7/10/96	1111	ATM	66.0860	7/25/96	0933	RLS				
11	65.6989	7/10/96	1108	ATM	65.6989	7/25/96	1020	RLS				
12	Broken											

KUMA #1
KUMIA 5
KUMA 4
BLANK 8/8/96

Checked By: _____ Date: _____ Time: _____

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	ZRH	Date	Time	By
58	70	47	7/3/96	0953	ATM
60	72	49	7/10/96	1006	ATM
57.5	69	48	8/1/96	0948	ATM
66	79	49	8/3/96	1235	ATM
60	72	49	8/9/96	0945	ATM
64	72	49	8/14/96	1116	ATM

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Dates From 6/20/96
Through 9/10/96

Scale Me 1/100
Model AE100
SN K04827

TROEMNER CLASS 5 WTS.

100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Tech	Date	Time	Dry Bulb	Wet Bulb	% RH
100.0003	10.0000	1.0000	1.0000	0.1999	PLS	6/20/96	1625	61	74	47
100.0005	10.0000	1.0000	1.0000	0.2000	ATM	6/21/96	1259	61	74	47
99.9997	10.0001	1.0001	1.0001	0.2001	ATM	6/25/96	1410	63	76	48
99.9996	10.0002	1.0002	1.0002	0.2002	ATM	6/26/96	1558	64	78	48
99.9995	10.0000	1.0000	1.0000	0.2000	ATM	6/27/96	1710	65	78	49
100.0001	10.0001	1.0001	1.0001	0.2001	ATM	6/28/96	1254	58	70	49
100.0002	10.0001	1.0001	1.0001	0.2001	ATM	7/1/96	1504	64	78	49
99.9997	10.0002	1.0002	1.0002	0.2002	ATM	7/2/96	1316	64	77	49
99.9998	10.0002	1.0002	1.0002	0.2002	ATM	7/3/96	953	58	70	49
99.9999	10.0001	1.0001	1.0001	0.2001	ATM	7/8/96	1727	57	83	49
99.9996	10.0000	1.0000	1.0000	0.2000	ATM	7/9/96	1456	90 RH To High	83	49
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	7/10/96	1006	60	72	48
99.9998	10.0002	1.0002	1.0002	0.2002	ATM	7/11/96	0918	59	71	48
99.9999	10.0001	1.0001	1.0001	0.2001	ATM	7/12/96	842	59	71	48
100.0000	10.0001	1.0001	1.0001	0.2001	ATM	7/16/96	1233	62	75	49
100.0003	10.0003	1.0003	1.0003	0.2003	ATM	7/17/96	1605	63	74	54
99.9996	9.9998	0.9998	0.9998	0.1998	ATM	7/18/96	0733	68	56	49
99.9999	10.0000	1.0000	1.0000	0.2000	ATM	7/19/96	0740	71	59	48
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	7/22/96	1445	82	68	48
99.9998	10.0001	1.0001	1.0001	0.2001	ATM	7/23/96	1513	80	66	47
99.9999	10.0000	1.0000	1.0000	0.2000	ATM	7/24/96	0757	59	71	48
100.0002	10.0002	1.0002	1.0002	0.2002	ATM	7/25/96	0814	61	73	49
99.9995	10.0000	1.0000	1.0000	0.2000	ATM	7/31/96	2035	65	79	47
100.0000	10.0001	1.0001	1.0001	0.2001	ATM	8/1/96	0905	69	57.5	48
100.0001	10.0001	1.0001	1.0001	0.2001	ATM	8/1/96	1950	60	72	49
99.9993	10.0002	1.0002	1.0002	0.2002	ATM	8/2/96	1801	57	71	47
100.0001	10.0002	1.0002	1.0002	0.2002	ATM	8/13/96	1235	66	79	49
99.9996	10.0000	1.0000	1.0000	0.2000	ATM	8/19/96	0454	60	72	49
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	8/19/96	1116	64	77	49
99.9999	10.0001	1.0001	1.0001	0.2001	ATM	8/15/96	1908	66	79	49
100.0002	10.0001	1.0001	1.0001	0.2001	ATM	8/28/96	1611	70	85	49
99.9995	10.0000	1.0000	1.0000	0.2000	ATM	9/29/96	1008	64	77	49
99.9996	10.0000	1.0000	1.0000	0.2000	ATM	9/30/96	1005	61	73	48
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	9/5/96	0954	59	71	48
99.9999	10.0000	1.0000	1.0000	0.2000	ATM	9/6/96	1030	72	80	49
100.0000	10.0000	1.0000	1.0000	0.2000	ATM	9/9/96	1806	76	83	48
100.0002	10.0002	1.0002	1.0002	0.2002	ATM	9/10/96	1726	77	84	48

Unit: Kuma Scott HT-1
 Run: 1
 Date: 8/28/96
 Technicians: ATM RLS
 WST20, Form 5

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 EPA M5G-1

Filters

Filter # 126 (R) Beaker # 4
 Final Wt .7449 g ✓ Ml 65
 Tare Wt .7449 g ✓ Desc. Acetone
 Net Wt .0000 g ✓

Final Wt. 67.5924 g ✓
 Tare Wt. 67.5865 g ✓
 Net Wt. .0059 g ✓

Filter # 127 (F) Beaker # _____
 Final Wt .7691 g ✓ Ml _____
 Tare Wt .7360 g ✓ Desc. _____
 Net Wt .0331 g ✓

Final Wt. _____ g
 Tare Wt. _____ g
 Net Wt. _____ g

Acetone Blank Calculation: Blank done 8/8/96

Blank Beaker # 6 Final Wt 67.4251 g.
 Ml 140 Tare Wt 67.4250 g.
 Desc Acetone Net Wt .0001 g.

$$\frac{.0001 \text{ g}}{140 \text{ ml}} = .0000007 \text{ g/ml}$$

Particulate Catch Calculation

Filter: .0331 g ✓
 Filter: .0000 g ✓
 Beakers: .0059 g - $(.0000007)(65)$ = .0059 g ✓
 Total Catch g/MI of Acetone
 Blank Value/MI of Acetone
 Total Catch = .0390 g ✓

Unit SCOTT KUMA HT-1
 Run # 1
 Date 8/28/96
 Technician ATM, RLS.
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 1.716 ft³

Dilution Tunnel Draft (If applicable): Start 0 Stop 0

Test Chamber Air Velocity: Start: 0 Stop: 0 Avg: 0

Wet Bulb/ Start: WB: 66 °F DB: 78 °F 17% Amb Moisture 53 %RH

Dry Bulb Stop: WB: 71 °F DB: 85 °F 21% Amb Moisture 50 %RH

$\bar{X} = 1.90$ % Ambient Moisture $\bar{X} = 51.5$ % Relative Humidity (RH)

Empty

Stove Wt: 343.1 lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 433.0 lbs. Dry: 432.6 lbs.

Empty

Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Paper: 0.3 lbs. Wood: 4.0 lbs.

Pre Burn Fuel Wt. 11.8 + 11.3 + 10.7 Total: 33.8 lbs.

Total Kindling and Pre Burn Fuel Wt 38.1 lbs.

Coal Bed Wt-lbs: Range (2.7 - 2.2) lbs. Actual: 2.5 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range 435.3 + 434.8 12 .25 = 16 lbs.
 Upper Wt. Lower Wt.

Test Fuel Wt-lbs: Ideal 12.0 lbs. Range: 10.9-13.2 lbs. Actual: 10.9 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 14 Pcs.

2 x 4's x 14 5/16 " 3 Pcs 6.5 lbs. 59.6 %

4 x 4's x 14 5/16 " 1 Pcs 4.4 lbs. 40.4 %

Est. Dry Burn Rate (Kg/Hr.) $\frac{10.9 - (10.9 \times 18139)}{2.2046} \times \frac{60}{220} = \frac{1.104}{1.104}$ Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO_E) (19,140) X $\frac{63}{100} \times \frac{1.104}{1.104} = \frac{13,310}{13,310}$ Est Heat Output (HO_E) BTU's/Hr

Comments:

STOVE OPERATING DATA
WOODSTOVE TEST DATA SHEET #9

Unit: Kuma Scott HT-1
Run: 1
Date: 8/28/96
Technician(s): ATM RLS
WST3-Form 1 Rev 9/90

Fire Started: 0838 P.O.S.T.

Warm up and Preburn: Primary Air: Wide open from ignition until the start of the preburn when the primary air control(s) was (were) adjusted to the run setting of 3/8" open. At the run setting until the start of the test.

3/8" open = Stop.

Secondary Air: No Controls. Naturally drafted.

Secondary Burn/~~By~~Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge.

Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 20 seconds.

Test: Door Wide Open during loading _____ min 25 sec, then Closed.

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 3/8" open between 4:55 and 5:00. At the run setting of 3/8" open (Stop) at 5:00 into the run.

Secondary Air:

No Controls. Naturally drafted.

Secondary Burn/~~By~~Bypass: N/A

Fan: off during warm up. On high during preburn. Off at start of test. Off for 1st 30 minutes of test. On high at 30 minutes. On high for rest of test.

Test Run Anomalies:

This was an attempt at a low burn. Ended up a med. low, probably due to temps at start.

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

- 1st Warm up/Pre Burn Fuel charge (11.8 lbs) added at 0910.
- 2nd Warm up/Pre Burn Fuel charge (11.3 lbs) added at 1012.
- 3rd Warm up/Pre Burn Fuel charge (10.7 lbs) added at 1110.
- 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
- 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
- 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
- 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
- 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3 ^{lb.} pre burn/warm up fuel charge. The stove lost 0.4 lbs.

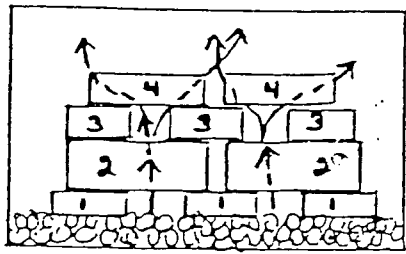
All pre burn/warm up fuel pieces were either 14" or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 14 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 14 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 14 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

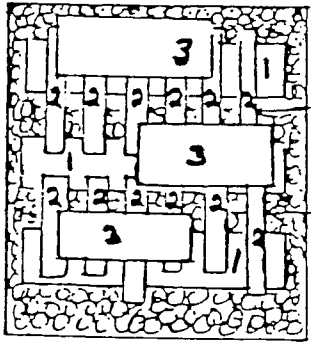
Unit: SCOTT KUMA HT-1
Run # 1
Date 8/22/96
Technician ATM, RLS
Page 2 of 3
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 880 °F.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 3/8" open on arc 3.5 lbs above the upper charcoal bed weight.

3/8" open on arc = 2.5 lbs

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit SCOTT KUHA HT-1
Run # 1
Date 8/28/96
Technician ATM, RLS
Page 3 of 3
WST5-Form2-Rev11/89

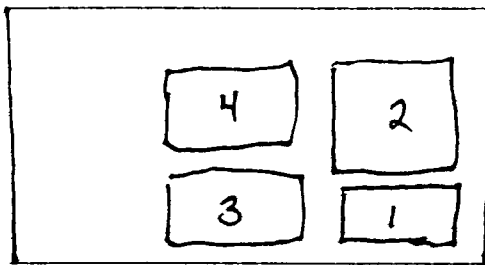
Additional Comments:

Test Start Sequence:

① Turned off fan, ② opened primary air control wide open, ③ opened door, ④ loaded test fuel into stove, ⑤ photo, ⑥ closed door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Front of stove view
4 X 4's: 2
2 X 4's: 1, 3 & 4
Loading Sequence: 1, 2, 3 & 4
Driest Pcs in Load 3

Loaded the test fuel charge on an essentially level, medium-large sized, hot coal bed (in appearance, color and temperature for a low burn rate).

Ignition 0:30. Vertical Column with secondaries igniting at 1:30. Front tube igniting 2:38. Good start.

5:00 Flames decreased after shut down. Vertical Column of flame (VC) on left side of left stack. Flickers in center canyon. VC w/ 2^{nds} on top
6:20. Steady VC in middle canyon 8:00 Back in balance. once fire was back in balance, balance slowly got better.
15:00 Gas balance 20:1.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: SCOTT KUWA HT-1
Run: 1
Date: 8/28/96
Technician: ATH, RLS.
WST1-Form7-Rev11/89

Room Temperature: 72 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture
Uncor Values are corrected for temperature: Yes No
Time Test Fuel Moisture Readings taken at: 1050
Calibration Checks: X Y 12.5 12.4 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4	K	7.5	7.9	8.0	8.4	8.0	8.4	8.233
2									
3									
4									
5	2x4x8'	P	19.0	20.3	21.0	22.6	18.0	19.2	20.700
6	"	P	18.0	19.2	18.0	19.2	18.0	19.2	19.200
7	"	P	18.0	19.2	18.5	19.8	18.0	19.2	19.400
8		P	18.5	19.8	18.0	19.2	18.0	19.2	19.400
9									78.700
10									
11									
12	2x4x14 1/2	T	20.0	21.4	20.0	21.4	20.0	21.4	21.400
13	"	T	22.5	24.3	21.5	23.1	21.0	22.6	23.333
14	"	T	18.5	19.8	18.5	19.8	18.0	19.2	19.600
15									
16	4x4x14 1/2	T	22.5	24.3	22.5	24.3	22.5	24.3	24.300
17									88.633
18									
19	FEET	T	18.0	19.2	18.0	19.2	18.5	19.8	19.400
20									OUT SPACERS

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.233%	19.675%	22.158%
% Moisture - Wet Basis:	7.607%	16.440%	18.139%

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: SCOTT KUMA HT-1
Run#: _____
Date: 8/28/96
Technician: ATH, RLS.
WST2 form 11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): in 1.575 cm 3.8481 ✓
Width (W): in 3.575 cm 8.9281 ✓
Length (L): 3.560 cm
3.568 cm
3.508 cm
3.517 cm
Length \bar{X} = in 3.53825 cm 8.9872 ✓
Volume: 308.765 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 73 °F Correction Factor: 0

Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	
Top:	<u>19.5</u>	<u>20.9</u> %	Avg % Moisture (Dry) <u>21.233</u> % ✓
Bottom:	<u>20.0</u>	<u>21.4</u> %	Aug % Moisture (Wet) <u>17.514</u> % ✓
Side:	<u>20.0</u>	<u>21.4</u> %	Scale: Levelled In <input checked="" type="checkbox"/> Out <input checked="" type="checkbox"/>
\bar{X} :		<u>21.233</u> % ✓	Zeroed: In <input checked="" type="checkbox"/> Out <input checked="" type="checkbox"/>

Wet Weight: 187.1 g Dry Weight: 160.4 g

% Moisture Dried Basis: 14.270 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

	Date	Time	Temp
Into Dryer	<u>8/28/96</u>	<u>1012</u>	<u>215</u> °F
Out of Dryer	<u>9/6/96</u>	<u>1715</u>	<u>220</u> °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 160.4 g ÷ 308.765 cm³ = .5195 g/cm³ ✓
(dry wt) (volume)

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.
% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

BURN AND FLUE GAS DATA
WOODSLOVE DATA SHEET #12
WST2-Form 14 Rev 1/88

Operator: SCOTT KUMA HT-1
Technician(s): ATH, R.S.
Date: 8/28/96
Page: 2 of 2

Minute Time	Scale Wt	lbs left	Burn Rate	1		2		3		T/C(1)T/C(2)		T/C(3)		SO2 v.	Stack	Static Press.	Comments
				CO2 v.	%CO2	CO2 v.	%CO2	CO v.	%CO	Wet Bulb	Dry Bulb	% H2O	Calc W/B				
120	436.6	1.5	.2	3.14	7.83	48.5	12.1	0.92	8.5	97	106	5.4	112		0.37		Flow
125	436.5	1.4	.1	3.24	8.07	47.7	11.9	0.89	9.1	97	106	5.4	112		0.36		SO2 1.5
130	436.4	1.3	.1	2.88	7.18	49.8	12.4	1.40	5.1	95	103	5.2	111		0.35		SO2 1.5
135	436.3	1.2	.1	2.66	6.64	51.7	12.9	1.57	4.2	92	99	4.6	108		0.34		SO2 1.5
140	436.2	1.1	.1	2.73	6.81	50.7	12.6	1.61	4.2	91	98	4.6	107		0.33		SO2 1.5
145	436.1	1.0	.1	2.72	6.79	50.9	12.7	1.61	4.2	90	97	4.5	107		0.32		
150	436.0	.9	.1	2.66	6.64	51.5	12.8	1.62	4.1	88	97	4.2	106		0.31		
155	435.9	.8	.1	2.83	7.06	49.7	12.4	1.52	4.6	87	99	3.9	105		0.30		
160	435.9	.8	0	2.75	6.86	50.9	12.7	1.56	4.4	86	100	3.6	103		0.29		
165	435.8	.7	.1	2.80	6.99	50.1	12.5	1.62	4.3	85	99	3.5	103		0.28		
170	435.7	.6	.1	2.72	6.79	51.0	12.7	1.65	4.1	85	100	3.5	103		0.28		
175	435.7	.6	0	2.62	6.54	53.2	13.3	1.46	4.5	85	100	3.5	103		0.27		
180	435.6	.5	.1	2.44	6.10	54.4	13.6							<u>2503</u>	<u>1.380</u>		Flow
185	435.5	.4	.1	2.43	6.07	54.1	13.5	1.41	4.3	85	100	3.5	102		0.27		SO2 1.5
190	435.5	.4	0	2.37	5.92	54.6	13.6	1.54	3.9	85	100	3.5	102		0.27		SO2 1.5
195	435.4	.3	.1	2.33	5.58	56.6	14.1	1.67	3.5	85	100	3.5	102		0.26		SO2 1.5
200	435.3	.2	.1	2.27	5.68	56.1	14.0	1.64	3.4	85	100	3.5	102		0.26		
205	435.3	.2	0	2.25	5.63	56.0	14.0	1.59	3.6	85	100	3.5	101		0.26		
210	435.2	.1	.1	2.27	5.68	55.7	13.9	1.57	3.6	85	100	3.5	101		0.26		
215	435.2	.1	0	2.27	5.68	56.0	14.0	1.64	3.5	85	99	3.5	101		0.25		
220	435.1	0	.1	2.27	5.68	56.0	14.0	1.61	3.5	85	99	3.5	101		0.25		
225	435.1	0	.1	2.28	5.70	56.0	14.0	1.63	3.5	84	99	3.4	100		0.24		
230														<u>1668</u>	<u>1.232</u>		
235											<u>45</u>			<u>1176</u>	<u>1.891</u>		
240														<u>260</u>	<u>1.042</u>		

TEMPERATURES
RECORD SHEET #14
WST2-Form14 Rev7/96

Un) SCOTT KUMA HT-1 Date: 8/28/96
Ru. Technician(s): ATK, RL
Page: 1 of 2

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con-	dar
0	376	479	147	444	450	930	823	80	96	248	36	78	35		
5	455	464	205	433	441	793	825	81	106	248	36	78	35		
10	515	456	224	425	444	749	793	81	100	248	36	77	36		
5	624	445	238	411	434	775	864	81	107	248	36	77	36		
20	675	439	243	403	428	833	999	80	103	248	36	78	36		
35	708	437	245	396	423	876	1144	81	104	248	36	78	35		
50	712	440	247	394	417	919	1246	81	104	248	36	78	36		
55	722	457	192	402	412	914	1233	81	104	248	36	78	35		
40	718	470	159	407	407	914	1279	81	104	248	36	78	35		
45	713	476	148	412	407	918	1296	81	103	248	36	78	35		
50	672	478	143	416	398	933	1326	81	107	248	36	78	35		
55	618	478	141	417	399	955	1286	81	101	247	36	78	36		
60	575	479	140	415	398	969	1274	82	100	247	36	79	36		
65	507	479	139	411	398	988	1217	82	99	248	36	79	36		
70	505	481	139	409	398	985	1157	82	99	248	36	78	36		
75	493	479	139	405	401	969	1127	82	98	248	36	78	36		
80	471	477	139	402	402	954	1059	81	94	248	36	78	36		
85	435	476	139	397	403	959	1026	82	97	247	36	78	36		
90	428	475	138	391	405	956	1007	82	97	247	37	78	36		
95	421	474	139	388	406	929	986	82	97	247	37	78	37		
100	413	473	139	386	406	906	979	82	97	247	37	78	36		
05	404	472	141	386	406	894	985	82	97	248	37	78	36		
10	388	468	142	386	405	869	954	83	96	248	37	78	36		
15	380	465	143	385	405	850	936	83	96	248	37	78	37		
20	3590	5698	1677	476	4833	11228	13702	985							
25	12,898	11,217	4009	9721	9888	21,717	25,786	1955							

TEMPERATURES
RECORD SHEET #14
WST2-Form14 Rev7/96

U# SCOTT KUMA HT-1 Date: 8/28/96
Ru. Technician(s): ATY, EA
Page: 2 of 2

T/C#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute/Time	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn Catalytic	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
120	374	460	145	385	404	830	965	83	95	248	37	78	37		
125	391	455	144	383	404	831	1062	83	95	248	37	78	37		
130	368	450	145	386	404	820	876	83	95	248	37	78	37		
135	357	445	146	386	405	804	846	83	95	248	37	78	37		
140	338	440	146	386	406	797	838	84	93	248	37	78	37		
145	329	437	146	386	407	796	832	83	94	248	37	78	37		
150	322	432	146	385	409	786	821	83	94	248	37	78	37		
155	317	429	146	384	410	766	807	83	94	248	37	78	37		
160	312	425	147	383	412	766	801	84	93	248	37	78	37		
165	309	422	147	383	414	753	795	84	93	248	37	78	37		
170	307	419	147	381	416	756	787	84	93	248	37	78	37		
175	304	416	146	381	417	725	782	84	93	248	37	78	38		
180	299	411	146	378	419	723	774	84	93	248	37	79	38		
185	296	407	145	375	420	718	774	84	93	248	37	79	38		
190	293	402	145	371	421	707	784	84	93	248	37	79	38		
195	289	395	144	363	420	692	802	84	93	248	38	79	38		
200	287	393	143	360	418	680	764	84	93	248	39	79	38		
205	284	389	142	355	415	678	757	84	93	248	39	79	38		
210	280	386	141	352	412	673	748	84	93	248	39	79	38		
215	276	383	140	347	408	673	756	84	93	248	39	79	38		
220	274	381	140	343	404	658	720	84	92	248	39	79	38		
225	2578	3547	1286	3244	3737	6202	6879	756	92	248	39	79	38		
230	25	25	25	25	25	25	25	25	25	25	25	25	25		
235	19478	19994	7046	17574	18533	37349	42879	3712	45	START	379.2	379.2	379.2		
240	433	444	157	391	412	830	953	82		FINISH	308.4	308.4	308.4		
245										ΔT=	-70.8	-70.8	-70.8		

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 8/28/96 Analyte: CO₂

Source: SCOTT KUMA HT-1 Run #: 1

Zero Cyl #: 4-36919 Conc. 00.0 % CO₂ Cyl Press: 2025 psi

Certified by: Air Gas Date: 4/24/96

Span Cyl #: W260657 Conc. 10.1 % CO₂ Cyl Press: 975 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: A.T. Myren Time: 1045 Temp: 72 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	.000	.000	.0666	.0666	+0.27
Span	40.4	.404	10.1	40.5	.404	10.051	-.0489	-0.48

Comments:

Post Run Audit: By: A.T. Myren Time: 1655 Temp: 83 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	+0.27
Span	40.4	.404	10.1	40.5	.406	10.1006	.0006	+0.01

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 8/28/96 Analyte: O₂

Source: SCOTT KUMA HT-1 Run #: 1

Zero Cyl #: 4-36919 Conc. 00.0 % O₂ Cyl Press: 2025 psi

Certified by: Aie Gas Date: 4/24/96

Span Cyl #: W260657 Conc. 12.5 % O₂ Cyl Press: 975 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH, Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂
EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: A.T. Myren Time: 1045 Temp: 72 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	00.054	0.0054	+0.02
Span	12.5	50.0	12.5	12.5	50.0	12.467	-0.0326	-0.26

Comments:

Post Run Audit: By: A.T. Myren Time: 1655 Temp.: 83 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.0	00.054	0.0054	+0.02
Span	12.5	50.0	12.5	12.5	50.0	12.467	-0.0326	-0.26

Comments:

± Conc. Difference = Act % - Exp (Std) %
 Zero % Differece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 8/28/96 Analyte: CO

Source: SCOTT KUMA HT-1 Run #: 1

Zero Cyl #: 4-36919 Conc. 00.0 % CO Cyl Press: 2025 psi

Certified by: AirGas Date: 4/24/96

Span Cyl #: W 260657 Conc. 2.47 % CO Cyl Press: 975 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 1045 Temp: 72 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.3	00.62	-0.062	-0.12
Span	2.47	49.4	2.47	2.47	49.0	2.376	-0.0938	-3.80

Comments:

Post Run Audit: By: A.T. Myren Time: 1655 Temp.: 83 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	00.0	00.3	00.62	-0.062	-0.12
Span	2.47	49.4	2.47	2.48	49.5	2400	-0.0696	-2.82

Comments:

+ Conc. Difference = Act % - Exp (Std) %
 Zero % Differece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: SCOTT KUMA HT-1
 Run: _____
 Date: 8/28/96
 Technicians: ATM, PLS.
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 71 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 73.4 °F; T/C#2: 73.0 °F;
 T/C #3: 73.0 °F; T/C #4: 73.0 °F; T/C #5: 73.4 °F;
 T/C #6: 73.6 °F; T/C #7: 73.6 °F; T/C #8: 73.8 °F;
 T/C #9: 74.4 °F; T/C #10: 74.4 °F; T/C #11: 70.8 °F;
 T/C #12: 72.4 °F; T/C #13: 72.2 °F; T/C #14: 72.2 °F;
 T/C #15: 72.2 °F; T/C #16: 72.2 °F; T/C #17: _____ °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: _____

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : -0.2 °F Adj to: 0.0 °F Post Test Check Zero (0°F): 0.2 °F % Difference +0.01
 Span (2000°F): 2000.6 °F Adj to: 2000.0 °F Span (2000°F): 2000.6 °F +0.03

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check
 0°F = 0.0 °F; 200°F = 201.6 °F; 400°F = 398.8 °F;
 600°F = 601.2 °F; 800°F = 800.8 °F; 1000°F = 1000.6 °F;
 1200°F = 1198.6 °F; 1400°F = 1399.2 °F; 1600°F = 1599.0 °F
 1800°F = 1799.6 °F; 2000°F = 2000.0 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre OK Post OK
 Draft (Static) Gauge Zero Check: Pre OK Post OK

Scale Check Pre (Wt, #'s): 433.3 - 438.3 5.0 lbs. OK (PLS.)
 Post (Wt, #'s): 434.8 - 439.8 5.0 lbs. OK (PLS.)

Stack cleaned prior to the run: Yes No _____
 Tunnel cleaned prior to the run: Yes No _____

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS
3/31/96

File Name: CKUMAR3

Stove Manufacturer: KUMA

Model Number: SCOTT HT-1

Lab Name: MYREN

Test Date: 9/5/96

Run Number: 3

Meter Box Y Factor: 1.012

Barometric pressure (in): 29.92

Gas meter temp (ave): 98

delta H(ave): 0.884

Gas meter initial reading: 913.404

Gas meter final reading: 982.885

Front catch (acetone) mg: 4.0

first filter catch (mg): 11.0

second filter catch (mg): -0.9

tunnel flow (ave cfm): 139.63

Emission Rate(g/hr): 1.795

Emission Rate(M5H) : 2.958

vs/VmTs: 0.02

vs ave: 789.53

Tunnel average temp (°f): 102.40

Test time(min): 140

Fuel Load(lb. wet): 10.9

Wood moisture(%wet): 17.915

Burn rate(dry kg/hr): 1.739

Samp vol(scf): 66.423

front filter number: 133

back filter number: 132

acetone beaker number: 3

PRELIMINARY RESULTS

FINAL RESULTS

DATA SUMMARY

MODEL: SCOTT HT-1

RUN: 3

DATE: 9/5/96

DBR: 1.739

GPH UNADJ: 1.795

ADJ: 2.958

RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.036	100	913.404	74	0.900	779.99		
10	0.037	112	918.365	78	0.900	799.17	107.1	4.936
20	0.038	114	923.465	84	0.880	811.32	106.6	5.018
30	0.036	116	928.280	91	0.870	791.05	98.3	4.677
40	0.036	113	933.170	96	0.870	788.99	100.9	4.708
50	0.037	109	938.090	99	0.870	797.07	100.5	4.711
60	0.038	106	943.020	102	0.880	805.64	98.7	4.696
70	0.038	101	948.005	102	0.880	802.08	97.8	4.748
80	0.037	99	952.910	105	0.890	790.04	95.8	4.647
90	0.036	97	957.875	107	0.890	777.89	97.8	4.687
100	0.036	94	962.822	106	0.890	775.80	98.6	4.679
110	0.037	95	967.860	106	0.890	787.21	100.9	4.765
120	0.037	94	972.865	108	0.890	786.50	98.6	4.733
130	0.036	93	977.845	109	0.880	775.10	97.5	4.685
140	0.036	93	982.885	110	0.880	775.10	99.9	4.733
150						0.00	0.0	0.000
160						0.00	0.0	0.000
170						0.00	0.0	0.000
180						0.00	0.0	0.000
190						0.00	0.0	0.000
200						0.00	0.0	0.000
210						0.00	0.0	0.000
220						0.00	0.0	0.000
230						0.00	0.0	0.000
240						0.00	0.0	0.000
250						0.00	0.0	0.000
260						0.00	0.0	0.000
270						0.00	0.0	0.000
280						0.00	0.0	0.000
290						0.00	0.0	0.000
300						0.00	0.0	0.000
310						0.00	0.0	0.000
320						0.00	0.0	0.000
330						0.00	0.0	0.000
340						0.00	0.0	0.000
350						0.00	0.0	0.000

DATE 9/5/96

PAGE 1 OF 1

MODEL # Scott HT-1

RUN # 3

METER BOX # 45G-P

METER Y 1.012

FILTER # (F) 133 (R) 132

PRE TEST LEAK RATE = .000 CFM @ -17.0 IN. HG

FILTER SIZE: 110 mm

POST TEST LEAK RATE = .000 CFM @ -16.0 IN. HG

PROBE LENGTH 24" glass

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1240	00	913.404	-036	100	74	0.90	0	N-1	0.5"	-029	105
50	10	918.365	-037	112	78	.90	0	2	1.5"	-042	105
1300	20	923.465	-038	114	84	.88	0	3	4.5"	-042	104
10	30	928.280	-036	116	91	.87	0	4	5.5"	-032	104
20	40	933.170	-036	113	96	.87	0	W-1	0.5"	-035	103
30	50	938.090	-037	109	99	.87	0	2	1.5"	-041	102
40	60	943.020	-038	106	102	.88	0	3	4.5"	-041	102
50	70	948.005	-038	101	102	.88	0	4	5.5"	-026	101
1400	80	952.910	-037	99	105	.89	0	Avg. 0360 10225			
10	90	957.875	-036	97	107	.89	0	563.25			
20	100	962.822	-036	94	106	.89	0	Pilot Leak Check			
30	10	967.860	-037	95	106	.89	0	Pre ok Post ok			
40	20	972.865	-037	94	108	.89	0	Cp = 0.99			
50	30	977.845	-036	93	109	.88	0	N 1 2 3 4			
1500	40	982.885	-036	93	110	.88	0	→ W 1 2 3 4			
	50							3 4			
	60							↑			
	70							* = point of Avg. delta p			
	80							Qs = (√(ΔP x BP)) x 3167.2 =			
	90							N 138,502 cfm			

10.9 lbs
17.915 %
140 min

Ace 1.2
E 11.7
R 0

BP = Street 29.92 in Hg
60 min 29.92
120 min 29.92

EW 29.92
X = 29.92

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

4th Round

Into Dessicator: Date: 6/27/96 Time: 1200 By: A.T./M...

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4824	8/8/96	1446	ATM	65.4819	8/9/96	1125	RLS				
2	66.1488	7/25/96	1217	RLS	66.1484	8/1/96	0958	ATM				
3	67.8548	8/8/96	1553	ATM	67.8542	8/9/96	1103	RLS	67.8544	8/14/96	11130	ATM
4	67.5870	8/8/96	14124	ATM	67.5865	8/9/96	1130	RLS	KUMA	#1		
5	67.2054	8/8/96	1618	ATM	67.2050	8/9/96	1058	RLS	KUMIA	5		
6	67.4250	7/3/96	1403	RLS	67.4241	7/10/96	1059	ATM	67.4250	7/25/96	1155	RLS
7	65.5422	8/8/96	1533	ATM	65.5423	8/9/96	1110	RLS	KUMA	4		
8	66.0183	7/10/96	1100	ATM	66.0187	7/25/96	1055	RLS				
9	66.9280	7/8/96	1312	ATM	66.9276	8/9/96	1120	RLS	KUMA	#2		
10	66.0862	7/10/96	1111	ATM	66.0860	7/25/96	0933	RLS				
11	65.6989	7/10/96	1108	ATM	65.6989	7/25/96	1020	RLS				
12	Broken											

KUMA 3
KUMA 3
BLANK 8/8/96

Checked By: _____ Date: _____ Time: _____

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	ZRH	Date	Time	By
58	70	47	7/3/96	0953	ATM
60	72	49	7/10/96	1026	ATM
57.5	69	48	8/1/96	0948	ATM

66 29 49 8/8/96 1235 ATM
60 72 49 8/9/96 0945 ATM
64 72 49 8/14/96 1116 ATM

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Scale Mc H/ce
Model AE 100
SN KO4027

Dates From 6/20/96

Through 9/10/96

TROEMNER CLASS 5 WTS.

100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Tech	Date	Time	Dry Bulb	Wet Bulb	% RH
100.0003	10.0000	1.0000	.1000	.0199	R/S	6/20/96	1625	61	74	47
100.0005	10.0000	1.0000	.1000	.0200	ATM	6/21/96	1259	61	74	47
99.9997	10.0001	1.0001	.1000	.0200	ATM	6/25/96	1410	63	76	48
99.9996	10.0000	1.0000	.1000	.0201	ATM	6/26/96	1558	64	78	48
99.9998	10.0000	1.0000	.1000	.0201	ATM	6/27/96	1718	65	78	49
100.0001	10.0000	1.0000	.1000	.0200	ATM	6/28/96	1254	58	70	49
100.0000	10.0000	1.0000	.1000	.0200	ATM	7/1/96	1504	65	78	49
99.9997	10.0001	1.0001	.1000	.0200	ATM	7/2/96	1816	64	77	49
99.9998	10.0000	1.0000	.1000	.0200	ATM	7/3/96	953	58	70	49
99.9999	10.0000	1.0000	.1000	.0201	ATM	7/3/96	1727	57	83	49
99.9996	10.0000	1.0000	.1000	.0200	ATM	7/9/96	1456	90 RH To high		49
99.9998	10.0000	1.0000	.1000	.0201	ATM	7/10/96	1006	60	78	49
99.9997	10.0000	1.0000	.1000	.0200	ATM	7/11/96	0918	59	71	48
99.9998	10.0000	1.0000	.1000	.0200	ATM	7/12/96	842	59	71	48
100.0000	10.0001	1.0001	.1001	.0201	ATM	7/16/96	1233	62	75	49
100.0003	10.0003	1.0003	.1003	.0202	ATM	7/17/96	1605	63	74	54
99.9996	9.9998	9.9998	.9998	.0198	ATM	7/18/96	0733	68	56	49
99.9999	10.0000	1.0000	.1000	.0200	ATM	7/19/96	0740	71	59	48
99.9999	10.0000	1.0000	.1000	.0200	ATM	7/20/96	1445	82	68	48
99.9997	10.0001	1.0001	.1001	.0201	ATM	7/23/96	1513	80	66	47
99.9996	10.0000	1.0000	.1000	.0200	ATM	7/24/96	0757	59	71	48
99.9999	10.0000	1.0000	.1000	.0201	ATM	7/24/96	1617	71	86	49
100.0002	10.0001	1.0001	.1001	.0201	ATM	7/25/96	0847	67	73	49
99.9995	10.0000	1.0000	.1000	.0201	ATM	7/31/96	2035	65	79	47
100.0000	10.0000	1.0000	.1000	.0202	ATM	8/1/96	0705	69	57.5	48
100.0000	10.0001	1.0001	.1001	.0202	ATM	8/1/96	1450	60	72	49
99.9998	10.0000	1.0000	.1000	.0202	ATM	8/2/96	801	59	71	49
100.0001	10.0000	1.0000	.1000	.0199	ATM	8/13/96	1235	66	79	49
99.9996	10.0000	1.0000	.1000	.0201	ATM	8/19/96	0754	60	72	49
100.0003	10.0000	1.0000	.1000	.0200	ATM	8/19/96	1176	64	77	49
99.9999	10.0001	1.0001	.1001	.0201	ATM	8/15/96	1408	66	79	49
100.0002	10.0000	1.0000	.1000	.0201	ATM	8/28/96	1611	70	85	49
99.9997	10.0000	1.0000	.1000	.0200	ATM	8/29/96	1008	64	77	49
99.9996	10.0000	1.0000	.1000	.0200	ATM	8/30/96	1005	61	73	48
99.9997	10.0000	1.0000	.1000	.0200	ATM	9/5/96	0954	59	71	48
99.9996	10.0000	1.0000	.1000	.0200	ATM	9/6/96	1030	72	80	49
100.0000	10.0000	1.0000	.1000	.0200	ATM	9/9/96	1806	76	83	48
100.0005	10.0002	1.0002	.1002	.0200	ATM	9/10/96	1736	77	84	48

Unit: Kuma Scott HT-1
 Run: 3
 Date: 9/5/96
 Technicians: ATM DLS
 WST20, Form 5

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 EPA M5G-1

Filters

Filter # 132 (R) Beaker # 3 Final Wt. 67.8585 g ✓
 Final Wt .7362 g ✓ Ml 53 Tare Wt. 67.8544 g ✓
 Tare Wt .7371 g ✓ Desc. Acetone Net Wt. .0041 g ✓
 Net Wt -.0009 g ✓

Filter # 133 (F) Beaker # _____ Final Wt. _____ g
 Final Wt .7479 g ✓ Ml _____ Tare Wt. _____ g
 Tare Wt .7369 g ✓ Desc. _____ Net Wt. _____ g
 Net Wt .0110 g ✓

Acetone Blank Calculation: Blank done 8/8/96
 Blank Beaker # 6 Final Wt 67.4251 g.
 Ml 140 Tare Wt 67.4250 g.
 Desc Acetone Net Wt .0001 g.
.0001 g ÷ 140 ml = .0000007 g/ml

Particulate Catch Calculation

Filter: .0110 g ✓
 Filter: -.0009 g ✓
 Beakers: .0041 - (.000001)(53) = .0040 g ✓
 Total Catch MI of Acetone
 Blank Value/MI of Acetone
 Total Catch = .0141 g ✓

Unit KUMA SCOTT HI-1
 Run # 3
 Date 9/5/96
 Technician ATM, RLS
 WST6-Form1, Rev8/96

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 1.716 ft³

Dilution Tunnel Draft (If applicable): Start 0 Stop 0

Test Chamber Air Velocity: Start: 0 Stop: 0 Avg: 0

Wet Bulb/ Start: WB: 63 °F DB: 74 °F 1.65 % Amb Moisture 54 %RH

Dry Bulb Stop: WB: 64 °F DB: 75 °F 1.60 % Amb Moisture 55 %RH

$\bar{X} = 1.625$ % Ambient Moisture $\bar{X} = 54.5$ % Relative Humidity (RH)

Empty Stove Wt: 343.1 lbs.

Stove Wt with Stack (Inc. Oil Seal) Wet: 433.2 lbs. Dry: 432.8 lbs.

Empty Stove Wt with Stack and Ash Ash: lbs. Total: lbs.

Kindling Wt. Paper: 0.3 lbs. Wood: 4.0 lbs.

Pre Burn Fuel Wt. 11.2 + 12.0 + 11.7 Total: 34.9 lbs.

Total Kindling and Pre Burn Fuel Wt 39.2 lbs.

Coal Bed Wt-lbs: Range (2.7 - 2.2) 435.5 - 435.0 lbs. Actual: 2.5 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range $\frac{435.5}{\text{Upper Wt.}} + \frac{435.0}{\text{Lower Wt.}} \cdot 12 \cdot .25 = \underline{0.6}$ lbs.

Test Fuel Wt-lbs: Ideal 12.0 lbs. Range: 10.9 - 13.2 lbs. Actual: 10.9 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 14 Pcs.

2 x 4's x 14.5/16 " 3 Pcs 6.9 lbs. 63.3 %

4 x 4's x 14.5/16 " 1 Pcs 4.0 lbs. 36.7 %

Est. Dry Burn Rate (Kg/Hr.) $\frac{10.9}{2.2046} - \frac{(10.9 \times 1.7915)}{140} \times \frac{60}{140} = \underline{1.739}$ Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO_E) (19,140) x $\frac{63}{100} \times \frac{1.739}{1} = \underline{20,973}$ Est Heat Output (HO_E) BTU's/Hr

Comments:

STOVE OPERATING DATA
WOODSTOVE TEST DATA SHEET #9

Unit: Kuma Scott HT-1
Run: 3
Date: 9/5/96
Technician(s): ATM RLS
WST3-Form 1 Rev 9/90

Fire Started: 0845 PDST

Warm up and Preburn: Primary Air: Wide open from ignition until the start of the preburn when the primary air control(s) was (were) adjusted to the run setting of $\frac{3}{4}$ " open on arc. At the run setting until the start of the test.

Secondary Air: No Controls, Naturally Drafted.

Secondary Burn/Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge.

Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 25 seconds.

Test: Door Wide Open during loading _____ min 25 sec, then closed.

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of $\frac{3}{4}$ " open on arc between 4:55 and 5:00. At the run setting of $\frac{3}{4}$ " open on arc at 5:00 into the run.

Secondary Air:
No Controls, Naturally Drafted.

Secondary Burn/Bypass: N/A

Fan: off during the warm up. On high during the preburn. Off at the start of the test. Off for the first 30 minutes of the test. On high at 30 minutes into the test. On high
Test Run Anomalies: for the rest of the test.

Unit KUMA Soft HT-1
 Run # 3
 Date 9/5/96
 Technician ATM, RLS
 Page 1 of 3
 WST7-Form2-A, Rev10/88

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4x8'</u>	<u>R.I.B. LUMBER</u>	<u>STD. & BTR</u>	<u>D. Fir, S. Gen.</u>
Test Fuel	<u>2x4x8'</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR</u>	<u>D. Fir, S. Gen.</u>
	<u>4x4x8'</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR</u>	<u>D. Fir, S. Gen.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (11.2 lbs) added at 0858.
 2nd Warm up/Pre Burn Fuel charge (12.0 lbs) added at 1005.
 3rd Warm up/Pre Burn Fuel charge (11.7 lbs) added at 1115.
 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3 RD pre burn/warm up fuel charge. The stove lost 0.4 lbs.

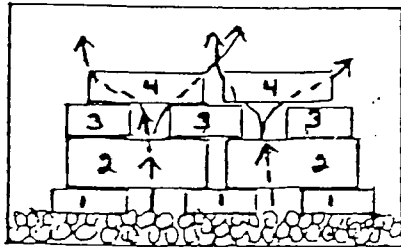
All pre burn/warm up fuel pieces were either 14" or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 14 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 14 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 14 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

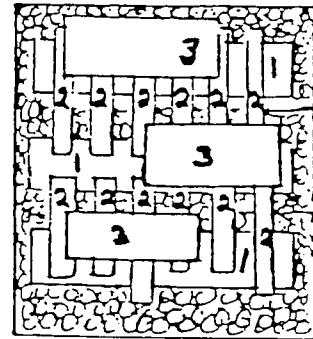
Unit KUNIA ST# 47-1
Run # 3
Date 9/5/96
Technician ATM, RLS
Page 2 of 3
WST7-Form2-A, Rev 6/90

Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP surface temperature(s) and the peak value(s) obtained were 975 OF.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

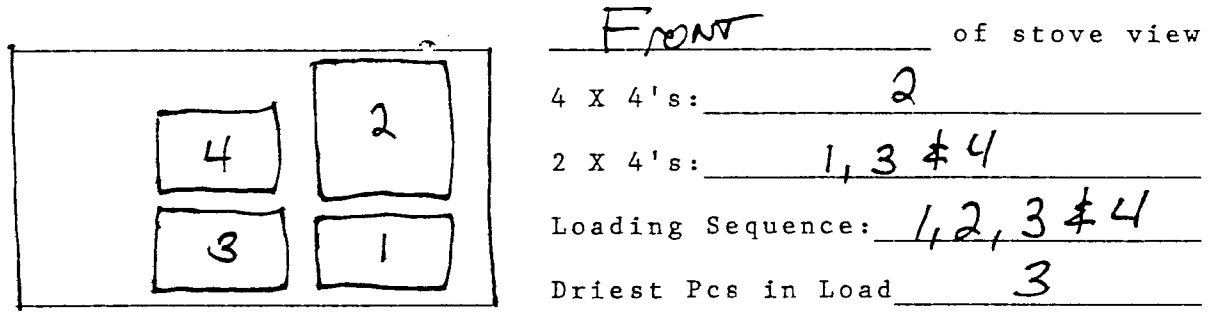
The primary air was adjusted to the run setting of 3/4" open on arc 4.7 lbs above the upper charcoal bed weight.

Additional Comments:

Test Start Sequence: ① turned fan off,
② opened primary air control wide open, ③ opened door,
④ loaded test fuel charge into the stove, ⑤ Photo,
⑥ closed the door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Loaded the test fuel charge on an essentially level, large to medium sized, average to hot coal bed (in appearance, color and temperature for a medium high burn rate. Load 0:25. Ignition 0:30. Vertical column to baffle 1:50. Secondaries began to ignite at 2:30. Secondaries full width of stove at 3:45. Front Tube igniting @ 4:30. 5:00 after primary air control adjusted to run setting. Flames decreased slightly. Maintained Vertical column of flame (VCF) to baffle L, C and R Hot Coals under pcs 3 & 1. Seconds the Full width of stove under baffle " off Front & Middle tubes.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: KEUMA SCOTT HT-1
Run: 3
Date: 9/5/96
Technician: ATH, RLS.
WST1-Form7-Rev11/89

Room Temperature: 71 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture
Uncor Values are corrected for temperature: Yes No
Time Test Fuel Moisture Readings taken at: 1055
Calibration Checks: X Y 12.5 12.4 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4	K	8.0	8.4	8.5	8.9	8.0	8.4	8.567
2									
3									
4									
5	2x4x8'	P	18.0	19.2	18.5	19.8	18.0	19.2	19.400
6	"	P	18.0	19.2	18.0	19.2	18.0	19.2	19.200
7	"	P	18.5	19.8	18.5	19.8	18.0	19.2	19.600
8									58.200
9									
10									
11	2x4x14 5/16"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
12	"	T	21.0	22.6	21.0	22.6	20.5	22.0	22.400
13	"	T	21.5	23.1	21.5	23.1	20.5	22.0	22.733
14									
15	4x4x14 5/16"	T	22.0	23.7	21.0	22.6	21.0	22.6	22.967
16									87.300
17									
18									
19	FEET	T	18.5	19.8	18.0	19.2	18.0	19.2	19.400
20									OUT SPACERS

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.567%	19.400%	21.825%
% Moisture - Wet Basis:	7.891%	16.248%	17.915%

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: KUMM SCOTT HT-1
Run#: 3
Date: 9/5/96
Technician: ATM, RLS
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): IN. 1.523 cm 3.8684 ✓
Width (W): IN. 3.534 cm 8.9764 ✓
Length (L): 3.570 cm
3.490 cm
3.533 cm
3.505 cm
Length \bar{X} = IN. 3.570 ✓ cm 8.9154 ✓
Volume: 309.581 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature? 71 °F Correction Factor: 0

Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	<u>19.0</u>	<u>20.3</u>	<u>20.3</u>
Bottom:	<u>19.0</u>	<u>20.3</u>	<u>20.3</u>
Side:	<u>19.5</u>	<u>20.9</u>	<u>20.9</u>
\bar{X} :		<u>20.500</u>	<u>20.500</u>

Avg % Moisture (Dry) 20.500 % ✓
Avg % Moisture (Wet) 17.012 % ✓
Scale: Leveled In Out
Zeroed: In Out

Wet Weight: 170.0 g Dry Weight: 145.6 g

% Moisture Dried Basis: 14.353 % ✓
[1 - (Dry Wt ÷ Wet Wt)] X 100

Into Dryer Date 9/5/96 Time 1045 Temp 215 °F
Out of Dryer Date 9/9/96 Time 1715 Temp 220 °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 145.6 g (dry wt) ÷ 309.581 cm³ (volume) = .4703 g/cm³ ✓

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.
% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

BURN AND FLUE GAS DATA
 WOODSTOVE DATA SHEET #12
 WST2-Form 14 Rev 1/88

Technician: Kuno Scott HT-1 Date: 9/5/96
 Technician(s): ATH, JLS
 Page: 3 of 2

Minute Time	Scale Wt	lbs left	Burn Rate	CO2		O2		Tel		CO		T/C(1)T/C(2)		T/C(3)		SO2 v.	Stack	Static Press.	Comments
				v.	%CO2	v.	%O2	v.	%CO	Wet Bulb	Dry Bulb	% H2O	Calc W/B	PPM					
0	446.2	10.9	0	13.19	7.95	48.6	18.1			0.65	12.2	86	116	3.1	105		335	7.059	Flow
5	446.4	10.1	.8	13.56	3.92	65.6	16.4			0.63	6.2	88	129	3.1	120		378	7.077	SO2 1.5
10	444.6	9.3	.8	14.79	11.9	33.3	8.31			0.73	16.3	115	150	8.8	138		480	7.081	SO2 1.5
15	443.6	8.3	1.0	15.63	14.0	25.5	6.36			1.13	12.4	126	151	12.5	145		501	7.083	SO2 1.5
20	442.7	7.4	.9	15.79	14.4	24.2	6.04			0.95	15.1	130	148	14.5	148		500	7.084	SO2 1.5
25	441.8	6.5	.9	16.00	14.9	22.2	5.54			1.06	14.1	124	143	12.5	145		509	7.084	
30	441.0	5.7	.8	16.18	15.3	20.1	5.02			1.07	14.3	119	139	10.0	142		570	7.084	
35	440.2	4.9	.8	15.95	14.8	22.4	5.59			0.82	18.0	114	132	9.0	139		506	7.083	
40	439.5	4.2	.7	16.01	14.9	21.5	5.36			0.57	22.3	108	126	7.5	136		494	7.082	
45	438.9	3.6	.6	15.64	14.0	25.9	6.46			0.16	87.5	103	121	7.0	134		480	7.080	
50	438.4	3.1	.5	15.72	12.7	31.8	7.93			0.10	127.2	98	114	5.8	131		449	7.076	
55	438.0	2.7	.4	15.03	12.5	31.7	7.91			0.08	156.2	95	111	4.9	128		432	7.074	Flow
60	437.5	2.2	.5	14.67	11.6	35.5	8.85										557.4	7.077	SO2 1.5
65	437.2	1.9	.3	14.42	11.0	37.7	9.40			0.12	96.7	92	108	4.4	126		418	7.072	SO2 1.5
70	437.0	1.7	.2	13.90	9.71	42.9	10.7			0.20	55.0	90	105	4.2	122		400	7.070	SO2 1.5
75	436.7	1.4	.3	13.39	8.44	47.8	11.9			0.22	44.1	88	100	4.1	123		389	7.066	SO2 1.5
80	436.6	1.3	.1	13.29	8.20	48.3	12.0			0.34	24.8	86	96	3.8	121		365	7.064	SO2 1.5
85	436.5	1.2	.1	12.87	7.16	52.3	13.0			0.42	19.5	84	92	3.7	119		357	7.062	
90	436.3	1.0	.2	12.42	6.05	56.4	14.1			0.48	14.9	83	91	3.7	117		342	7.060	
95	436.2	.9	.1	12.39	5.97	55.8	13.9			0.90	6.7	82	88	3.5	115		327	7.057	
100	436.1	.8	.1	12.34	5.85	56.4	14.1			0.97	6.2	81	86	3.4	114		311	7.055	
105	436.0	.7	.1	12.31	5.78	56.6	14.1			1.03	5.7	80	84	3.3	112		300	7.053	
110	435.9	.6	.1	12.29	5.73	56.7	14.1			1.07	5.4	80	84	3.3	111		295	7.051	
115	435.8	.5	.1	12.35	5.87	55.9	13.9			1.23	4.7	81	84	3.4	112		290	7.050	
120	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
125	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
130	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
135	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
140	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
145	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
150	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
155	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
160	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
165	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
170	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
175	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
180	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
185	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
190	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
195	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
200	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
205	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
210	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
215	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
220	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
225	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
230	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
235	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
240	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
245	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
250	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
255	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
260	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
265	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
270	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
275	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
280	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
285	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
290	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
295	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
300	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
305	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
310	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
315	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
320	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
325	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
330	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
335	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
340	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
345	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
350	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
355	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
360	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
365	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
370	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
375	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
380	435.8	.5	.1	12.35	5.87	55.9	13.9			1.28	4.6	81	84	3.4	111		284	7.049	
385																			

BURN () AND FLUE GAS DATA
 WOODSTOVE DATA SHEET #12
 WST2-Form 14 Rev 1/88

Name: Kenneth Scott HT-1 Date: 9/5/96
 Technician(s): ATH ds.

Page: 3 of 2

Minute Time	Scale Wt	Ibs left	Burn Rate	CO2		O2		T/C(1)T/C(2)			T/C(3)			SO2 v.	PPM	Static Press.	Comments
				v.	%CO2	v.	%O2	Wet Bulb	Dry Bulb	% H2O	Calc W/B	Stack	SO2				
120	435.7	1.4	1.1	1.232	5.80	56.4	14.1	81	85	3.4	112	281			7.048	Flow	
125	435.6	1.3	1.1	1.226	5.65	57.0	14.2	82	86	3.5	111	278			7.048	SO2 1.5	
130	435.5	1.2	1.1	1.219	5.48	57.7	14.4	82	86	3.5	111	275			7.047	CO2 1.5	
135	435.4	1.1	1.1	1.219	5.48	58.3	14.5	82	86	3.5	110	270			7.046	O2 1.5	
140	435.3	0	1.1	1.214	5.36	58.7	14.6	82	86	3.5	110	267			7.046	CO 1.5	
145	05											1371			7.235		
150	10																
155	15											11,017			1.891		
160	20											380			7.065		
165	25																
170	30																
175	35																
180																Flow	
185																SO2 1.5	
190																CO2 1.5	
195																O2 1.5	
200																CO 1.5	
205																	
210																	
215																	
220																	
225																	
230																	
235																	

435.3

U: KUMAR Scott HT-1 Date: 9/5/96
 RL: 3 Technician(s): ATH, S,
 Page: 1 of 2

T/G#	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute Time	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar	
0	456	533	158	508	450	885	922	71	100	248	36	76	37		DGM
5	455	505	210	489	432	927	1233	72	115	248	36	76	36		
10	611	552	238	493	453	915	1214	72	112	247	35	75	35		
15	677	482	254	461	457	966	1341	71	114	248	36	76	35		
20	708	480	263	455	442	991	1361	72	114	248	36	76	35		
25	727	482	269	454	432	1022	1357	72	116	248	37	77	35		
30	741	487	273	458	428	1068	1347	73	116	248	37	77	34		
35	747	496	209	464	428	1094	1338	74	116	247	37	77	34		
40	750	522	188	492	439	1195	1334	73	113	248	37	78	34		
45	734	535	165	502	443	1143	1346	74	111	248	37	77	35		
50	694	548	140	509	447	1164	1305	73	109	248	37	77	34		
55	658	553	158	514	456	1171	1320	73	107	248	37	76	34		
60	622	557	158	519	464	1161	1308	73	106	248	37	76	34		
65	607	559	158	522	473	1133	1227	72	104	248	37	76	34		
70	583	556	160	526	475	1098	1192	72	101	247	36	75	35		
75	550	553	160	525	483	1065	1106	72	100	247	35	75	35		
80	521	546	159	522	488	1016	1075	72	99	247	35	75	34		
85	502	537	160	519	489	947	1056	72	98	247	35	75	34		
90	477	529	160	515	484	911	974	74	97	247	35	76	35		
95	444	514	159	507	491	897	961	71	96	247	35	76	35		
100	411	501	159	497	491	866	942	72	94	248	35	76	35		
105	401	496	159	492	486	857	932	72	95	248	34	76	35		
110	388	490	159	485	490	827	926	73	95	248	34	76	34		
115	377	483	160	480	480	815	924	73	95	248	35	76	35		
120	358	468	160	468	480	815	924	73	95	248	35	76	35		
125	341	453	160	453	480	815	924	73	95	248	35	76	35		
130	324	438	160	438	480	815	924	73	95	248	35	76	35		
135	307	423	160	423	480	815	924	73	95	248	35	76	35		
140	290	408	160	408	480	815	924	73	95	248	35	76	35		
145	273	393	160	393	480	815	924	73	95	248	35	76	35		
150	256	378	160	378	480	815	924	73	95	248	35	76	35		
155	239	363	160	363	480	815	924	73	95	248	35	76	35		
160	222	348	160	348	480	815	924	73	95	248	35	76	35		
165	205	333	160	333	480	815	924	73	95	248	35	76	35		
170	188	318	160	318	480	815	924	73	95	248	35	76	35		
175	171	303	160	303	480	815	924	73	95	248	35	76	35		
180	154	288	160	288	480	815	924	73	95	248	35	76	35		
185	137	273	160	273	480	815	924	73	95	248	35	76	35		
190	120	258	160	258	480	815	924	73	95	248	35	76	35		
195	103	243	160	243	480	815	924	73	95	248	35	76	35		
200	86	228	160	228	480	815	924	73	95	248	35	76	35		
205	69	213	160	213	480	815	924	73	95	248	35	76	35		
210	52	198	160	198	480	815	924	73	95	248	35	76	35		
215	35	183	160	183	480	815	924	73	95	248	35	76	35		
220	18	168	160	168	480	815	924	73	95	248	35	76	35		
225	1	153	160	153	480	815	924	73	95	248	35	76	35		

13,841 12,496 4456 11,888 11,095 24,134 28,036 1738

PRE AND. POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 4/5/96 Analyte: CO₂

Source: Kuma Scott HT-1 Run #: 3

Zero Cyl #: 4-36919 Conc. 00.0 % CO₂ Cyl Press: 1975 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260657 Conc. 10.1 % CO₂ Cyl Press: 950 psi

Certified by: B30C Gases Date: 1/18/95

Analyzer: Make: Hörriba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂
EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: A.J. Myren Time: 1045 Temp: 74 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.4	.404	10.1	40.25	.404	10.0511	-.0489	-0.48

Comments:

Post Run Audit: By: A.J. Myren Time: 1535 Temp: 80 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.4	.404	10.1	40.0	.403	10.0264	-.0736	-0.73

Comments:

± Conc. Difference = Act % - Exp (Std) %
 Zero % Differece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 9/5/96 Analyte: O₂

Source: Kuma Scott, HT-1 Run #: 3

Zero Cyl #: 4-36919 Conc. 00.0 % O₂ Cyl Press: 1975 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260657 Conc. 12.5 % O₂ Cyl Press: 950 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂
EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: A.T. Myren Time: 1045 Temp: 74 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.5	00.1	.0303	.0303	0.12
Span	12.5	50.0	12.5	12.55	50.0	12.467	-0.0826	-0.26

Comments:

Post Run Audit: By: A.T. Myren Time: 1535 Temp.: 80 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.5	00.1	.0303	.0303	0.12
Span	12.5	50.0	12.5	12.5	49.8	12.48	-0.0825	-0.66

Comments:

+ Conc. Difference = Act % - Exp (Std) %
 Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 9/5/96 Analyte: CO

Source: Kuma Scott HT-1 Run #: 3

Zero Cyl #: 4-36919 Conc. 00.0 % CO Cyl Press: 1975 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260657 Conc. 2.47 % CO Cyl Press: 950 psi

Certified by: BOC Gases Date: 1/13/95

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO
EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myrum Time: 1045 Temp: 74 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.3	-0062	-0062	-0.12
Span	2.47	49.4	2.47	2.48	49.4	23955	-0745	-3.01

Comments:

Post Run Audit: By: A.T. Myrum Time: 1535 Temp.: 80 °F

Audit Results

Point #	Expected Response			Actual Response			± Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.2	-0013	-0013	-0.23
Span	2.47	49.4	2.47	2.45	48.9	2371	-0986	-3.99

Comments:

+ Conc. Difference = Act % - Exp (Std) %
 Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$
 Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: KUMA SCOTT HT-1
 Run: 3
 Date: 9/5/96
 Technicians: ATH, PLS.
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 71 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 69.0 °F; T/C#2: 69.2 °F;
 T/C #3: 69.2 °F; T/C #4: 69.4 °F; T/C #5: 69.4 °F;
 T/C #6: 69.4 °F; T/C #7: 69.6 °F; T/C #8: 69.6 °F;
 T/C #9: 69.2 °F; T/C #10: 69.6 °F; T/C #11: 69.8 °F;
 T/C #12: 69.2 °F; T/C #13: 69.4 °F; T/C #14: 69.4 °F;
 T/C #15: 69.2 °F; T/C #16: 66.0 °F; T/C #17: _____ °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: _____

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : -0.2 °F Adj to: 0.0 °F Post Test Check Zero (0°F): 0.4 °F % Difference +0.02
 Span (2000°F): 2000.4 °F Adj to: 2000.0 °F Span (2000°F): 2000.6 °F +0.03
 (Allowable % Difference = 1.5%.^o Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check
 0°F = 0.0 °F; 200°F = 201.6 °F; 400°F = 398.8 °F;
 600°F = 601.0 °F; 800°F = 800.8 °F; 1000°F = 1000.4 °F;
 1200°F = 1198.6 °F; 1400°F = 1399.4 °F; 1600°F = 1598.6 °F
 1800°F = 1799.6 °F; 2000°F = 2000.0 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre OK Post OK
 Draft (Static) Gauge Zero Check: Pre OK Post OK

Scale Check Pre (Wt, #'s): 433.2 - 438.2 5.0 lbs. OK (PLS.)
 Post (Wt, #'s): 435.2 - 440.2 5.0 lbs. OK (PLS.)

Stack cleaned prior to the run: Yes _____ No ✓
 Tunnel cleaned prior to the run: Yes _____ No ✓

DILUTION TUNNEL CALCULATIONS
3/31/96

MYREN CONSULTING CERTIFICATION TEST DATA

File Name:	ckumar4	RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
Stove Manufacturer:	KUIMA	0	0.040	110	984.200	73	0.900	829.07		
Model Number:	SCOTT HT-1	10	0.039	125	989.225	77	0.900	829.34	106.1	5.014
Lab Name:	MYREN	20	0.038	125	994.160	82	0.870	818.64	103.2	4.879
Test Date:	9/6/96	30	0.038	124	999.055	88	0.870	817.94	102.4	4.786
Run Number:	4	40	0.039	117	1003.980	93	0.870	823.65	100.9	4.772
Meter Box Y Factor:	1.012	50	0.040	118	1008.975	97	0.870	834.87	101.1	4.805
Barometric pressure (in):	29.95	60	0.039	116	1013.875	100	0.880	822.94	97.0	4.688
Gas meter temp (ave):	93.09	70	0.039	113	1018.815	102	0.880	820.79	98.3	4.710
delta H(ave):	0.882	80	0.039	109	1023.780	103	0.880	817.92	98.2	4.725
Gas meter initial reading:	984.2	90	0.040	107	1028.735	104	0.890	826.89	97.8	4.707
Gas meter final reading:	1032.693	98	0.040	103	1032.693	105	0.890	823.96	95.8	3.754
Front catch (acetone) mg:	3.1	110						0.00	0.0	0.000
first filter catch (mg):	3.7	120						0.00	0.0	0.000
second filter catch (mg):	-1.9	130						0.00	0.0	0.000
tunnel flow (ave cfm):	142.66	140						0.00	0.0	0.000
Emission Rate(g/hr):	0.904	150						0.00	0.0	0.000
Emission Rate(M5H) :	1.673	160						0.00	0.0	0.000
vs/VmTs:	0.03	170						0.00	0.0	0.000
vs ave:	824.18	180						0.00	0.0	0.000
Tunnel average temp (°f):	115.18	190						0.00	0.0	0.000
Test time(min):	98	200						0.00	0.0	0.000
Fuel Load(lb. wet):	10.9	210						0.00	0.0	0.000
Wood moisture(%wet):	18.234	220						0.00	0.0	0.000
Burn rate(dry kg/hr):	2.475	230						0.00	0.0	0.000
Samp vol(scf):	46.840	240						0.00	0.0	0.000
front filter number	135	250						0.00	0.0	0.000
back filter number	134	260						0.00	0.0	0.000
acetone beaker number	7	270						0.00	0.0	0.000
PRELIMINARY RESULTS		280						0.00	0.0	0.000
FINAL RESULTS		290						0.00	0.0	0.000
DATA SUMMARY		300						0.00	0.0	0.000
MODEL :	SCOTT HT-1	310						0.00	0.0	0.000
RUN:	4	320						0.00	0.0	0.000
DATE:	9/6/96	330						0.00	0.0	0.000
DBR:	2.475	340						0.00	0.0	0.000
GPH UNADJ	0.904	350						0.00	0.0	0.000
ADJ	1.673							0.00	0.0	0.000

DATE 9/6/96

PAGE 1 OF 1

MODEL # Scott HT-1

RUN # 4

METER BOX # 45G-P

METER Y 1,012

FILTER # (F) B5 (R) 134

PRE TEST LEAK RATE = .000 CFM @ -15.75 IN. HG

FILTER SIZE: 110MM

POST TEST LEAK RATE = .000 CFM @ -15.00 IN. HG

PROBE LENGTH 84" glass

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
1035	00	984.200	-0.040	110	73	-0.90	0	N-1	0.5"	-0.024	132
45	10	989.225	-0.039	125	77	-0.90	0	2	1.5"	-0.045	132
55	20	994.160	-0.038	125	82	0.87	0	3	4.5"	-0.046	133
1105	30	999.055	-0.038	124	88	.87	0	4	5.5"	-0.034	132
15	40	1003.980	-0.039	117	93	.87	0	W-1	0.5"	-0.033	130
25	50	1008.975	-0.040	118	97	.87	0	2	1.5"	-0.043	131
35	60	1013.875	-0.039	116	100	.88	0	3	4.5"	-0.039	130
45	70	1018.815	-0.039	113	102	.88	0	4	5.5"	-0.021	131
55	80	1023.780	-0.039	109	103	.88	0	Avg. <u>0.03562</u> <u>131.375</u>			
1205	90	1028.735	-0.040	107	104	.89	0	Pilot Leak Check Pre <u>OK</u> Post <u>OK</u>			
1213	90 98	1032.693	-0.040	103	105	.89	0	Cp = <u>0.99</u>			
	10							N * → W 1 2 3 4 3 4 ↑			
	20							* = point of Avg. delta p			
	30							Qs = $\left(\sqrt{\frac{\Delta P \times BP}{T(^{\circ}R)}} \right) \times 3167.2 =$			
	40							N <u>134.463</u> cfm			
	50							BP = <u>Start 29.95</u> in Hg <u>60 min 29.95</u> <u>End 29.95</u>			
	60										
	70										
	80										
	90										

$\bar{X} = 29.95$

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 6/1/96 Time 1532 By ATM Front Half _____ Back Half _____

Manufacturer: S&S Size: 110 MM Lot.No.: 20941 Grade: F20-105

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
126	.7451	6/3/96	1111	ATM	.7449	6/5/96	1853	RLS				
127	.7364	"	1110	ATM	.7360	6/5/96	1852	RLS				
128	.7419	"	1109	ATM	.7416	6/5/96	1857	RLS				
129	.7422	"	1108	ATM	.7420	6/5/96	1850	RLS				
130	.7306	"	1107	ATM	.7304	6/5/96	1849	RLS				
131	.7420	"	1106	ATM	.7413	6/5/96	1848	RLS	.7414	6/6/96	11:35	ATM
132	.7374	"	1102	ATM	.7371	6/5/96	1848	RLS				
133	.7371	"	1102	ATM	.7369	6/5/96	1847	RLS				
134	.7404	"	1101	ATM	.7403	6/5/96	1846	RLS	✓			
135	.7390	"	1101	ATM	.7389	6/5/96	1845	RLS	✓			
136	.7388	"	1100	ATM	.7386	6/5/96	1844	RLS				
137	.7395	"	1059	ATM	.7392	6/5/96	1843	RLS				
138	.7394	"	1056	ATM	.7392	6/5/96	1843	RLS				
139	.7435	"	1058	ATM	.7433	6/5/96	1842	RLS				
140	.7395	"	1057	ATM	.7393	6/5/96	1840	RLS				
141	.7486	"	1057	ATM	.7477	6/5/96	1839	RLS	.7476	6/6/96	1133	ATM
142	.7265	6/5/96	1838	RLS	.7264	6/6/96	11:32	ATM				
143	.7258	6/5/96	1837	RLS	.7258	6/6/96	11:31	ATM				
144	.7254	6/5/96	1836	RLS	.7254	6/6/96	11:30	ATM				
145	.7377	"	1056	ATM	.7372	6/5/96	1830	RLS	.7376	6/6/96	10:58	ATM
146	.7513	"	1056	ATM	.7510	"	1832	RLS				
147	.7465	"	1055	ATM	.7462	"	1833	RLS				
148	.7450	"	1054	ATM	.7448	"	1834	RLS				
149	.7474	"	1054	ATM	.7471	"	1835	RLS				
150	.7415	"	1053	ATM	.7413	"	1835	RLS				

Checked by ATM Date: 6/6/96 Time 11:41

QA REWEIGH

Filter #	WT	Date	Time	By
136	.7386	6/6/96	11:34	ATM
139	.7412	6/6/96	11:36	ATM
149	.7472	6/6/96	11:39	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
59	72	45	6/3/96	1005	ATM
57	73	49	6/5/96	1825	RLS
51	73	44	6/6/96	1035	ATM

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

4th Round

Into Dessicator: Date: 6/27/96 Time: 1200 By: A.J. Kuma

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4824	8/9/96	1446	ATM	65.4819	8/9/96	1125	PLS				
2	66.1488	7/25/96	1217	PLS	66.1484	8/1/96	0958	ATM				
3	67.8548	8/8/96	1553	ATM	67.8542	8/9/96	1103	PLS	67.8544	8/14/96	11:30	ATM
4	67.5870	8/8/96	14124	ATM	67.5865	8/9/96	1130	PLS	KUMA #1			
5	67.2054	8/2/96	1618	ATM	67.2050	8/9/96	1058	PLS	KUMA 5			
6	67.4250	7/3/96	1403	PLS	67.4244	7/10/96	1059	ATM	67.4250	7/25/96	1155	PLS
7	65.5422	8/8/96	1533	ATM	65.5423	8/9/96	1110	PLS	KUMA 4			
8	66.0183	7/10/96	1100	ATM	66.0187	7/25/96	1055	PLS				
9	66.9280	7/8/96	1312	ATM	66.9276	8/9/96	1120	PLS	KUMA #2			
10	66.0862	7/10/96	1111	ATM	66.0860	7/25/96	0933	PLS				
11	65.6989	7/10/96	1108	ATM	65.6989	7/25/96	1020	PLS				
12	Broken											

KUMA #2
KUMA #1
KUMA 5
KUMA 4
BLANK 8/10/96

Checked By: _____ Date: _____ Time: _____

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	ZRH	Date	Time	By
58	70	47	7/3/96	0953	ATM
60	72	49	7/10/96	1006	ATM
57.5	69	48	8/1/96	0948	ATM
66	70	49	8/10/96	1235	ATM
60	72	49	8/9/96	0745	ATM
64	72	49	8/14/96	1116	ATM

WOODSTOVE DATA SHEET #4-4
SCALE QA SHEET

Dates From 6/20/96

Scale Metric

Model RE100
SN A04027

Through 9/10/96

TROEMNER CLASS 5 WTS.

100g Weight	10g Weight	1.0g Weight	100mg Weight	20mg Weight	Tech	Date	Time	Dry Bulb	Wet Bulb	% RH
100.0003	10.0000	1.0000	1.0000	0.1994	PLS	6/20/96	1625	61	74	47
100.0000	10.0000	1.0000	1.0000	0.2000	ATM	6/21/96	1259	61	74	47
99.9996	10.0000	1.0000	1.0000	0.2001	ATM	6/25/96	1410	63	76	48
99.9996	10.0000	1.0000	1.0000	0.2001	ATM	6/27/96	1318	65	78	46
99.9998	10.0000	1.0000	1.0000	0.2000	ATM	6/28/96	1254	58	78	49
100.0001	10.0000	1.0000	1.0000	0.2000	ATM	7/1/96	1504	63	78	48
100.0003	10.0000	1.0000	1.0000	0.2000	ATM	7/2/96	1316	64	77	47
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	7/3/96	953	58	70	47
99.9998	10.0000	1.0000	1.0000	0.2001	ATM	7/3/96	1727	57	83	42
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	7/9/96	1456	% RH TO high		
99.9996	10.0000	1.0000	1.0000	0.2001	ATM	7/10/96	1006	60	78	49
99.9998	10.0000	1.0000	1.0000	0.2000	ATM	7/11/96	0918	59	71	48
100.0000	10.0000	1.0000	1.0000	0.2000	ATM	7/12/96	842	59	71	48
100.0003	10.0000	1.0000	1.0000	0.2001	ATM	7/16/96	1233	62	75	47
99.9996	10.0000	1.0000	1.0000	0.2002	ATM	7/17/96	1605	63	74	47
99.9999	10.0000	1.0000	1.0000	0.1998	ATM	7/18/96	0733	68	56	49
99.9999	10.0000	1.0000	1.0000	0.2000	ATM	7/19/96	0740	71	59	48
99.9997	10.0000	1.0000	1.0000	0.2000	ATM	7/20/96	1445	82	68	48
99.9996	10.0000	1.0000	1.0000	0.2001	ATM	7/23/96	1513	80	66	47
99.9999	10.0000	1.0000	1.0000	0.2000	ATM	7/24/96	0757	59	71	48
99.9999	10.0000	1.0000	1.0000	0.2001	ATM	7/24/96	1617	71	86	47
100.0002	10.0000	1.0000	1.0000	0.2001	ATM	7/25/96	0814	67	73	49
99.9995	10.0000	1.0000	1.0000	0.2002	ATM	7/31/96	2035	65	79	47
100.0000	10.0000	1.0000	1.0000	0.2002	ATM	8/1/96	0905	69	57.5	48
99.9999	10.0000	1.0000	1.0000	0.2002	ATM	8/1/96	1950	60	72	49
99.9999	10.0000	1.0000	1.0000	0.2002	ATM	8/2/96	1301	59	71	47
100.0001	10.0000	1.0000	1.0000	0.1999	ATM	8/9/96	1335	66	79	49
99.9996	10.0000	1.0000	1.0000	0.2001	ATM	8/9/96	0154	60	72	49
100.0003	10.0000	1.0000	1.0000	0.2000	ATM	8/14/96	1116	64	77	49
99.9999	10.0000	1.0000	1.0000	0.2001	ATM	8/15/96	1908	66	79	49
100.0002	10.0000	1.0000	1.0000	0.2001	ATM	8/28/96	1611	70	85	49
99.9995	10.0000	1.0000	1.0000	0.2000	ATM	8/29/96	1008	74	77	49
99.9996	10.0000	1.0000	1.0000	0.2000	ATM	8/30/96	1005	61	73	48
99.9996	10.0000	1.0000	1.0000	0.2000	ATM	9/5/96	0954	59	71	48
99.9996	10.0000	1.0000	1.0000	0.2000	ATM	9/6/96	1030	72	60	49
100.0000	10.0000	1.0000	1.0000	0.2000	ATM	9/9/96	1806	76	63	48
100.0003	10.0000	1.0000	1.0000	0.2000	ATM	9/10/96	1726	77	64	48

Unit: KAMA Scott HT-1
 Run: 7
 Date: 9/6/96
 Technicians: ATM 12LS
 WST20, Form 5

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 EPA M5G-1

Filters

Filter # 134 (R) Beaker # 7 Final Wt. 65.5455 g ✓
 Final Wt .7384 g ✓ Ml 78 Tare Wt. 65.5423 g ✓
 Tare Wt .7403 g ✓ Desc. Acetone Net Wt. .0032 g ✓
 Net Wt -.0019 g ✓

Filter # 135 (F) Beaker # _____ Final Wt. _____ g
 Final Wt .7426 g ✓ Ml _____ Tare Wt. _____ g
 Tare Wt .7389 g ✓ Desc. _____ Net Wt. _____ g
 Net Wt .0037 g ✓

Acetone Blank Calculation: Blank done 8/8/96

Blank Beaker # 6 Final Wt 67.4251
 Ml 140 Tare Wt 67.4250
 Desc Acetone Net Wt .0001
.0001 g ÷ 140 ml = .000001 g/ml

Particulate Catch Calculation

Filter: .0037 g ✓
 Filter: -.0019 g ✓
 Beakers: .0032 - (.000001)(78) = .0031 g ✓
 Total Catch Ml of Acetone
 Blank Value/Ml of Acetone
 Total Catch = .0049 g ✓

Unit SCOTT KUMA HT-1
 Run # 4
 Date 9/6/96
 Technician ATM, RLS.
 WST6-Form1, Rev11/89

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 1.716 ft³

Dilution Tunnel Draft (If applicable): Start 0 Stop 0

Test Chamber Air Velocity: Start: 0 Stop: 0 Avg: 0

Wet Bulb/ Start: WB: 61 °F DB: 71 °F 1.5 % Amb Moisture 56 %RH

Dry Bulb Stop: WB: 59 °F DB: 70 °F 1.3 % Amb Moisture 51 %RH

$\bar{X} = 1.40$ % Ambient Moisture $\bar{X} = 53.5$ % Relative Humidity (RH)

Empty

Stove Wt: 343.1 lbs.

Empty

Stove Wt with Stack (Inc. Oil Seal) Wet: 433.0 lbs. Dry: 432.8 lbs.

Empty

Stove Wt with Stack and Ash Ash: — lbs. Total: — lbs.

Kindling Wt. Paper: 0.3 lbs. Wood: 4.0 lbs.

Pre Burn Fuel Wt. 11.4 + 10.8 + 13.7 Total: 35.9 lbs.

Total Kindling and Pre Burn Fuel Wt 40.2 lbs.

Coal Bed Wt-lbs: Range (2.7 - 2.2) lbs. Actual: 2.3 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range $\frac{435.5}{\text{Upper Wt.}} + \frac{435.0}{\text{Lower Wt.}} \cdot 12 \times .25 = \underline{0.6}$ lbs.

Test Fuel Wt-lbs: Ideal 12.0 lbs. Range: 10.9-13.2 lbs. Actual: 10.9 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 14 Pcs.

2 x 4's x 14^{5/16} " 3 Pcs 6.8 lbs. 62.4 %

4 x 4's x 14^{5/16} " 1 Pcs 4.1 lbs. 37.6 %

Est. Dry Burn Rate (Kg/Hr.) $\frac{10.9}{2.20} - (10.9 \times 1.8234) \times \frac{60}{98} = \underline{2.475}$ Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (HO_E) (Avg BTU's/Hr) $(19,140) \times \frac{63}{100} \times 2.475 = \underline{29,045}$ Est Heat Output (HO_E) BTU's/Hr

Comments:

STOVE OPERATING DATA
WOODSTOVE TEST DATA SHEET #9

Unit: Kumra Scott HT-1
Run: 4
Date: 9/6/96
Technician(s): AMM, DLS
WST3-Form 1 Rev 9/90

Fire Started: 0722 PDST

Warm up and Preburn: Primary Air: Wide open from ignition until the start of the preburn when the primary air control(s) was (were) adjusted to the run setting of Wide Open. At the run setting until the start of the test.

High Burn - Wide Open from ignition to start of test.

Secondary Air:

No Controls. Naturally drafted.

Secondary Burn/~~W~~ Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge.

Starting 1130 before the start of the test, broke up, raked and leveled the coal bed. In stove for 25 seconds.

Test: Door Wide Open during loading _____ min 25 sec, then Closed.

Primary Air: Wide open during the start of the test until End of test. Adjusted to the run setting of N/A between _____ and _____. At the run setting of Wide Open at 0:00 into the run. High Burn. Wide open from start to end of test.

Secondary Air:

No Controls. Naturally drafted

Secondary Burn/~~W~~ Bypass: N/A

Fan: Off during warm up. On high during preburn. Off at the start of the test. Off for 1st 5 minutes of the test. On high @ 5:00 into the test. On high for the rest of the test.

Test Run Anomalies:

Very Good high burn.

WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

- 1st Warm up/Pre Burn Fuel charge (11.4 lbs) added at 0743
- 2nd Warm up/Pre Burn Fuel charge (10.8 lbs) added at 0822
- 3rd Warm up/Pre Burn Fuel charge (13.7 lbs) added at 0913
- 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____
- 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____
- 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____
- 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____
- 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 0.2 lbs.

All pre burn/warm up fuel pieces were either 14 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 14 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 14 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 14 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

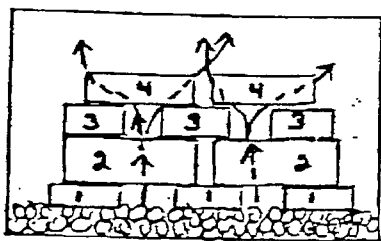
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

Unit: SCOTT KUMA HT-1
Run # 4
Date 9/6/96
Technician ATM, RLS
Page 2 of
WST7-Form2-A, Rev 6/90

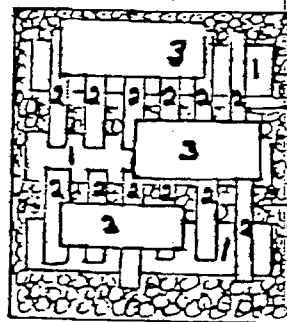
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a collapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP

surface temperature(s) and the peak value(s) obtained were 925 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of Wide Open 35.9 lbs above the upper charcoal bed weight..

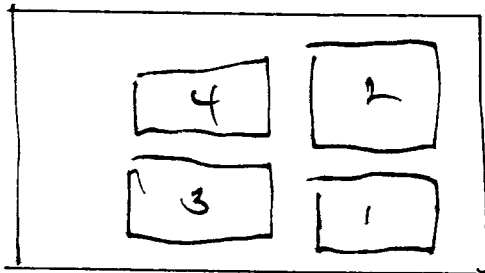
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit SCOTT KUMA HT-1
Run # 4
Date 9/6/96
Technician ATH, RLS
Page 3 of 3
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① Turned fan off.
② opened door ③ loaded test fuel charge into
the stove ④ photo ⑤ closed the door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



Front of stove view
4 X 4's: 2
2 X 4's: 1, 3 & 4
Loading Sequence: 1, 2, 3 & 4
Driest Pcs in Load 3

Loaded the test fuel charge on an essentially level, medium-large
sized, average coal bed (in appearance, color and temperature
for a High burn rate.

Load 0:30
Ignition 0:25
Door Closed 0:30
Firebox engulfed in flames 2:45
Very nice start.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: SCOTT KUMA HT-1
Run: 4
Date: 9/6/96
Technician: ATH, RLS
WST1-Form7-Rev11/89

Room Temperature: 69 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture

Uncor Values are corrected for temperature: Yes No

Time Test Fuel Moisture Readings taken at: 0845

Calibration Checks: X Y 12.5 12.4 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4	K	8.0	8.4	8.0	8.4	8.0	8.4	(8.400)
2									
3									
4									
5	2x4x8'	P	18.0	19.2	18.0	19.2	18.0	19.2	19.200
6	"	P	18.0	19.2	18.5	19.8	18.0	19.2	19.400
7	"	P	22.0	23.7	22.5	24.3	22.0	23.7	23.900
8									(62.500)
9									
10									
11	2x4x14 5/16"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200
12	"	T	22.5	24.3	22.5	24.3	22.5	24.3	24.300
13	"	T	22.0	23.7	22.0	23.7	22.0	23.7	23.700
14									
15	4x4x14 5/16"	T	19.5	20.9	20.0	21.4	22.0	23.7	22.000
16									(89.200)
17									
18									
19	FEET	T	18.0	19.2	18.0	19.2	18.0	19.2	(19.200)
20									(OUT SPACERS)

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.400 % ✓	20.833 % ✓	22.300 % ✓
% Moisture - Wet Basis:	7.749 % ✓	17.241 % ✓	18.234 % ✓

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: SCOTT KUWA HT-1
 Run#: 4
 Date: 9/6/96
 Technician: ATM, RLS
 WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
 Depth (D): IN 1.568 cm 3.9827 ✓
 Width (W): IN 3.533 cm 8.9738 ✓
 Length (L): 3.568 cm
3.548 cm
3.566 cm
3.543 cm
 Length \bar{X} = IN 3.556 ✓ cm 9.0322
 Volume: 322.814 cm³ ✓
 (D X W X L)

MOISTURE: Room Temperature: 69 °F Correction Factor: 0
 Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	
Top:	<u>20.5</u>	<u>22.0</u> %	
Bottom:	<u>20.0</u>	<u>21.4</u> %	
Side:	<u>19.5</u>	<u>20.9</u> %	
\bar{X} :		<u>21.433</u> %	

Avg % Moisture (Dry) 21.433 % ✓
 Avg % Moisture (Wet) 17.650 % ✓
 Scale: Levelled In Out
 Zeroed: In Out

Wet Weight: 186.0 g Dry Weight: 157.1 g

% Moisture Dried Basis: 15.538 % ✓
 [1 - (Dry Wt - Wet Wt)] X 100

Into Dryer Date 9/6/96 Time 1100 Temp 215 °F
 Out of Dryer Date 9/9/96 Time 1715 Temp 220 °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = $\frac{157.1}{(\text{dry wt})}$ g ÷ $\frac{322.814}{(\text{volume})}$ cm³ = 4867 g/cm³ ✓

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
 Wet Wt: _____ g - _____ g = _____ g
 Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
 Dry Wt: _____ g - _____ g = _____ g
 Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: _____ %
 [1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

END: 435.1 lbs.

Minute	Scale Wt	lbs left	Burn Rate	CO ₂		O ₂		Tel	CO v.	BaL	Wet Bulb	Dry Bulb	% H ₂ O	Calc W/B	Stack	SO ₂ v.	PPM	Static Press.	Comments
				v.	%CO ₂	v.	%O ₂												
0	446.0	10.9	0	8.07	8.07	49.0	12.2			10.4	82	85	3.5	122	294			-0.72	Flow
5	445.1	10.0	.9	9.95	9.95	31.5	8.60			26.9	107	118	7.5	136	476			-0.87	SO₂ 1.5
10	444.1	9.0	1.0	14.20	14.20	26.4	6.59			52.5	103	130	8.6	141	546			-0.91	CO₂ 1.5
15	443.1	8.0	1.0	12.4	12.4	32.9	8.21			42.1	122	133	12.0	147	550			-0.90	O₂ 1.5
20	442.1	7.0	1.0	13.8	13.8	27.1	6.76			81.4	127	139	13.5	148	553			-0.90	CO 1.5
25	441.2	6.1	.9	14.2	14.2	26.5	6.61			71.9	129	134	14.5	150	555			-0.91	
30	440.4	5.3	.8	13.3	13.3	27.9	7.46			100.0	125	134	13.0	148	557			-0.88	
35	439.8	4.7	.6	11.6	11.6	36.5	9.10			64.4	122	130	12.0	145	524			-0.85	
40	439.2	4.1	.6	10.8	10.8	39.3	9.80			41.6	119	121	11.0	143	502			-0.83	
45	438.6	3.5	.6	11.5	11.5	37.2	9.28			63.8	116	120	10.0	142	505			-0.83	
50	438.0	2.9	.6	11.8	11.8	35.6	8.86			78.4	112	119	9.0	140	515			-0.84	
55	437.5	2.4	.5	10.9	10.9	39.1	9.75			72.9	103	110	7.5	137	501			-0.82	
60	437.1	2.0	.4	10.1	10.1	42.0	10.5			50.3	95	103	6.3	133	485			-0.87	SO₂ 1.5
65	436.7	1.6	.4	9.16	9.16	45.3	11.3			36.6	93	104	4.7	132	475			-0.80	CO₂ 1.5
70	436.3	1.2	.4	8.79	8.79	46.5	11.6			31.4	89	102	4.2	128	459			-0.78	O₂ 1.5
75	436.0	.9	.3	8.94	8.94	45.7	11.4			34.4	89	100	4.2	128	454			-0.77	CO 1.5
80	435.7	.6	.3	7.93	7.93	49.7	12.4			28.3	88	101	4.2	126	435			-0.75	
85	435.5	.4	.2	7.03	7.03	53.1	13.2			14.4	87	97	4.0	124	415			-0.72	
90	435.4	.3	.1	6.71	6.71	54.1	13.5			11.2	85	95	3.7	123	400			-0.70	
95	435.2	.1	.2	6.15	6.15	56.5	14.1			8.3	83	93	3.5	121	386			-0.69	
100	435.1	.0	.1	5.48	5.48	58.5	14.6			6.0	82	93	3.4	120	370			-0.67	
105															385			1.669	
110											21.5								
115															501			1.695	
120															474			1.081	

T/C#	Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp.	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar
0	10:35	521	578	158	561	427	1107	1008	70	110	247	35	77	35	
5	40	550	557	214	539	436	979	1103	69	122	248	36	75	34	
10	45	687	556	180	530	429	1046	1165	69	125	248	36	75	34	
15	50	707	557	163	518	428	1025	1211	69	125	248	36	75	34	
20	55	712	548	155	509	415	1044	1286	69	125	248	36	76	34	
25	1:00	725	546	157	509	408	1103	1348	69	125	248	36	76	34	
30	05	712	542	150	515	404	1115	1340	70	124	247	36	76	34	
35	10	679	544	148	520	394	1109	1260	70	120	247	36	76	34	
40	15	640	544	149	522	389	1092	1256	70	117	247	36	77	34	
45	20	626	542	150	523	386	1071	1250	69	117	247	36	77	34	
50	25	633	542	157	524	388	1072	1250	69	118	248	37	77	34	
55	30	629	547	153	527	384	1066	1236	70	117	248	37	77	34	
60	35	606	543	155	535	399	1071	1176	70	116	248	37	76	34	
65	40	583	540	156	536	398	1043	1131	70	114	248	37	76	34	
70	45	563	538	157	537	405	1031	1113	70	113	248	37	76	34	
75	50	545	534	157	538	408	1026	1104	70	112	248	37	75	34	
80	55	529	530	158	540	413	977	1074	70	109	247	37	75	34	
85	1:00	498	527	158	544	420	944	1038	70	108	246	37	75	34	
90	05	474	526	158	543	433	969	1024	70	107	247	37	76	34	
95	10	455	522	158	541	436	907	985	70	105	246	37	74	34	
100	15	433	519	157	535	434	876	957	70	103	248	37	74	34	
105	20	468	547	144	549	374	884	959	70	103	248	37	74	34	
110	25														
116	30	19,507	11,372	3337	11,146	8634	21,623	24,309	1463		21		START.	449.0	✓
													FINISH	45.6	✓
													Δ T =	-33.4	✓

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 9/6/96 Analyte: CO₂

Source: SCOTT KUMA HT-1 Run #: 4

Zero Cyl #: 4-36919 Conc. 00.0 % CO₂ Cyl Press: 1950 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260657 Conc. 10.1 % CO₂ Cyl Press: 925 psi

Certified by: BOC Gases Date: 1/10/95

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: A.T. Myren Time: 0920 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.4	.404	10.1	40.0	.404	10.0511	-.0489	-0.48

Comments:

Post Run Audit: By: A.T. Myren Time: 1247 Temp: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.4	.404	10.1	40.4	.405	10.0759	-.0241	-0.24

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 9/6/96 Analyte: O₂

Source: SCOTT KUMA HT-1 Run #: 4

Zero Cyl #: 4-36919 Conc. 00.0 % O₂ Cyl Press: 1950 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260657 Conc. 12.5 % O₂ Cyl Press: 925 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: A.T. Myren Time: 0920 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.5	00.2	0552	.0552	0.22
Span	12.5	50.0	12.5	12.6	50.0	12.467	-0.0326	-0.26

Comments:

Post Run Audit: By: A.T. Myren Time: 1240 Temp.: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.5	00.2	0552	.0552	0.22
Span	12.5	50.0	12.5	12.6	49.9	12.442	-0.0576	-0.46

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 9/6/96 Analyte: CO

Source: SCOTT KUMA HT-1 Run #: 4

Zero Cyl #: 4-36919 Conc. 00.0 % CO Cyl Press: 1950 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260657 Conc. 2.47 % CO Cyl Press: 925 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter: _____

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A. Timmy Time: 0920 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.3	-0062	-.0062	-0.12
Span	2.47	49.4	2.47	2.48	49.4	2396	-.0745	-3.01

Comments:

Post Run Audit: By: A. Timmy Time: 1248 Temp.: 71 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.3	-0062	-.0062	-0.12
Span	2.47	49.4	2.47	2.48	49.4	2396	-.0745	-3.01

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: SCOTT KUMIA HT-1
 Run: 4
 Date: 9/6/96
 Technicians: ATM, PLS
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 67 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 69.0 °F; T/C#2: 69.2 °F;
 T/C #3: 69.4 °F; T/C #4: 69.4 °F; T/C #5: 69.2 °F;
 T/C #6: 69.2 °F; T/C #7: 69.4 °F; T/C #8: 69.6 °F;
 T/C #9: 69.4 °F; T/C #10: 69.6 °F; T/C #11: 67.4 °F;
 T/C #12: 69.4 °F; T/C #13: 69.6 °F; T/C #14: 69.4 °F;
 T/C #15: 69.2 °F; T/C #16: 66.0 °F; T/C #17: _____ °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: _____

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : -0.4 °F Adj to: 0.0 °F Post Test Check Zero (0°F): 0.4 °F % Difference +0.02
 Span (2000°F): 1999.6 °F Adj to: 2000.0 °F Span (2000°F): 2000.0 °F 0
 (Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

Thermocouple Readout Pretest Linearity Check
 0°F = 0.0 °F; 200°F = 201.6 °F; 400°F = 398.8 °F;
 600°F = 601.0 °F; 800°F = 800.8 °F; 1000°F = 1000.4 °F;
 1200°F = 1198.4 °F; 1400°F = 1399.0 °F; 1600°F = 1598.6 °F
 1800°F = 1799.6 °F; 2000°F = 2000.0 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre OK Post OK
 Draft (Static) Gauge Zero Check: Pre OK Post OK

Scale Check Pre (Wt, #'s): 433.0 - 438.0 5.0 lbs. OK (PLS)
 Post (Wt, #'s): 435.0 - 440.0 5.0 lbs. OK (PLS)

Stack cleaned prior to the run: Yes _____ No ✓
 Tunnel cleaned prior to the run: Yes _____ No ✓

MYREN CONSULTING CERTIFICATION TEST DATA

DILUTION TUNNEL CALCULATIONS
3/31/96

File Name: CKUMAR5

Stove Manufacturer: KUMA

Model Number: SCOTT HT-1

Lab Name: MYREN

Test Date: 9/19/96

Run Number: 5

Meter Box Y Factor: 1.012

Barometric pressure (in): 29.955

Gas meter temp (ave): 102.65

delta H(ave): 0.882

Gas meter initial reading: 32.1

Gas meter final reading: 139.32

Front catch (acetone) mg: 3.8

first filter catch (mg): 28.7

second filter catch (mg): 1.0

tunnel flow (ave cfm): 144.30

Emission Rate(g/hr): 2.87

Emission Rate(M5H) : 4.37

vs/MmTs: 0.01

vs ave: 797.54

Tunnel average temp (°f): 90.35

Test time(min): 215

Fuel Load(lb. wet): 10.9

Wood moisture(%wet): 18.133

Burn rate(dry kg/hr): 1.130

Samp vol(scf): 101.927

front filter number: 137

back filter number: 136

acetone beaker number: 5

PRELIMINARY RESULTS

FINAL RESULTS

DATA SUMMARY

MODEL : SCOTT HT-1

RUN: 5

DATE: 9/19/96

DBR: 1.130

GPH UNADJ: 2.874

ADJ: 4.372

RUN TIME (min)	PITOT DELTAP (- INCH H2O)	TNL TEMP (°F)	GAS METER RDG (ft3)	GAS METER TEMP (°F)	GAS METER DELTA H (in.H2O)	TUNNEL VELOCIT (ft/min)	PROP RATE (%)	dDGM vol std (ft3)
0	0.038	90	32.100	72	0.900	793.71		
10	0.039	98	37.245	77	0.890	809.91	110.3	5.135
20	0.039	97	42.175	82	0.880	809.19	102.5	4.875
30	0.038	99	47.065	88	0.870	800.18	101.0	4.782
40	0.038	99	51.925	94	0.860	800.18	100.4	4.701
50	0.038	99	56.810	98	0.870	800.18	100.2	4.691
60	0.038	97	61.715	101	0.870	798.74	99.7	4.685
70	0.038	95	66.655	104	0.880	797.31	99.7	4.694
80	0.038	94	71.620	106	0.870	796.59	99.8	4.701
90	0.038	92	76.585	107	0.870	795.15	99.4	4.693
100	0.038	90	81.565	108	0.880	793.71	99.3	4.699
110	0.037	89	86.570	109	0.880	782.48	99.7	4.714
120	0.038	89	91.575	109	0.880	792.99	101.1	4.714
130	0.039	88	96.575	110	0.880	802.62	99.3	4.701
140	0.039	88	101.590	110	0.890	802.62	98.4	4.715
150	0.039	87	106.615	110	0.890	801.89	98.4	4.725
160	0.039	86	111.650	110	0.890	801.16	98.5	4.734
170	0.039	85	116.685	111	0.890	800.42	98.3	4.726
180	0.040	83	121.725	111	0.890	809.13	98.1	4.730
190	0.038	84	126.750	111	0.890	789.37	96.9	4.716
200	0.038	83	131.785	111	0.890	788.64	99.4	4.726
210	0.038	83	136.835	111	0.890	788.64	99.8	4.740
215	0.038	83	139.320	111	0.890	788.64	98.2	2.332
230						0.00	0.0	0.000
240						0.00	0.0	0.000
250						0.00	0.0	0.000
260						0.00	0.0	0.000
270						0.00	0.0	0.000
280						0.00	0.0	0.000
290						0.00	0.0	0.000
300						0.00	0.0	0.000
310						0.00	0.0	0.000
320						0.00	0.0	0.000
330						0.00	0.0	0.000
340						0.00	0.0	0.000
350						0.00	0.0	0.000

METHOD 5G-1

PARTICULATE SAMPLING DATA

Kuma

LAB-1

DATE 9/9/96

PAGE 1 OF 2

MODEL # Scott HT-1

RUN # 5

METER BOX # 45G-P

METER Y 1.012

FILTER # (F) 137 (R) 136

PRE TEST LEAK RATE = .001 CFM @ -17.5 IN. HG

FILTER SIZE: 110 mm

POST TEST LEAK RATE = .000 CFM @ -13.0 IN. HG

PROBE LENGTH 24" glass

TIME		METER READING CU. FT.	PITOT dp	TNL TEMP. (°F)	METER TEMP. (°F)	GAS METER dh	VAC IN. Hg	VELOCITY TRAVERSE			
CLOCK	ELAPSED							POINT	LOCATION	ΔP	TEMP
2125	00	32.100	-038	90	72	0.90	0	N-1	0.5"	-023	95
35	10	37.245	-039	98	77	.89	0	2	1.5"	-046	95
45	20	42.175	-039	97	82	.88	0	3	4.5"	-046	95
55	30	47.065	-038	99	88	.87	0	4	5.5"	-032	94
2205	40	51.925	-038	99	94	.86	0	W-1	0.5"	-031	94
15	50	56.810	-038	99	98	.87	0	2	1.5"	-043	94
75	60	61.715	-038	97	101	.87	0	3	4.5"	-045	94
35	70	66.655	-038	95	104	.88	0	4	5.5"	-028	92
45	80	71.620	-038	94	106	.87	0	Avg. -03675			94.125
55	90	76.585	-038	92	107	.87	0	Pilot Leak Check			554.125
2305	100	81.565	-038	90	108	.88	0	Pre OK Post OK			
15	10	86.570	-037	89	109	.88	0	Cp = 0.99			N *
25	20	91.575	-038	89	109	.88	0	→ W 1 2 3 4			3
35	30	96.575	-039	88	110	.88	0				4 ↑
45	40	101.590	-039	88	110	.89	0	* = point of Avg. delta p			
55	50	106.615	-039	87	110	.89	0	Qs = (√(ΔP x BP) / T(°R)) x 3167.2 =			
0005	60	111.650	-039	86	110	.89	0	N 141,156 cfm			
15	70	116.685	-039	85	111	.89	0	BP = 29.95 in Hg			
25	80	121.725	-040	83	111	.89	0	20 mm 29.95			
35	90	126.750	-038	84	111	.89	0	120 mm 29.95			
								150 mm 29.96			

17:36
 1762 X 2 29.955
 1762

WOODSTOVE DATA SHEET #4-1: INITIAL FILTER WEIGHTS (TARE WEIGHTS)

Into Dessicator: Date 6/1/96 Time 1532 By ATM Front Half _____ Back Half _____

Manufacturer: S&S Size: 110 HVA Lot.No.: 28941 Grade: F.25 .105

Filter #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
126	.7451	6/3/96	1111	ATM	.7449	6/5/96	1853	RLS				
127	.7364	"	1110	ATM	.7360	6/5/96	1852	RLS				
128	.7419	"	1109	ATM	.7416	6/5/96	1851	RLS				
129	.7422	"	1108	ATM	.7420	6/5/96	1850	RLS				
130	.7306	"	1107	ATM	.7304	6/5/96	1849	RLS				
131	.7420	"	1106	ATM	.7415	6/5/96	1848	RLS	.7414	6/6/96	11:35	ATM
132	.7374	"	1102	ATM	.7371	6/5/96	1848	RLS				
133	.7371	"	1102	ATM	.7369	6/5/96	1847	RLS				
134	.7404	"	1101	ATM	.7403	6/5/96	1846	RLS				
135	.7390	"	1101	ATM	.7389	6/5/96	1845	RLS				
136	.7388	"	1100	ATM	.7386	6/5/96	1844	RLS				
137	.7395	"	1059	ATM	.7392	6/5/96	1843	RLS				
138	.7394	"	1056	ATM	.7392	6/5/96	1843	RLS				
139	.7435	"	1058	ATM	.7433	6/5/96	1842	RLS				
140	.7395	"	1059	ATM	.7393	6/5/96	1840	RLS				
141	.7486	"	1057	ATM	.7477	6/5/96	1839	RLS	.7476	6/6/96	1133	ATM
142	.7265	6/5/96	1838	RLS	.7264	6/6/96	11:32	ATM				
143	.7258	6/5/96	1837	RLS	.7258	6/6/96	11:31	ATM				
144	.7254	6/5/96	1836	RLS	.7254	6/6/96	11:30	ATM				
145	.7377	"	1056	ATM	.7372	6/5/96	1830	RLS	.7376	6/6/96	11:33	ATM
146	.7513	"	1055	ATM	.7510	"	1832	RLS				
147	.7465	"	1055	ATM	.7462	"	1833	RLS				
148	.7450	"	1054	ATM	.7448	"	1834	RLS				
149	.7474	"	1054	ATM	.7471	"	1835	RLS				
150	.7415	"	1053	ATM	.7413	"	1835	RLS				

Checked by ATM Date: 6/6/96 Time 1:41

QA REWEIGH

Filter #	WT	Date	Time	By
136	.7386	6/6/96	11:34	ATM
129	.7412	6/6/96	11:35	ATM
149	.7472	6/6/96	11:39	ATM

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	%RH	Date	Time	By
59	72	45	6/3/96	1005	ATM
57	73	49	6/5/96	1825	RLS
51	73	49	6/6/96	1035	ATM

WOODSTOVE DATA SHEET #4-2:
INITIAL BEAKER WEIGHTS (TARE WEIGHTS)

4th Round

Into Dessicator: Date: 6/22/96 Time: 1200 By: A.J. Miller

Beaker #	First Wt	Date	Time	By	Second Wt	Date	Time	By	Third Wt	Date	Time	By
1	65.4824	8/14/96	1446	ATM	65.4819	8/14/96	1125	RLS				
2	66.1488	7/25/96	1217	RLS	66.1484	8/11/96	0958	ATM				
3	67.8548	7/8/96	1553	ATM	67.8542	8/9/96	1103	RLS	67.8544	8/14/96	1130	ATM
4	67.5870	8/8/96	14124	ATM	67.5865	8/9/96	1130	RLS	KUMA #1			
5	67.2054	8/8/96	1618	ATM	67.2050	8/9/96	1058	RLS	KUMA 5			
6	67.4250	7/3/96	1403	RLS	67.4244	7/10/96	1059	ATM	67.4250	7/25/96	1155	RLS
7	65.5428	8/8/96	1533	ATM	65.5423	8/9/96	1110	RLS	KUMA 4			
8	66.0183	7/10/96	1100	ATM	66.0187	7/25/96	1055	RLS				
9	66.9280	7/8/96	1312	ATM	66.9276	8/9/96	1120	RLS	KUMA #2			
10	66.0862	7/10/96	1111	ATM	66.0860	7/25/96	0933	RLS				
11	65.6989	7/10/96	1108	ATM	65.6989	7/25/96	1020	RLS				
12	BROKEN											

KUMA 2
KUMA 5
BLANK 8/10/96

Checked By: _____ Date: _____ Time: _____

QA REWEIGH

Beaker #	WT	Date	Time	By

BALANCE ROOM ENVIRONMENTAL CONDITIONS

WB	DB	ZRH	Date	Time	By
58	70	47	7/3/96	0953	ATM
60	72	49	7/10/96	1026	ATM
57.5	69	48	8/1/96	0948	ATM

66	70	49	8/8/96	1235	ATM
60	72	49	8/9/96	0745	ATM
64	72	49	8/14/96	1116	ATM

Unit: Kuma Scott HT-1
 Run: 5
 Date: 9/9/96
 Technicians: ATM
 WST20, Form5

Woodstove Particulate
 Catch Processing Sheet
 Woodstove Data Sheet #5
 © EPA M5G-1

Filters

Filter # 136 (R) ✓ Beaker # 5 ✓ Final Wt. 67.2089 g ✓
 Final Wt. .7396 g ✓ Ml 55 Tare Wt. 67.2050 g ✓
 Tare Wt. .7386 g ✓ Desc. Acetone Net Wt. .0039 g ✓
 Net Wt. .0010 g ✓

Filter # 137 (F) Beaker # _____ Final Wt. _____ g
 Final Wt. .7679 g Ml _____ Tare Wt. _____ g
 Tare Wt. .7392 g Desc. _____ Net Wt. _____ g
 Net Wt. .0287 g

Acetone Blank Calculation: Blank done 8/8/96

Blank Beaker # 6 Final Wt. 67.4251
 Ml 140 Tare Wt. 67.4250
 Desc Acetone Net Wt. .0001
.0001 g ÷ 140 ml = .000001 g/ml

Particulate Catch Calculation

Filter: .0010 g ✓
 Filter: .0287 g ✓
 Beakers: .0039 - (.000001) 55 = .0038 g ✓
 Total Catch g/Ml of Acetone
 Blank Value/Ml of Acetone
 Total Catch = .0335 g ✓

Unit SCOTT KUMA 4T-1
 Run # 5
 Date 9/9/96
 Technician ATH, PLS.
 WST6-Form1, Rev11/89

MISCELLANEOUS TEST DATA
 WOODSTOVE DATA SHEET #8

Useable Firebox Dimensions: See QC Section Useable Volume: 1.716 ft³

Dilution Tunnel Draft (If applicable): Start 0 Stop 0

Test Chamber Air Velocity: Start: 0 Stop: 0 Avg: 0

Wet Bulb/ Start: WB: 62 °F DB: 71 °F 1.6 % Amb Moisture 60 %RH

Dry Bulb Stop: WB: 62 °F DB: 73 °F 1.5 % Amb Moisture 53 %RH

$\bar{X} = 1.55$ % Ambient Moisture $\bar{X} = 56.5$ % Relative Humidity (RH)

Empty Stove Wt: 343.1 lbs.

Empty Stove Wt with Stack (Inc. Oil Seal) Wet: 433.1 lbs. Dry: 432.8 lbs.

Empty Stove Wt with Stack and Ash Ash: - lbs. Total: - lbs.

Kindling Wt. Paper: 0.3 lbs. Wood: 4.0 lbs.

Pre Burn Fuel Wt. 10.9 + 11.5 + 12.1 Total: 34.5 lbs.

Total Kindling and Pre Burn Fuel Wt 38.8 lbs.

Coal Bed Wt-lbs: Range (2.7 - 2.2) lbs. Actual: 2.5 lbs.

Allowable Amount of Charcoal that can be removed:

Coal Bed Wt. Range $\frac{435.5}{\text{Upper Wt.}} + \frac{435.0}{\text{Lower Wt.}} \cdot 12 \cdot .25 = \underline{0.6}$ lbs.

Test Fuel Wt-lbs: Ideal 12.0 lbs. Range: 10.9 - 13.2 lbs. Actual: 10.9 lbs.

Test Fuel Size (pcs.) (.75 x 1.5 x 5" Flanges) 14 Pcs.

2 x 4's x 14^{5/16}" 3 Pcs 6.8 lbs. 62.4 %

4 x 4's x 14^{5/16}" 1 Pcs 4.1 lbs. 37.6 %

Est. Dry Burn Rate (Kg/Hr.) $\frac{10.9 - (10.9 \times .18133)}{2.2025} \times \frac{60}{215} = \underline{1.130}$ Est. Dry Burn Rate (Kg/Hr)

Est EPA Heat Output (H_{0E}) (19,140) X $\frac{63}{100} \times \frac{1.130}{1} = \underline{13,621}$ Est Heat Output (H_{0E}) BTU's/Hr

Comments:

STOVE OPERATING DATA
WOODSTOVE TEST DATA SHEET #9

Unit: KUMM SLO# HT-1
Run: 5
Date: 9/9/96
Technician(s): AM RLS
WST3-Form 1 Rev 9/90

Fire Started: 1725 PDST

Warm up and Preburn: Primary Air: Wide open from ignition until the start of the preburn when the primary air control(s) was (were) adjusted to the run setting of 3/8" open on Arc. At the run setting until the start of the test.

3/8" open on arc = stop.

Secondary Air:

No Controls. Naturally drafted.

Secondary Burn/~~By~~Bypass: N/A

Charcoal Bed Preparation: Broke up, raked and leveled the coal bed prior to the addition of each warm up/pre burn fuel charge.

Starting 1:30 before the start of the test, broke up, raked and leveled the coal bed. In stove for 25 seconds.

Test: Door Wide Open during loading _____ min 30 sec, then closed.

Primary Air: Wide open during the start of the test until 4:55. Adjusted to the run setting of 3/8" open on arc between 4:55 and 5:00. At the run setting of 3/8" open on arc at 5:00 into the run.

Secondary Air:

No Controls. Naturally drafted

Secondary Burn/~~By~~Bypass: N/A

Fan: OFF during entire warm up, preburn and test.
FAN Confirmation Test.

Test Run Anomalies:

None.

Unit SCOTT KUMA HT-1
 Run # 5
 Date 9/9/96
 Technician ATH, RLS.
 Page 1 of 3
 WST7-Form2-A, Rev10/88

WOODSTOVE OPERATING DATA
 WOODSTOVE DATA SHEET #9A-1

Wood Data: Kindling: A mix of the below grades

	Size	Mill	Grade	Species
Pre Burn	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
Test Fuel	<u>2x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>
	<u>4x4</u>	<u>R.I.B. LUMBER</u>	<u>#2 STD. & BTR.</u>	<u>D. FIR, S. GRN.</u>

All grades WCLB Rules unless otherwise noted.

Warm up Information:

1st Warm up/Pre Burn Fuel charge (10.9 lbs) added at 1547.
 2nd Warm up/Pre Burn Fuel charge (11.5 lbs) added at 1837.
 3rd Warm up/Pre Burn Fuel charge (12.1 lbs) added at 1932.
 4th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 5th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 6th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 7th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.
 8th Warm up/Pre Burn Fuel charge (_____ lbs) added at _____.

The coals were scooped out of the stove immediately prior to adding the 3rd pre burn/warm up fuel charge. The stove lost 0.3 lbs.

All pre burn/warm up fuel pieces were either 14 or _____ inches long. All preburn pieces/fuel charges were "ricked" in the stove. The pieces in the bottom layer in each rick contained 2 pcs that were 14 inches long and were loaded flat and perpendicular to the door. The pieces in the second layer in each rick were loaded on their side (edge) approximately parallel to the door and contained 4 pcs 14 inches long. The third layer (and fourth layer if present) was loaded flat, perpendicular to the door and contained 2 pcs 14 inches long. The majority of the pieces in each rick were in the second layer which had an approximate 0.5-1.0" space between pieces. (The loading directions indicate the direction of the longest dimension on each piece relative to the loading door opening.) Each pre burn/warm up fuel charge normally weighs within the weight range allowed for the actual test fuel charge

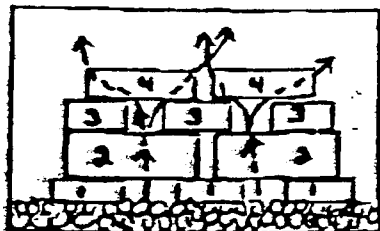
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-2

Unit: SCOTT RWYA HT-1
Run # 5
Date 4/9/96
Technician ATH, PLS
Page 2 of 3
WST7-Form2-A, Rev 6/90

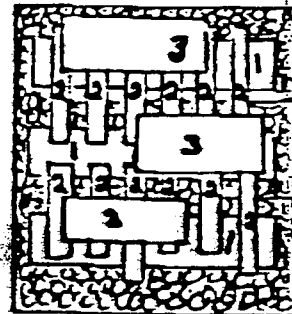
Warm up Information (cont.):

Each warm up/preburn fuel charge was ricked in exactly (as much as possible) the same manner and the weight of each rick was usually within the allowable weight range for the test fuel charge. The physical arrangement and alignment of each rick was designed to accomplish three (3) things: (1) The bottom layer was nestled firmly into the coal bed and was as close to being level with the bottom of the stove as possible, thus providing a stable loading platform for the rest of the rick, keeping it in a ricked state (as opposed to a col-lapsed or fallen down state) until the rick reached the charcoal stage and sags or collapses of its own accord. (2) It enhances the flow of primary air through the ricked preburn fuel charge, for the primary air would flow through the spaces between the pieces in the first layer and then up through the spaces between the pieces in the second, third and, if present, fourth layers. (3) It maximized, as much as possible, the surface to volume ratio of each preburn fuel charge, thereby allowing the fire immediate access to as much wood surface as possible and, thereby, insuring uniform charcoalization. All three of these enhance combustion and so get the stove as hot as possible during the warm up period, thereby maximizing the amount of heat (BTU's) stored in the stove. The actual preburn was not started until the stove surface temperatures had maximized and stabilized, thus indicating that the amount of heat stored in the stove had peaked. For this stove, the thermal storage was monitored using the TOP

surface temperature(s) and the peak value(s) obtained were 915 of.



Front View



Top View

The arrows indicate the direction of the air flow through the rick.

The primary air was adjusted to the run setting of 3/8 open on a 3.0 lbs above the upper charcoal bed weight.

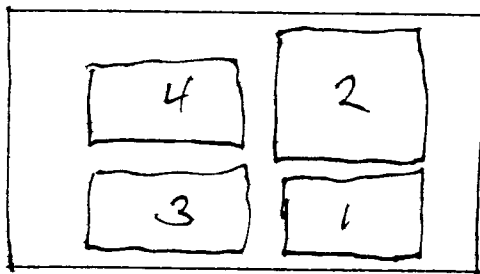
WOODSTOVE OPERATING DATA
WOODSTOVE DATA SHEET #9A-3

Unit SCOTT KUMAH-T-1
Run # 5
Date 9/9/96
Technician ATM, RLS
Page 3 of
WST5-Form2-Rev11/89

Additional Comments: Test Start Sequence: ① opened door ② opened primary air control wide open ③ loaded test fuel charge into the stove ④ photo ⑤ closed door.

Test Fuel Charge Loading Information:

Test Fuel Charge and Loading Sequence Diagram



FRONT of stove view
4 X 4's: 2
2 X 4's: 1, 3 & 4
Loading Sequence: 1, 2, 3 & 4
Driest Pcs in Load 3

Loaded the test fuel charge on an essentially level, large-medium sized, hot coal bed (in appearance, color and temperature for a medium low burn rate. Load 0:30. Ignition 0:35. Vertical column of flame (VC) to baffle 2:20. Secondaries beginning to ignite @ 3:00. Top of pc 2 igniting 3:20. Front tube igniting 3:30. Gas Balance 40:1 @ 5:00 5:00 Primary Air Control → stop Flames decreased. Maintained vertical column of flame (VC) in the center chimney with secondaries at top of VC. Also had a VC on the left side of fuel stack. Never lost gas balance. Low CO₂ 6.6% Hi CO 0.64%.

FUEL MOISTURE
WOODSTOVE TEST DATA SHEET #10

Unit: SCOTT KUMA HT-1

Run: 5

Date: 9/9/96

Technician: ATH, RLS

WST1-Form7-Rev11/89

Room Temperature: 73 °F

Correction Factor: 0

NOTE: Record readings to the nearest 0.5% moisture

Uncor Values are corrected for temperature: Yes No

Time Test Fuel Moisture Readings taken at: 1955 ✓

Calibration Checks: X Y 12.5 12.4 22.0 22.0

Pc #	Dimen	Use	Top		Bottom		Side		Piece Avg Corrected
			Uncor	Cor	Uncor	Cor	Uncor	Cor	
1	2x4x	K	8.0	8.4	8.0	8.4	8.0	8.4	8.400 ✓
2									
3									
4	2x4x8'	P	18.0	19.2	18.0	19.2	18.0	19.2	19.200 ✓
5	"	P	18.0	19.2	18.0	19.2	18.5	19.8	19.400 ✓
6	"	P	22.0	23.7	22.0	23.7	22.5	24.3	23.900 ✓
7									62.500 ✓
8									
9									
10	2x4x14 5/16"	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200 ✓
11	"	T	21.5	23.1	22.5	24.3	22.0	23.7	23.700 ✓
12	"	T	22.5	24.3	22.5	24.3	22.5	24.3	24.300 ✓
13									
14	4x4x14 5/16"	T	20.0	21.4	20.0	21.4	20.0	21.4	21.400 ✓
15									88.600 ✓
16									
17									
18									
19	FEET	T	18.0	19.2	18.0	19.2	18.0	19.2	19.200 ✓
20									OUT SPACERS

	Kindling	Pretest Fuel	Test Load
% Moisture - Dry Basis:	8.400% ✓	20.833% ✓	22.150% ✓
% Moisture - Wet Basis:	7.749% ✓	17.241% ✓	18.133% ✓

To obtain Wet from Dry: $\frac{100 \times \% \text{ Dry Rdg.}}{100 + \% \text{ Dry Rdg.}} = \% \text{ Moisture, Wet Basis}$

Acceptable Ranges: 16-20% wet; 19-25% dry
(17.5 - 22.5 on Meter [Uncor reading] at 70°F)

Key for Use: K= Kindling P= Pretest Fuel T= Test Fuel

WOOD DENSITY DETERMINATION
WOODSTOVE TEST DATA SHEET #11

Unit: Kuma Scott HT-1
Run#: 5
Date: 9/9/96
Technician: ATM
WST2-form11-Rev 6/90

Wood Piece: Nominal Dimensions: 3 1/2" x 3 1/2" x 1 1/2"
Depth (D): IN 1.560 cm 3.9624 ✓
Width (W): IN 3.592 cm 9.1237 ✓
Length (L): 3.582 cm
3.585 cm
3.560 cm
3.587 cm
Length \bar{X} = IN 3.5785 cm 9.0894 ✓
Volume: 328.597 cm³ ✓
(D X W X L)

MOISTURE: Room Temperature: 73 °F Correction Factor: 0

Uncorrected Meter Readings Corrected for temperature: Yes No

NOTE: Record moisture meter readings to the nearest 0.5%

	Uncor	Cor	%
Top:	<u>22.5</u>	<u>24.3</u>	<u>%</u>
Bottom:	<u>22.5</u>	<u>24.3</u>	<u>%</u>
Side:	<u>22.5</u>	<u>24.3</u>	<u>%</u>
\bar{X} :		<u>24.300</u>	<u>%</u>

Avg % Moisture (Dry) 24.300 % ✓

Avg % Moisture (Wet) 19.549 % ✓

Scale: Leveled In Out

Zeroed: In Out

Wet Weight: 209.5 g Dry Weight: 167.3 g

% Moisture Dried Basis: 20.143 % ✓
[1 - (Dry Wt - Wet Wt)] X 100

Into Dryer Date 9/9/96 Time 2100 Temp 215 °F
Out of Dryer Date 9/11/96 Time 2000 Temp 200 °F

(Minimum Time in Dryer: 24 hrs.) Minimum Dryer Temp 100°C (212°F)

Density = 167.3 g (dry wt) ÷ 328.597 cm³ (volume) = .5091 ✓ g/cm³

Pellet Fuel Moisture Content Determination

Tare Beaker Wt. _____ g
Wet Wt: _____ g - _____ g = _____ g
Gross Wet Wt. Tare Beaker Wt. Net Wet Wt.
Dry Wt: _____ g - _____ g = _____ g
Gross Dry Wt. Tare Beaker Wt. Net Dry Wt.

% Moisture Dried Basis: _____ %
[1 - (Net Dry Wt ÷ Net Wet Wt.)] X 100

Minute	Scale Wt	Ibs left	Burn Rate	CO2		O2		T/C(1)T/C(2)		T/C(3)		SO2 v.	PPM	Static Press.	Comments	
				v.	%CO2	v.	%O2	Wet Bulb	Dry Bulb	% H2O	Calc W/B					Stack
0	446.2	10.9	0	1255	6.37	55.0	13.7	0.97	6.6	78	99	2.5	106	256	7046	Flow
5	445.3	10.0	.9	1233	5.83	54.1	13.5	0.56	10.4	81	112	2.5	113	353	7078	SO2 1.5
10	444.9	9.6	1.4	1263	6.57	55.7	13.9	0.62	10.6	93	126	4.1	119	336	7062	SO2 1.5
15	444.4	9.1	1.5	1227	10.6	37.4	9.33	0.16	66.4	100	132	5.4	124	357	7068	SO2 1.5
20	443.8	8.5	1.6	1443	11.0	38.6	9.63	0.23	47.9	106	135	6.6	128	373	7070	SO2 1.5
25	443.2	7.9	1.6	1467	11.7	36.5	9.10	0.18	64.5	109	135	7.6	130	384	7071	
30	442.6	7.3	1.6	1521	12.9	31.2	7.78	0.12	107.9	110	136	7.8	132	392	7071	
35	442.0	6.7	1.6	1577	12.8	31.7	7.91	0.21	61.2	111	137	7.9	132	387	7070	
40	441.5	6.2	1.5	1545	13.5	28.9	7.21	0.34	39.8	111	136	8.0	132	389	7070	
45	440.9	5.6	1.6	1571	14.2	26.2	6.54	0.33	43.0	110	135	7.8	132	393	7070	
50	440.5	5.2	1.4	1505	12.5	34.4	8.58	0.20	62.7	108	130	7.6	131	380	7068	
55	440.1	4.8	1.4	1388	9.66	43.3	10.8	0.75	12.9	105	123	6.9	127	349	7064	
60	439.8	4.5	1.3	414	10.3	40.6	10.1	0.62	16.6	102	120	6.1	125	345	7064	Flow
65	439.5	4.2	1.3	407	10.1	41.3	10.3	0.62	16.3	99	116	5.7	122	332	7062	SO2 1.5
70	439.1	3.8	1.4	378	9.41	44.0	11.0	0.75	12.5	97	113	5.4	121	323	7059	SO2 1.5
75	438.9	3.6	1.2	344	8.57	47.0	11.7	0.82	10.4	95	110	5.0	120	311	7057	SO2 1.5
80	438.6	3.3	1.3	321	8.00	49.3	12.3	0.83	9.6	93	107	4.8	118	302	7056	
85	438.4	3.1	1.2	304	7.58	51.1	12.7	0.87	8.7	91	105	4.4	115	295	7055	
90	438.2	2.9	1.2	278	6.94	53.3	13.3	1.02	6.8	90	103	4.3	114	279	7057	
95	438.0	2.7	1.2	264	6.59	54.7	13.6	1.08	6.1	89	101	4.2	112	270	7050	
100	437.8	2.5	1.2	245	6.12	56.2	14.0	1.20	5.1	87	100	3.8	111	264	7049	
105	437.7	2.4	1.1	246	6.15	56.3	14.0	1.08	5.7	87	98	3.9	110	259	7048	
110	437.5	2.2	1.2	252	6.29	55.5	13.8	1.05	6.0	86	98	3.7	109	254	7046	
115	437.3	2.0	1.2	257	6.27	55.7	13.9	1.09	5.8	86	98	3.7	108	250	7046	
120															1643	

Unit: SCOTT KUMA HT-1
 Job: 5
 Page: 2 of 2

Date: 9/9/96
 Technician(s): ATH, RLS.

Minute Time	Scale Wt	lbs left	Burn Rate	CO2		O2		T/C(1) T/C(2)		T/C(3)		SO2 v.	Static Press.	Comments
				v.	%CO2	v.	%O2	Wet Bulb	Dry Bulb	% H2O	Calc W/B			
120	435.1	1.8	1.2	26.2	6.54	54.6	13.6	85	98	3.6	108		-0.446	Flow
125	436.9	1.6	1.2	28.7	7.16	52.0	13.0	85	99	3.6	109		-0.446	SO2 1.5
130	436.8	1.5	1.1	31.2	7.77	49.8	12.2	86	100	3.6	109		-0.447	CO2 1.5
135	436.6	1.3	1.2	32.4	8.07	48.5	12.1	86	100	3.6	110		-0.447	CO2 1.5
140	436.4	1.1	1.2	26.6	6.64	53.3	13.3	86	97	3.7	109		-0.446	CO2 1.5
145	436.3	1.0	1.1	23.2	5.80	55.9	13.9	85	95	3.7	108		-0.444	
150	436.2	1.9	1.1	21.7	5.43	57.2	14.3	84	91	3.7	108		-0.443	
155	436.1	1.8	1.1	20.8	5.21	58.0	14.5	82	91	3.4	106		-0.442	
160	436.1	1.8	0	20.9	5.23	58.0	14.5	82	89	3.4	106		-0.441	
165	436.0	1.7	1.1	20.1	5.03	58.6	14.6	81	89	3.3	105		-0.441	
170	435.9	1.6	1.1	20.1	5.03	59.0	14.7	80	88	3.2	105		-0.440	
175	435.8	1.5	1.1	19.0	4.76	59.8	14.9	80	87	3.2	104		-0.440	
180	435.8	1.5	0	18.6	4.66	60.3	15.0	79	87	3.1	103		-0.523	Flow
185	435.7	1.4	1.1	18.4	4.61	60.6	15.1	78	87	3.0	103		-0.440	SO2 1.5
190	435.6	1.3	1.1	18.0	4.52	60.9	15.2	78	87	3.0	103		-0.440	CO2 1.5
195	435.6	1.3	0	17.5	4.39	61.2	15.4	78	86	3.0	103		-0.440	CO2 1.5
200	435.5	1.2	1.1	17.3	4.34	61.7	15.4	78	87	3.0	103		-0.039	
205	435.4	1.1	1.1	17.3	4.34	61.8	15.4	77	87	2.8	102		-0.039	
210	435.4	1.1	0	17.0	4.27	62.1	15.5	77	87	2.8	102		-0.037	
215	435.3	0	1.1	16.8	4.22	62.4	15.6	77	87	2.8	102		-0.037	
220													-0.310	
225														
230														
235														
240														
245														
250														

435.3

44.5

12.451

283

2.284

7.052

TEMPERATURES
RECORD SHEET #14
WST2-Form14 Rev7/96

U: SCOTT KUMAR HT-F
R: 5 of 2
Page: 1 of 2

Date: 9/19/96
Technician(s): ATH, R. S.

T/Off	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Minute	Stove Top	Left Side	Back Side	Right Side	Bottom	Firebox	2nd Burn	Room Temp.	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con-	dar
0	380	467	297	438	421	825	831	70	90	248	36	74	35		
5	403	466	294	438	395	923	1202	67	109	247	36	77	34		
10	471	462	286	427	404	796	860	66	98	248	36	77	34		
15	536	454	279	411	399	808	888	66	95	248	36	76	34		
20	587	446	272	396	390	857	987	66	97	248	36	75	34		
25	615	440	265	386	380	894	1034	68	98	248	36	76	34		
30	638	437	260	379	376	944	1193	70	99	248	36	76	34		
35	655	439	257	375	368	927	1260	70	99	247	36	76	35		
40	662	442	256	376	365	921	1295	71	99	248	36	76	34		
45	667	443	256	381	360	934	1327	71	100	248	36	77	35		
50	638	446	258	388	360	937	1325	71	99	248	36	77	34		
55	578	447	259	393	362	895	1321	71	98	248	36	77	34		
	(6830)	(5389)	(3234)	(4788)	(4580)	(10,655)	(13,593)	(827)	✓						
60	555	447	260	396	363	897	1343	71	97	248	36	77	34		
65	520	447	261	398	365	894	1303	71	96	248	36	77	34		
70	503	446	262	401	366	881	1307	70	95	247	36	77	34		
75	481	445	263	402	368	864	1196	70	94	247	36	77	34		
80	467	444	263	404	369	857	1139	70	94	248	37	77	35		
85	457	441	263	405	370	842	1025	70	93	248	37	77	34		
90	433	437	262	405	370	835	983	70	92	248	37	77	34		
95	419	434	262	404	373	820	922	70	91	248	37	77	35		
100	407	430	262	401	374	806	889	70	90	248	37	77	35		
105	395	424	262	399	375	795	886	69	90	247	37	76	35		
110	383	420	261	397	374	772	900	69	89	248	37	76	35		
116	373	416	261	395	373	759	917	69	89	248	37	76	35		
	(5387)	(5331)	(3142)	(4802)	(4440)	(10,010)	(12,810)	(839)	✓						
	12,217	10,620	6576	9595	9020	20,665	26,333	1666							

T/C#	Minute	Stove Top	Left Side	Back	Right Side	Bottom	Firebox	2nd Burn	Room Temp	Tunnel	C. Gas Box	Impinger Out	5G-1 Filter	5G-1 Condenser	Con- dar
120	25	366	411	261	394	371	755	949	69	89	248	37	76	35	
125	30	369	408	262	396	368	758	966	69	88	248	37	76	35	
130	35	376	404	264	398	365	765	983	69	88	248	36	75	35	
135	40	385	401	266	403	362	763	993	70	88	248	36	76	35	
140	45	380	398	270	407	362	740	944	72	88	248	36	75	35	
145	50	369	397	272	411	364	727	879	72	87	248	36	75	35	
150	55	358	395	273	415	365	713	850	73	87	247	36	75	35	
155	2400	349	393	272	418	364	698	829	73	86	248	37	75	35	
160	05	342	390	271	420	364	681	818	73	86	247	37	75	35	
165	10	336	387	270	423	366	671	808	73	85	247	36	75	35	
170	15	330	384	270	427	365	674	796	73	85	247	36	75	35	
175	20	325	381	269	430	364	669	779	73	85	248	35	75	35	
180	25	321	378	269	432	365	656	769	73	83	248	35	75	35	
185	30	316	374	268	433	362	647	761	72	84	248	35	75	35	
190	35	311	370	267	433	363	635	752	73	84	248	35	75	35	
195	40	307	366	266	432	363	626	741	72	84	248	35	74	35	
200	45	303	361	265	430	361	613	732	72	83	248	35	74	35	
205	50	300	357	264	428	360	603	726	73	83	248	35	74	35	
210	55	297	352	263	425	359	599	718	73	83	248	35	74	35	
215	0100	295	349	261	421	357	589	707	72	83	248	36	74	35	
220	05	2450	290	213	343	2890	4968	5906	580						
225	10														
230	15	18952	18276	1179	1797	16290	34247	49833	3105		441		START	399.6	
235	20												FINISH	336.6	
		431	415	266	408	370	778	973	71				ΔT=	-63.0	

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-1

Site: Myren Consulting, Woodinville, WA Date: 9/9/96 Analyte: CO₂

Source: SCOTT KILMA HT-1 Run #: 5

Zero Cyl #: 4-36919 Conc. 00.0 % CO₂ Cyl Press: 1975 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W 260657 Conc. 10.1 % CO₂ Cyl Press: 920 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Horiba Model: PIR-2000 SN: 607024

Range: 0 - 25.0% CO₂ Analyzer Output: 0 - 1.0 v.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% CO₂

EPA Control Limits = + 2.5% of 25.0% CO₂ = + 0.625% CO₂

Pre Run Audit: By: A.T. Myrum Time: 2015 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.4	.404	10.1	40.5	.405	10.0759	-.0241	-0.24

Comments:

Post Run Audit: By: A.T. Myrum Time: 0040 Temp: 72 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	.000	00.0	00.0	.000	.0666	.0666	0.27
Span	40.4	.404	10.1	40.5	.405	10.0759	-.0241	-0.24

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-2

Site: Myren Consulting, Woodinville, WA Date: 9/9/96 Analyte: O₂

Source: SCOTT KUMA HT-1 Run #: 5

Zero Cyl #: 4-36919 Conc. 00.0 % O₂ Cyl Press: 197.5 psi

Certified by: Canode Airgas Date: 4/24/96

Span Cyl #: W260 657 Conc. 0 % O₂ Cyl Press: 920 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Taylor Model: OA 137 SN: 137/4772

Range: 0 - 25.0% O₂ Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 25.0% O₂

EPA Control Limits = + 2.5% of 25.0% O₂ = + 0.625% O₂

Pre Run Audit: By: A. Myren Time: 2015 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.5	00.2	0.552	0.552	0.22
Span	12.5	500	12.5	12.6	50.0	12.467	-0.0326	-0.26

Comments:

Post Run Audit: By: A. Myren Time: 0040 Temp.: 72 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ%
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.5	00.2	0.552	0.552	0.22
Span	12.5	500	12.5	12.6	50.1	12.492	-0.0077	-0.06

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

PRE AND POST TEST ZERO/SPAN CHECK
WOODSTOVE DATA SHEET #15-3

Site: Myren Consulting, Woodinville, WA Date: 9/9/96 Analyte: CO

Source: SCOTT KUMA HT-1 Run #: 5

Zero Cyl #: 4-36919 Conc. 00.0 % CO Cyl Press: 1975 psi

Certified by: Cascade Airgas Date: 4/24/96

Span Cyl #: W260 657 Conc. 2.47 % CO Cyl Press: 920 psi

Certified by: BOC Gases Date: 1/18/95

Analyzer: Make: Infra Red Model: 702 D SN: 113

Range: 0 - 10.0% CO Analyzer Output: 0 - 100 mv.

Flow: 1.5 SCFH Measured by: Rotameter: X Flowmeter:

EPA Span Value = 5.0% CO

EPA Control Limits = +2.5% of 5.0% CO = + 0.125% CO

Pre Run Audit: By: A.T. Myren Time: 2015 Temp: 77 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.3	-0.062	-0.062	-0.12
Span	2.47	49.4	2.47	2.48	49.4	2396	-0.0745	-3.01

Comments:

Post Run Audit: By: A.T. Myren Time: 0040 Temp.: 72 °F

Audit Results

Point #	Expected Response			Actual Response			+ Conc. Difference	Δ %
	Meter	DVM	%	Meter	DVM	%		
Zero	00.0	00.0	00.0	0.00	-00.3	-0.062	-0.062	-0.12
Span	2.47	49.4	2.47	2.49	49.7	2410	-0.0600	-2.43

Comments:

+ Conc. Difference = Act % - Exp (Std) %

Zero % Differece = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Full Scale Value}} \times 100$

Span % Difference = $\frac{\text{Act \% (ppm)} - \text{Exp \% (ppm)}}{\text{Exp \% (ppm)}} \times 100$

Unit: SCOTT KUWA HT-1
 Run: 5
 Date: 9/9/96
 Technicians: ATM, RLS
 WST6-Form3-Rev11/89

QUALITY CHECKS
 WOODSTOVE DATA SHEET #16

Ambient = Tr: 73 °F T/C#30: _____ °F
 Thermocouple Check (at ambient): T/C#1: 73.2 °F; T/C#2: 73.6 °F;
 T/C #3: 73.6 °F; T/C #4: 73.6 °F; T/C #5: 76.4 °F;
 T/C #6: 71.6 °F; T/C #7: 71.8 °F; T/C #8: 71.8 °F;
 T/C #9: 75.8 °F; T/C #10: 72.0 °F; T/C #11: 72.4 °F;
 T/C #12: 73.2 °F; T/C #13: 73.4 °F; T/C #14: 73.2 °F;
 T/C #15: 72.8 °F; T/C #16: 72.2 °F; T/C #17: _____ °F;
 T/C #18: _____ °F; T/C #19: _____ °F; T/C #20: _____ °F;
 T/C #21: _____ °F; T/C #22: _____ °F; T/C #23: _____ °F;
 T/C #24: _____ °F; T/C #25: _____ °F; T/C #26: _____ °F;

Comments: _____

Thermocouple Readout: Pretest Zero/Span Check and Calibration:
 Zero (0°F) : 0.2 °F Adj to: 0.0 °F Post Test Check Zero (0°F): 0.2 °F % Difference +0.01
 Span (2000°F): 1999.8 °F Adj to: 2000.0 °F Span (2000°F): 2000.4 °F +0.02

(Allowable % Difference = 1.5%. Use formulas on Woodstove Data Sheet #15 to calculate % Difference)

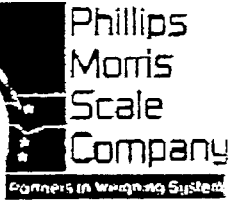
Thermocouple Readout Pretest Linearity Check
 0°F = 0.0 °F; 200°F = 201.8 °F; 400°F = 398.6 °F;
 600°F = 601.2 °F; 800°F = 800.6 °F; 1000°F = 1000.4 °F;
 1200°F = 1198.4 °F; 1400°F = 1399.4 °F; 1600°F = 1598.8 °F;
 1800°F = 1799.6 °F; 2000°F = 2000.0 °F

Combustion Gas (CO₂, O₂, CO) Train Leak Check: Pre OK Post OK
 Draft (Static) Gauge Zero Check: Pre OK Post OK

Scale Check Pre (Wt, #'s): 433.1 - 438.1 5.0 lbs, OK (RLS)
 Post (Wt, #'s): 435.1 - 440.1 5.0 lbs, OK (RLS)

Stack cleaned prior to the run: Yes _____ No ✓
 Tunnel cleaned prior to the run: Yes _____ No ✓

INSPECTION CERTIFICATE



CUSTOMER: Myren Consulting
 ADDRESS: 12810 N.E. 78th #106
Woodinville Wa
 TECHNICIAN: ART Hall
 AUTHORIZATION SIGNATURE: _____

DATE OF INSPECTION: 4-11-96
 NEXT INSPECTION DUE: 10-11-96
 CERTIFICATION TYPE
 _____ STANDARD
 ISO 9000
 _____ MIL STD-45662

934 Elliott Avenue W.
 Seattle, WA 98119
 Ph#(206)284-6090
 Fax#(206)282-6612

EQUIPMENT TESTED

INDICATOR	BASE	OPTIONS INSTALLED
MAKE <u>Digi</u>	<u>Digi</u>	PRINTER _____
MODEL <u>DI10</u>	<u>Remote</u>	SCORE BOARD _____
SR# <u>881165</u>	_____	COMPUTER _____
CLASS <u>II</u>	<u>III</u>	OTHER _____
CAP. <u>1000LB</u>	<u>1000LB</u>	
PRE-TEST	POST-TEST	MANUFACTURER TOLERANCE
<u>50 + 1</u>	<u>50 +/- 0</u>	<u>1.00190</u>
<u>100 + 1-2</u>	<u>100 +/- 0</u>	_____
<u>150 + 2</u>	<u>200 +/- 0</u>	_____
<u>200 + 3</u>	<u>500 +/- 0</u>	_____
_____	<u>1000 +/- 1</u>	_____
_____	<u>0</u>	_____
CORNER TEST	P <input checked="" type="checkbox"/> F _____	
SHIFT TEST	P <input checked="" type="checkbox"/> F _____	
STATIC TEST	2 MIN. <input checked="" type="checkbox"/> 5 MIN. _____	
WEIGHT KIT# <u>TRK #10</u>	NIST# <u>822/250904</u>	
	<u>STATE TEST NO, A 0353</u>	
SERIAL NUMBERS OF WEIGHTS USED (OR COPY OF CERTIFICATE)		
<u>R133/50</u>	<u>R137/50</u>	_____
<u>R134/50</u>	<u>WA105-3/500LB</u>	_____
<u>R135/50</u>	<u>WA106-0/500LB</u>	_____
<u>R136/50</u>	_____	_____

QUALITY CONTROL SERVICES

LABORATORY AND METROLOGY EQUIPMENT: SALES AND SERVICE

DATE: April 18, 1996

CUSTOMER: Myren Consulting
12810 NE 178th
Woodinville, WA 98072
Attn: Ben Myren

WEIGHT TRACEABILITY CERTIFICATE

THE BALANCES/SCALES LISTED BELOW HAVE BEEN SERVICED AND CALIBRATED BY QUALITY CONTROL SERVICES.

THIS DOCUMENT CERTIFIES THAT THE TEST WEIGHTS USED ARE TRACEABLE TO THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (N.I.S.T.) UNDER TEST # 822/251337.

QCS Weight Set I.D. Number	Calibration Date	Next Calibration Due
A45	07-08-95	07-96
AW8543	08-16-95	08-96
AW2902	08-16-95	08-96
AW5735	08-16-95	08-96

DATE OF SERVICE	TYPE	MAKE	SERIAL NUMBER	TECHNICIAN
04-16-96	AE100	Mettler	K04827	R. Beier
04-16-96	HR200	A&D	12301167	R. Beier

AUTHORIZED REPRESENTATIVE: R. Beier

WOODSTOVE DATA SHEET #33

w/ Floke (Rendool)

Thermocouple Calibration Record

TC #	Location	Ice Water Bath (°F)	Boiling Water (°F)	TC #	Location	Ice Water Bath (°F)	Boiling Water (°F)
1	Wet Bulb	32.3	210.9	21			
2	Dry Bulb	32.4	210.4	22			
3	Stack	32.5	210.4	23			
4	Stove Top	32.3	210.5	24			
5	Left Side	32.4	210.8	25			
6	Back	32.4	210.7	26			
7	Right Side	32.6	210.5	27			
8	Bottom	32.7	210.1	28			
9	Firebox	32.9	210.0	29	Oven		
	2nd Burn			30	N/A-Calibrator		
10	Catalytic	32.0	209.9	31			
11	Room	32.8	210.0	32			
12	TNL TEMP Tube Furnace	33.1	210.1	33			
13	HOT (C Gas) Sample Box	33.0	209.8	34			
14	C Gas Impinger Out	32.8	209.8	35	Rear Top		
15	Filter #1 Gas Box	32.9	210.1	36	Rear L Side		
16	Cond. #1 C Gas Out	32.9	210.6	37	Rear R Side		
17	Filter #2 Gas Out	32.7	210.7	38	Rear Firebox		
18	Extra Cond. #2	32.6	210.9	39	Rear 2nd/cat		
19	Extra			40			
20	Extra						

Thermocouples checked against

Reference Thermometer #: NBSIce Water Bath 32.1 °FBoiling Water 211 °FRoom Temp 71 °FB.P. 30.02 "HgDate: 4/17/96 Technician: A.T. Mullen

Date: 4/18/96
 Ambient Temperature: 71 °F
 Calibrator: A.T. Mysen

Thermocouple No.: 40
 Barometric Pressure: 30.02 "Hg
 Reference: Mercury-in-glass: _____

Other: Altec
Remount Calibration

Fluke REMOUNT SN 6120410

Reference point No. ^a	Source ^b (specify)	Reference thermometer temperature, °F	Thermocouple potentiometer temperature, °F	Difference, % ^c
0	Altec		0.0	0
200			202.1	+0.32
400			399.9	-0.01
600			601.6	+0.15
800			800.2	+0.02
1000			1000.8	+0.05
1200			1199.1	-0.05
1400			1400.4	+0.02
1600			1599.0	-0.05
1800			1799.7	-0.01
2000			2000.0	0.0

^a Every 300C (500F) for each reference point
^b Type of Calibration system used
^c $(\text{Ref. temp. } ^\circ\text{C} + 273) - (\text{Test therm. temp. } ^\circ\text{C} + 273) \times 100 / 1.5 \times \text{Ref. Temp. } ^\circ\text{C} + 273$

Date: 8/11/11
 P. 11.00

Thermometer ID

ERTCO ERTCO
 Cat 1005-3FC Cat 517
 SN 16917 KBS-163
 -1 to +101°C 0-260°C
 0.1° 1°

VWR
 C1016-015 U.A.
 -30° - +50°C
 1°

Fisher
 A511.54F
 A04544
 0-180°F
 1°

Thermometer ID

Mfr.
 Cat #
 S/N
 Range
 Graduations
 Temp PT

ERTCO
 1005-3FC
 16917
 -1 to +101°C
 0.1°

ERTCO
 517
 KBS-163
 0-260°C
 1°C

VWR
 C1016-015 U.A.
 -30 to +50°C
 1°C

Fisher
 A511.54F
 A04544
 0-180°F
 1°F

1	21.5°C	23°C	21.5	70°F
2	19.4°C	21°C	19.5	67
3	13.2°C	15°C	13.5	56
4	0.6	4°C	1.1	33.5
5	40	41.5	40	105
6.	99	99		

Mfr.
 Cat #
 S/N
 Range
 Graduations
 Temp #

Taylor
 1330NA
 WB
 20-100°F
 1°F

Taylor
 1330NA
 DB
 20-100°F
 1°F

Reinew
 Instruments
 AI
 0-220°F
 1°F

Weston
 model
 -40-160°F
 2°F

1	70°F	69.5	61.5	69.5
2	66	66	58	66
3	55	55.5	46	56
4	33	33	23	33
5	104	109	95 199	105

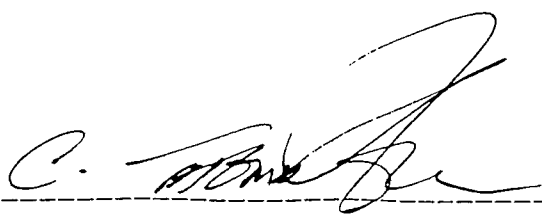
R E P O R T O F C A L I B R A T I O N

LIQUID-IN-GLASS-THERMOMETER

THE THERMOMETER WAS TESTED IN A LARGE, CLOSED-TOP, ELECTRICALLY HEATED, LIQUID BATH, BEING "IMMERSED" 76MM. THE TEMPERATURE OF THE ROOM WAS ABOUT 25 DEGREES C (77 DEGREES F). IF THE THERMOMETER IS USED UNDER CONDITIONS WHICH WOULD CAUSE THE AVERAGE TEMPERATURE OF THE EMERGENT LIQUID COLUMN TO DIFFER MARKEDLY FROM THAT PREVAILING IN THE TEST, APPRECIABLE DIFFERENCES IN THE INDICATIONS OF THE THERMOMETER WOULD RESULT.

THE TABULATED CORRECTIONS APPLY PROVIDED THE ICE-POINT READING, TAKEN AFTER EXPOSURE FOR NOT LESS THAN 3 DAYS TO A TEMPERATURE OF ABOUT 20 DEGREES C (70 DEGREES F) IS 0.00 DEGREES C. IF THE ICE-POINT READING IS FOUND TO BE HIGHER (OR LOWER) THAN STATED, ALL OTHER READINGS WILL BE HIGHER (OR LOWER) TO THE SAME EXTENT. IF THE THERMOMETER IS USED AT A GIVEN TEMPERATURE SHORTLY AFTER BEING HEATED TO A HIGHER TEMPERATURE. AN ERROR OF 0.01 DEGREES OR LESS, FOR EACH 10 DEGREE DIFFERENCE BETWEEN THE TWO TEMPERATURES, MAY BE INTRODUCED. THE TABULATED CORRECTIONS APPLY IF THE THERMOMETER IS USED IN THE UPRIGHT POSITION; IF USED IN A HORIZONTAL POSITION, THE INDICATIONS MAY BE A FEW HUNDREDTHS OF A DEGREE HIGHER.

TEST NUMBER: 152439
DATE: 07/16/96
STANDARD SERIAL NO. 128239
NIST IDENTIFICATION NO. 88024



Charles Tang-Nian
QUALITY CONTROL MANAGER

R E P O R T O F C A L I B R A T I O N

LIQUID-IN-GLASS-THERMOMETER

CALIBRATED BY EVER READY THERMOMETER CO.

MARKED: ERTCO CAT 1005-3FC S/N-1697

RANGE: -1 TO +101 DEGREES C IN 0.1 DEGREE GRADUATIONS.

THERMOMETER READING	CORRECTION (ITS-90)**
0.00 C	0.00 C
10.00	0.00
20.00	0.00
30.00	0.00
37.00	0.00
40.00	0.00
50.00	0.00
56.00	0.00
60.00	0.02
70.00	0.00
80.00	0.00
90.00	0.00
100.00	0.00

** ALL TEMPERATURES IN THIS REPORT ARE BASED ON THE INTERNATIONAL TEMPERATURE SCALE OF 1990 (ITS-90) PUBLISHED IN THE METROLOGIA 27, NO. 1, 3/10/90.

THIS THERMOMETER WAS CALIBRATED AGAINST A STANDARD CALIBRATED AT THE NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY (NIST) FORMERLY THE NATIONAL BUREAU OF STANDARDS (NBS) IN ACCORDANCE WITH ASTM METHOD E 77, AND NBS MONOGRAPH 174.

FOR A DISCUSSION OF ACCURACIES ATTAINABLE WITH SUCH THERMOMETERS SEE NBS MONOGRAPH 250-23.

IF NO SIGN IS GIVEN ON THE CORRECTION, THE TRUE TEMPERATURE IS HIGHER THAN THE INDICATED TEMPERATURE; IF THE SIGN GIVEN IS NEGATIVE, THE TRUE TEMPERATURE IS LOWER THAN THE INDICATED TEMPERATURE. TO USE THE CORRECTIONS PROPERLY, REFERENCE SHOULD BE MADE TO THE NOTES GIVEN BELOW.

CONTINUED

TEST NUMBER: 152439
DATE: 07/16/96
STANDARD SERIAL NO. 128239
NIST IDENTIFICATION NO. 88024

MYREN CONSULTING
 EPA METHOD 5
 METER BOX PRE TEST 5 POINT CALIBRATION
 English Meter Box and English Calibration Meter Units

Filename: C:\WINDOWS\DESKTOP\DAW\SU-1\DGMCAL1.WK1

Model Number: 45G-P Date: -> April 18, 1996
 Serial Number: 1 Barometric Pressure: -> 29.81 (in. Hg)
 Calibration Meter Factor Yc: -> 0.9903 (number)

dH (in H2O)	Elapsed Time (min)	DRY GAS METER READING			GAS			CALIBRATION METER READINGS			CALIBRATION METER	
		Volume Initial (cu ft)	Volume Final (cu ft)	Volume Total (cu ft)	Temperature Inlet (deg F)	Temperature Outlet (deg F)	Volume Initial (cu ft)	Volume Final (cu ft)	Volume Total (cu ft)	Temperature Inlet (deg F)	Temperature Outlet (deg F)	
0.25	31.47	446.100	451.712	5.612	Initial-> Final---->	70.0 79.0	70.0 79.0	418.254 423.927	423.927 5.673	73.0 73.0	73.0 73.0	
0.50	19.87	452.202	457.401	5.199	Initial-> Final---->	80.0 83.0	80.0 83.0	424.428 429.639	429.639 5.211	73.0 73.0	73.0 73.0	
0.75	13.00	458.001	464.000	5.999	Initial-> Final---->	82.0 84.0	82.0 84.0	430.231 436.251	436.251 6.020	73.0 73.0	73.0 73.0	
1.00	17.84	464.701	474.501	9.800	Initial-> Final---->	84.0 85.0	84.0 85.0	436.968 446.836	446.836 9.868	73.0 73.0	73.0 73.0	
1.25	8.55	474.901	480.004	5.103	Initial-> Final---->	85.5 86.0	85.5 86.0	447.238 452.401	452.401 5.164	73.0 73.0	73.0 73.0	

DRY GAS METER
 METER CALIBRATION FACTOR

Value (number)	Variation (number)
1.003	-0.009
1.007	-0.005
1.011	-0.001
1.016	0.004
1.023	0.011
Average	1.012

DRY GAS METER
 ORIFICE CALIBRATION FACTOR

Value (in H2O)	Variation (in H2O)
4.434	1.566
4.136	1.268
1.984	-0.883
1.849	-1.018
1.935	-0.933
Average	2.867

Note: For Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptable tolerance of individual values from the average is ± 0.02 .

For Orifice Calibration Factor dH_0 , the orifice differential pressure in inches of H2O that equates to 0.75 cfm of air at 68 F and 29.92 inches of Hg, acceptable tolerance of individual values from the average is ± 0.2 .

I certify that the above Dry Gas Meter was calibrated in accordance with E.P.A. Method 5, paragraph 7.1; CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3785, certificate # F107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature: Albert J. Myren Jr. Date: 4/18/96

METER BOX CALIBRATION AUDIT

Run #	Test Data									
	1	2	3	4	5	6	7	8	9	10
Avg. ΔH	.886	.877	.884	.882	.882					
Max Vac	0	0	0	0	0					
Avg. Test Series ΔH : <u>.8822</u> in H ₂ O. Test Series Max Vac: <u>0</u> in Hg										

Audit Dry Gas Meter: MC-1 300332 Correction (Y) Factor: 0.9903
 Test Dry Gas Meter: 45G-P Correction (Y) Factor: 1.012

Audit Data

	Audit #1	Audit #2	Audit #3
BP:	<u>29.88</u>	<u>29.88</u>	<u>29.88</u>
Vac:	<u>0</u>	<u>0</u>	<u>0</u>
Audit Meter:			
Final Vol	<u>624.719</u>	<u>630.221</u>	<u>635.798</u>
Initial Vol	<u>619.745</u>	<u>625.015</u>	<u>630.635</u>
Vol (V _w , ft ³)	<u>4.974</u> ✓	<u>5.206</u> ✓	<u>5.163</u> ✓
Audit Meter:			
Initial	<u>78</u>	<u>77</u>	<u>76</u>
Temp (°F)(T _w)			
Mid	<u>78</u>	<u>77</u>	<u>76</u>
Final	<u>77</u> ✓	<u>76</u> ✓	<u>76</u>
Avg (°F/°A)	<u>(77.67) 537.67</u>	<u>(76.67) 536.67</u>	<u>(76) 536</u> ✓
ΔH (in H ₂ O)			
Initial	<u>.88</u>	<u>.88</u>	<u>.88</u>
Mid	<u>.88</u>	<u>.88</u>	<u>.88</u>
Final	<u>.88</u>	<u>.88</u>	<u>.88</u>
Avg	<u>.88</u> ✓	<u>.88</u> ✓	<u>.88</u> ✓
Dry Gas Meter:			
Final Vol	<u>151.520</u>	<u>156.993</u>	<u>162.392</u>
Initial Vol	<u>146.700</u>	<u>151.800</u>	<u>157.300</u>
Vol (V _d , ft ³)	<u>4.820</u> ✓	<u>5.193</u> ✓	<u>5.092</u> ✓
Dry Gas Meter			
Initial	<u>83</u>	<u>86</u>	<u>89</u>
Temp (°F):Inlet			
Mid	<u>86</u>	<u>89.5</u>	<u>93</u>
Final	<u>88</u> ✓	<u>91.5</u> ✓	<u>95</u> ✓
Avg (°F/°A)	<u>(85.67) 545.67</u>	<u>(89) 549</u>	<u>(92.3) 552.3</u>
Dry Gas Meter			
Initial	<u>83</u>	<u>86</u>	<u>89</u>
Temp (°F):Outlet			
Mid	<u>86</u>	<u>89.5</u>	<u>93</u>
Final	<u>88</u> ✓	<u>91.5</u> ✓	<u>95</u> ✓
Avg (°F/°A)	<u>(85.67) 545.67</u>	<u>(89) 549</u>	<u>(92.3) 552.3</u>
Avg Dry Gas	<u>5.163</u> ✓	<u>5.193</u> ✓	<u>5.163</u> ✓
Meter Temp (T _m -°F/°A)	<u>(85.67) 545.67</u>	<u>(89) 549</u>	<u>(92.3) 552.3</u>
Time (minutes)	<u>10:00</u>	<u>10:00</u>	<u>10:00</u>

$$Y = \frac{(V_w)(MCF)(BP)(T_m)}{(V_d)(BP + \frac{\Delta H}{13.6})(T_w)}$$

$$Y \text{ Factor } \% \text{ Difference} = \frac{\text{Act} - \text{Exp}}{\text{Exp}} \times 100$$

NOTE: MCF = Meter Correction (Y) Factor for Dry Gas Meter used as a Transfer Standard

Run 1

$$Y = \frac{(4.974)(.9903)(29.85)(545.47)}{(4.850)(29.85 + \frac{.88}{13.6})(537.67)} = \frac{80,307.516}{77,603.783} = 1.0349$$

$$\Delta\% = \frac{(1.0349 - 1.0136)}{1.0136} \times 100 = + 2.10 \%$$

Run 2

$$Y = \frac{(5.206)(.9903)(29.85)(549)}{(5.193)(29.85 + \frac{.88}{13.6})(536.67)} = \frac{84,571.470}{83,452.719} = 1.0133$$

$$\Delta\% = \frac{(1.0133 - 1.0136)}{1.0136} \times 100 = - 0.02 \%$$

Run 3

$$Y = \frac{(5.162)(.9903)(29.85)(552.33)}{(5.092)(29.85 + \frac{.88}{13.6})(536)} = \frac{84,381.673}{81,728.445} = 1.0325$$

$$\Delta\% = \frac{(1.0325 - 1.0136)}{1.0136} \times 100 = 1.86 \%$$

NOTE: The Y Factor % Difference must be < +5.0% to be acceptable

Determination of Interpolated Y Factor for Average Certification Test Series Delta H from Dry Gas Meter Calibration Data:

$\bar{Y} = 1.0136\%$

$\frac{.75}{(A)}$ inch H₂O Delta H = $\frac{1.011}{(C)}$ Calculated Calibration Y Factor (from Calibrations)

$\frac{1.000}{(B)}$ inch H₂O Delta H = $\frac{1.016}{(D)}$ Calculated Calibration Y Factor (from Calibrations)

$$\frac{1.00}{(B)} - \frac{.75}{(A)} = \frac{.25}{(A)} \times 100 = \frac{25}{(E)}$$

$$\frac{1.016}{(D)} - \frac{1.011}{(C)} = \frac{.005}{(C)} \div \frac{25}{(E)} = \frac{.0002}{(F)}$$

$$\frac{.8822}{\text{Avg Delta H}} - \frac{.75}{(A)} = \frac{.1322}{(A)} \times 100 = \frac{13.22}{(G)}$$

$$\left[\frac{.0002}{F} \times \frac{13.22}{G} \right] + \frac{1.011}{C} = \frac{1.0136}{\text{Interpolated Y Factor For Avg. Test Series Delta H}}$$

1,000 CFM @ -17.5" Hg Pave 1 min.

Volume Metering System Leak Check: _____ inch H₂O in one minute

REFERENCE METER CALIBRATION
ENGLISH REFERENCE METER UNITS

Filename: F:\DATAFILE\CALIBRAT\CAL_MENU_DSK\DGM_REF.
Revised: 06/08/95

DGM Serial # 300392
Date 4/1/96

Barometric Pressure 29.45
Meter Yw 1.00000
K (deg R/inches Hg) 17.64

Time (min)	Pressure (in. H2O)		Dry Gas Meter (DGM)		Temperature		Wet Test Meter (WTM)		DGM Coefficient Yds	Coefficient Variation Yds-(Avg.Yds)	Flow Rate (CFM)
	Initial	Final	Volume (cubic feet)	Volume (cubic feet)	Initial (deg.F)	Final (deg.F)	Volume (cubic feet)	Temp (deg.F)			
9.00	-6.40	26.28	11.33	37.60	70.0	71.0	10.938	67.0	0.988	0.000	1.198
8.50	-6.40	37.60	10.69	48.29	71.0	72.0	10.302	67.0	0.988	0.000	1.195
11.50	-6.40	48.29	14.43	62.72	72.0	73.0	13.891	67.0	0.989	0.000	1.191
Max Yds - Min Yds = 0.000614711 Must be no greater than 0.030											
Average Yds = 0.988195552 Must be between 0.95 to 1.05											
8.50	-4.10	62.72	8.32	71.03	73.0	74.0	8.044	67.0	0.989	0.000	0.933
6.00	-4.10	71.03	5.89	76.92	74.0	74.0	5.696	67.0	0.990	0.000	0.926
5.50	-4.10	76.92	5.36	82.28	74.0	75.0	5.184	68.0	0.989	0.000	0.927
Max Yds - Min Yds = 0.000811587 Must be no greater than 0.030											
Average Yds = 0.989551764 Must be between 0.95 to 1.05											
23.00	-3.00	82.28	18.41	100.69	74.0	76.0	17.834	68.0	0.989	-0.001	0.763
10.50	-3.00	100.69	8.41	109.10	76.0	77.0	8.141	68.0	0.991	0.001	0.763
20.50	-3.00	109.10	16.49	125.59	77.0	78.0	15.915	68.0	0.990	0.000	0.764
Max Yds - Min Yds = 0.002111523 Must be no greater than 0.030											
Average Yds = 0.990046834 Must be between 0.95 to 1.05											
9.00	-1.80	125.59	5.12	130.71	78.0	78.0	4.960	68.0	0.992	0.001	0.542
9.50	-1.80	130.71	5.39	136.10	78.0	79.0	5.225	69.0	0.991	0.000	0.540
10.00	-1.80	136.10	5.71	141.81	79.0	79.0	5.524	69.0	0.991	-0.001	0.542
Max Yds - Min Yds = 0.001237161 Must be no greater than 0.030											
Average Yds = 0.991169657 Must be between 0.95 to 1.05											
13.50	-1.20	141.81	5.60	147.41	79.0	80.0	5.433	69.0	0.992	0.000	0.395
14.50	-1.20	147.41	6.03	153.44	80.0	80.0	5.848	69.0	0.993	0.001	0.396
13.50	-1.20	153.44	5.62	159.06	80.0	80.0	5.445	69.0	0.992	-0.001	0.396
Max Yds - Min Yds = 0.001332081 Must be no greater than 0.030											
Average Yds = 0.992331519 Must be between 0.95 to 1.05											

Overall Average Yds = 0.990259065

I certify that the above Dry Gas Meter was calibrated in accordance with E.P.A. Method 5, paragraph 7.1, CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3785, certificate # F107, which is traceable to the National Bureau of Standards (N.I.S.T.).

Signature *[Handwritten Signature]* Date 4-1-96

VANEOMETER CALIBRATION

Myren Consulting uses a Dwyer Model #480 Vaneometer to measure test chamber air velocity. The manufacturer's specifications for accuracy are $\pm 5.0\%$ to 100 FPM and $\pm 10\%$ from 100 FPM to top of scale. Myren Consulting insures that the instrument is level and clean prior to taking each reading. According to EPA personnel (Westlin, RTP) no further calibration of the instrument is necessary.

DRAFT GAUGE CALIBRATION

Myren Consulting uses a Dwyer Model 115-AV 0 - 0.25" inclined water manometer (readability resolution $\pm 0.001"$ of water) to measure the static pressure in the stack. Once leveled and zeroed as per the manufacturer's written operating instructions, the Dwyer 0 - 0.25" manometer is a primary standard and needs no additional calibration.

The manometer is leveled and zeroed at the start of each test run, checked as necessary during the run to verify that the settings have not changed and again at the end of each test run. The results of each check are recorded on Woodstove Data Sheet #16 in each individual test run.

BAROMETER CALIBRATION

Myren Consulting uses a Weems and Plath aneroid barometer to measure barometric pressure (BP) in the Woodinville, WA lab. The barometer is calibrated daily by obtaining the barometric pressure (station pressure) from the National Weather Service (NWS) adjusting that pressure for altitude and then calibrating the lab barometer as necessary to that pressure.

MOISTURE METER CALIBRATION

The Delmhorst Model RC-1E, SN 1509 Moisture Meter is calibrated each time the meter is turned on using the two (2) calibration settings (Zero and Span). The potentiometers for each calibration point (X = Zero, Y = Span) are adjusted until the meter is correctly calibrated. Then the operation of the meter is checked in the normal operating range used during testing (11 - 25%) with a Delmhorst Model MCS-1 Moisture Content Standard at 12.5% and 22%.

Myren Consulting has a second moisture meter - Delmhorst Model RDX-1 SN 1359 - to use as a backup and as means of checking the readings on the Model RC-1E.

The readings obtained from the moisture meter are corrected as per the manufacturer's written instructions. See the following page for the correction table used to correct the readings.

10.0 - 10.6
 10.5 - 11.2
 11.0 - 11.7
 11.5 - 12.3
 12.0 - 12.8
 12.5 - 13.3
 13.0 - 13.9
 13.5 - 14.4
 14.0 - 14.9
 14.5 - 15.4
 15.0 - 15.9
 15.5 - 16.5
 16.0 - 17.0
 16.5 - 17.5
 17.0 - 18.1
 17.5 - 18.6

24.0 - 26.0
 24.5 - 26.6
 25.0 - 27.2

26-ED ELECTRODE

OPERATING INSTRUCTIONS

The 26-E and 18-E Electrodes, fitted with insulated pins and used with any Delmhorst Moisture Detectors for Wood, are available in detecting moisture gradient in lumber or in testing dry stock that is wet on the surface.

These Electrodes, as long as they have good insulation on their shanks, measure moisture content at the tip of the pins only, that is in a layer about 3/16" thick.

Shell and core, moisture content is easily measured by driving the pins to the proper depths.

When using the Electrode, place the pins on the wood so that the current will flow parallel to the grain and drive the pins into the wood by means of the sliding hammer. Note the pins' penetration, and read the meter.

The Moisture Meter is calibrated for use with a 4-pin Electrode. When using a 2-pin Electrode, a small correction should be applied, as noted below, where line "A" shows meter readings, and line "B" the correct readings for the 2-pin Electrode.

A= 7	8	10	12	14	16	18	20	22
B= 7.3	8.4	10.6	12.8	14.9	17.0	19.2	21.4	23.7

When the insulation on the contact pins wears off, the above correction should be disregarded, and the electrode should not be used on lumber which may have a wet surface. Always use the L-319 insulating washer especially if surface moisture on the wood is expected. If washers are not available, do not allow the retainers to touch the surface of the wood.



LEGAL ↑
 RANGE

18.0 - 19.2
 18.5 - 19.8
 19.0 - 20.3
 19.5 - 20.9
 20.0 - 21.4
 20.5 - 22.0
 21.0 - 22.6
 21.5 - 23.1
 22.0 - 23.7
 22.5 - 24.3
 ↓ 23.0 - 24.9
 23.5 - 25.4

Calibration DATA
 for
 Taylor Sling Psychrometer

<u>Reference</u>	<u>WB</u>	<u>DB</u>
Fisher	Taylor	Taylor
ASTM-59F	1330NA	1330NA
A04544	WB	DB
0-180°F	20-120°F	20-120°F
in 1° graduations	1°F	1°F
70°F	70°F	69.5°F
67°F	66	66
56°F	55.5	55.5
33.5°F	33	33
105°F	104	103

DATE: 4/17/96

Technician: A.J. Myra

Pre kuma

InterMountain Ambient

P.O. Box 5108 □ Missoula, MT 59806 □ (406) 543-6174

QA WS 1/85

CO₂ ANALYZER MULTIPOINT CALIBRATION REPORT FORM

Site: Woodinville, WA Date: 8/27/96
 Analyzer: Make: MORIBA Model: PIR 2000 SN: 6070241
 Calibration by: A. TIMMYSON
 Cal Gas Flow: 1.5 SCFH Measured by: Rotameter: Mass Flowmeter:
 BP: 29.88" Hg Instrument ID: Weems
 Temp: 72 °F Instrument ID: Fluke
 Analyzer last calibrated: 7/15/96 By: A. TIMMYSON

Cylinders:

- # 4-36919 Concentration: 00.0 % CO₂ Cyl. Press.: 2025 psi.
 Certified by: Airgas Date: 4/24/96
- # W260657 Concentration: 10.1 % CO₂ Cyl. Press.: 975 psi.
 Certified by: BOC Gases Date: 1/18/95
- # W19567 Concentration: 17.0 % CO₂ Cyl. Press.: 1825 psi.
 Certified by: BOC Gases Date: 1/25/95
- # W392263 Concentration: 5.08 % CO₂ Cyl. Press.: 1830 psi.
 Certified by: BOC Gases Date: 1/25/95

Analyzer: Calibrated Range. 0-25.0 % Output: 0-1.0 v.
 Flow: 1.5 SCFH Measured by: Rotameter: Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% CO ₂	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadj.	Adj.
1	1	0	00.0	.000	-0.5	.004	00.0	.000	-	5.04	5.35
2	2	10.1	40.4	.404	41.0	.411	40.4	.404	-	3.37	2.88
3	3	17.0	68.0	.680	68.7	.686	-	-	+0.12	-	-
4	4	5.08	20.3	.203	20.7	.204	-	-	+0.56	-	-
5	1	00.0	00.0	.000	00.0	.000	-	-	0	-	-

Comments:

$0.500 = 12.4257$ Span Value = 25%
 $29.88 \text{ SpH} = 0.500\%$
 $.186 = 17.0206\% - 17.0 = .0206$ $.204 = 5.083 - 5.08 = .0283$

Linear Regression Results:

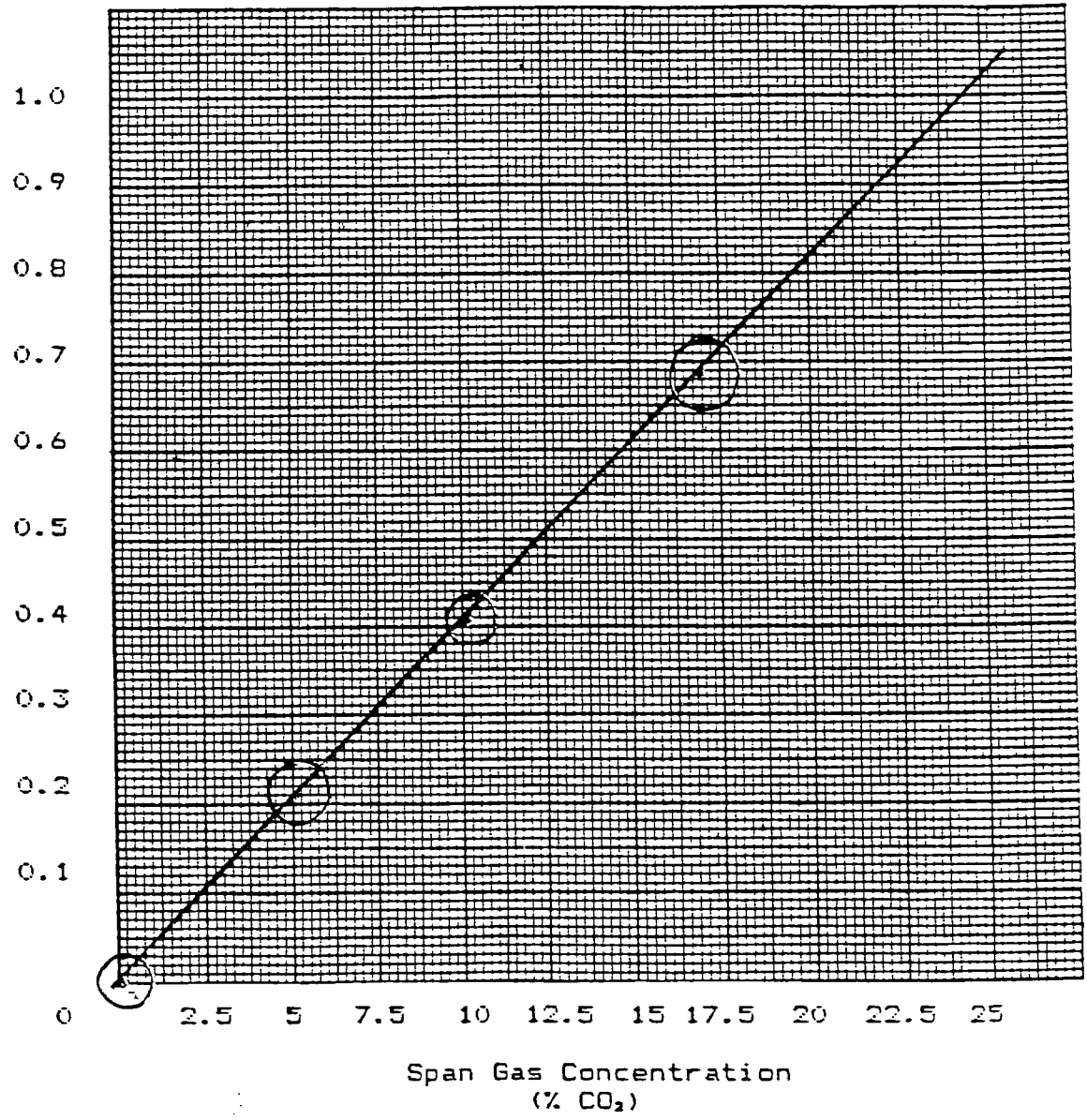
$Y = MX + B$

Slope (M) = $\frac{.040325}{}$

Y Intercept (B) = $\frac{-1.000916}{}$

Correlation Coefficient (r) = $\frac{0.999984}{}$

Analyzer
Output
(volts)



Comments

Pre kuma

InterMountain Ambient

P.O. Box 5106 □ Missoula, MT 59806 □ (406) 543-6174

QA WS 1/85

O₂ ANALYZER MULTIPOINT CALIBRATION REPORT FORM

Site: Woodinville, WA Date: 8/27/96

Analyzer: Make: Taylor Model: OA-137 SN: 137 / 4772

Calibration by: A. J. Meyer

Cal Gas Flow: 1500 cc/min Measured by: Rotameter: Mass Flowmeter:
BP: 29.88" Hg Instrument ID: Weems
Temp: 72°F Instrument ID: Floke

Analyzer last calibrated: 7/15/96 By: A. J. Meyer

Cylinders:

- # 4-36919 Concentration: 00.0 % O₂ Cyl. Press.: 2025 psi.
Certified by: Argas Date: 4/21/96
- # W260657 Concentration: 12.5 % O₂ Cyl. Press.: 975 psi.
Certified by: BOC Gases Date: 1/18/95
- # W19567 Concentration: 21.1 % O₂ Cyl. Press.: 1825 psi.
Certified by: BOC Gases Date: 1/25/95
- # W392263 Concentration: 6.25 % O₂ Cyl. Press.: 1830 psi.
Certified by: BOC Gases Date: 1/25/95

Analyzer: Calibrated Range: 0 - 25.0 % Output: 0 - 100 m.v.

Flow: 1500 cc/min Measured by: Rotameter: Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% O ₂	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadj.	Adj.
1	1	0	00.0	00.0	00.0	00.0	-	-		-	✓
2	2	12.5	12.5	50.0	51	50.7	12.5	50.0		-	✓
3	3	21.1	21.1	84.4	85.0	84.7	-	-		-	-
4	4	6.25	6.25	25.0	6.3	25.1	-	-		-	-
5	1	0	00.0	00.0	0.5	00.2	-	-		-	-

Comments: $50.0 \text{ m.v.} = 12.4674$ Span Value = 25.0%
 $2\% \text{ of Span Value} = 0.500\%$
 $84.7 = 21.116 - 21.1 = .01599 = 25.1 = 6.261 - 6.25 = 0.0113$

Linear Regression Results:

$Y = MX + B$

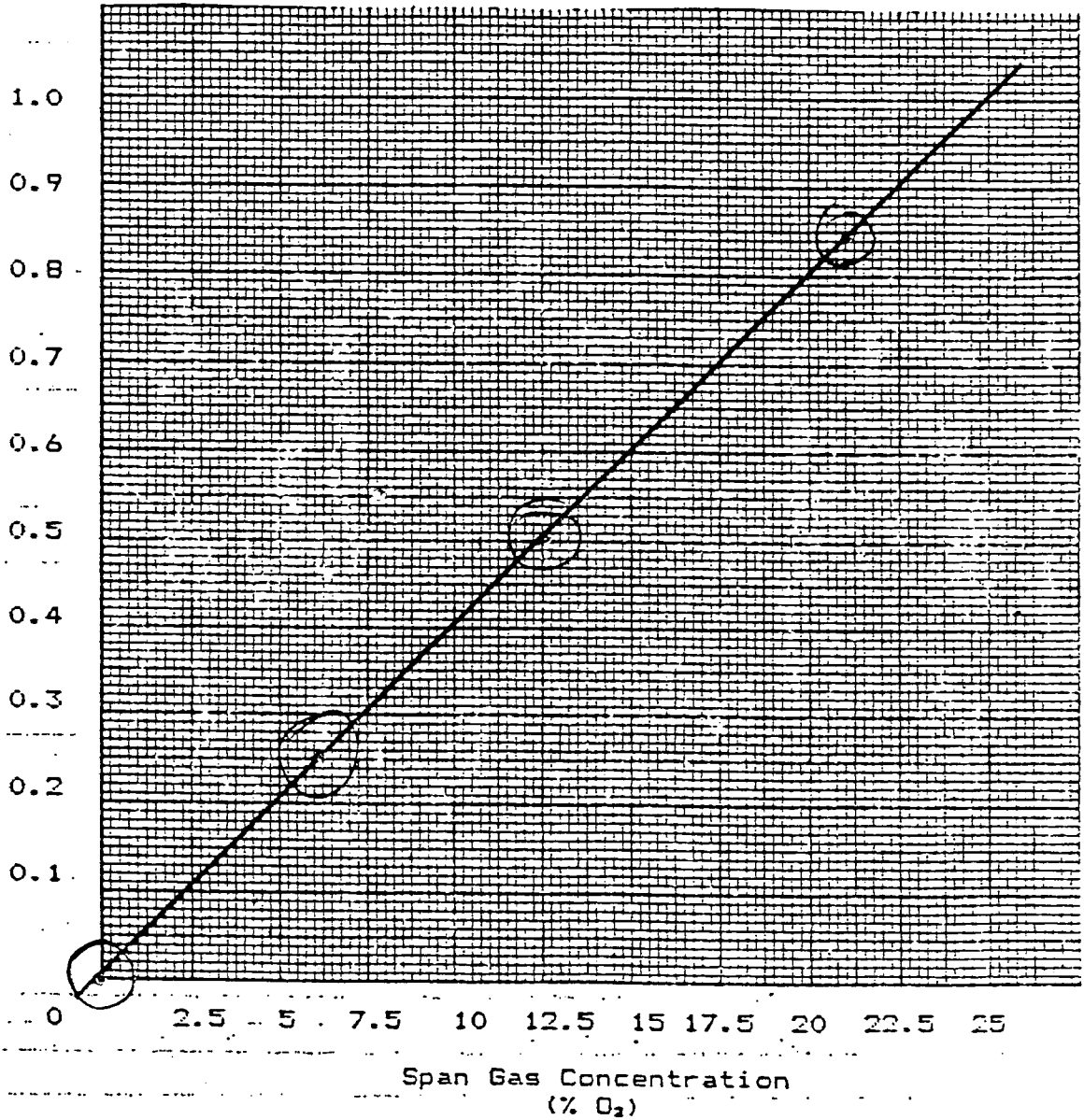
Slope (M) = 4.0121963

Y Intercept (B) = -0.02151

Correlation Coefficient (r) = 0.9999997

Analyzer
Output
M(volts)

$\times 10^2$



Comments

Pre kumq

QA.WS 1/85

CO ANALYZER
MULTIPOINT CALIBRATION REPORT FORM

Site: Woodinville, WA Date: 8/27/96
 Analyzer: Make: Infra RED Model: 702 D SN: 113
 Calibration by: A. Timyann
 Cal Gas Flow: 1.5 SCFH Measured by: Rotameter: X Mass Flowmeter:
 BF: 29.58" Hg Instrument ID: Wepms
 Temp: 72°F Instrument ID: Floke
 Analyzer last calibrated: 7/15/96 By: A. Timyann

Cylinders:

1. # 4-36919 Concentration: 00.0 % CO Cyl. Press.: 2025 psi.
 Certified by: Aie gas Date: 4/24/96
2. # W260657 Concentration: 2.47 % CO Cyl. Press.: 975 psi.
 Certified by: BOC Gases Date: 1/18/95
3. # W19567 Concentration: 4.11 % CO Cyl. Press.: 1825 psi.
 Certified by: BOC Gases Date: 1/25/95
4. # W392263 Concentration: 1.19 % CO Cyl. Press.: 1830 psi.
 Certified by: BOC Gases Date: 1/25/95

Analyzer: Calibrated Range: 0 - 5.0 % Output: 0 - 100 mV.
 Flow: 1.5 SCFH Measured by: Rotameter: X Mass Flowmeter:

Calibration Results

Point #	Cyl. #	% CO	Expected		Actual		Adj.		% Dif.	Potentiometer	
			Meter	DVM	Meter	DVM	Meter	DVM		Unadi.	Adj.
1	1	00.0	0.00	00.0	0.00	00.3	-	-	-	-	-
2	2	2.47	2.47	49.4	2.47	48.4	2.47	49.0	-	-	✓
3	3	4.11	4.11	80.2	4.31	85.8	-	-	1.08	-	-
4	4	1.19	1.19	23.8	1.28	25.3	-	-	3.44	-	-
5	1	0	0.00	00.0	0.00	00.3	-	-	-0.12	-	-

Comments: 50 > 2.42 45 287

EPA Spans Value: 5.0%
2% of " " = 0.100%

$4.1545 - 4.11 = .0445$, $1.0309 - 1.19 = .0409\%$

Linear Regression Results:

$Y = MX + B$

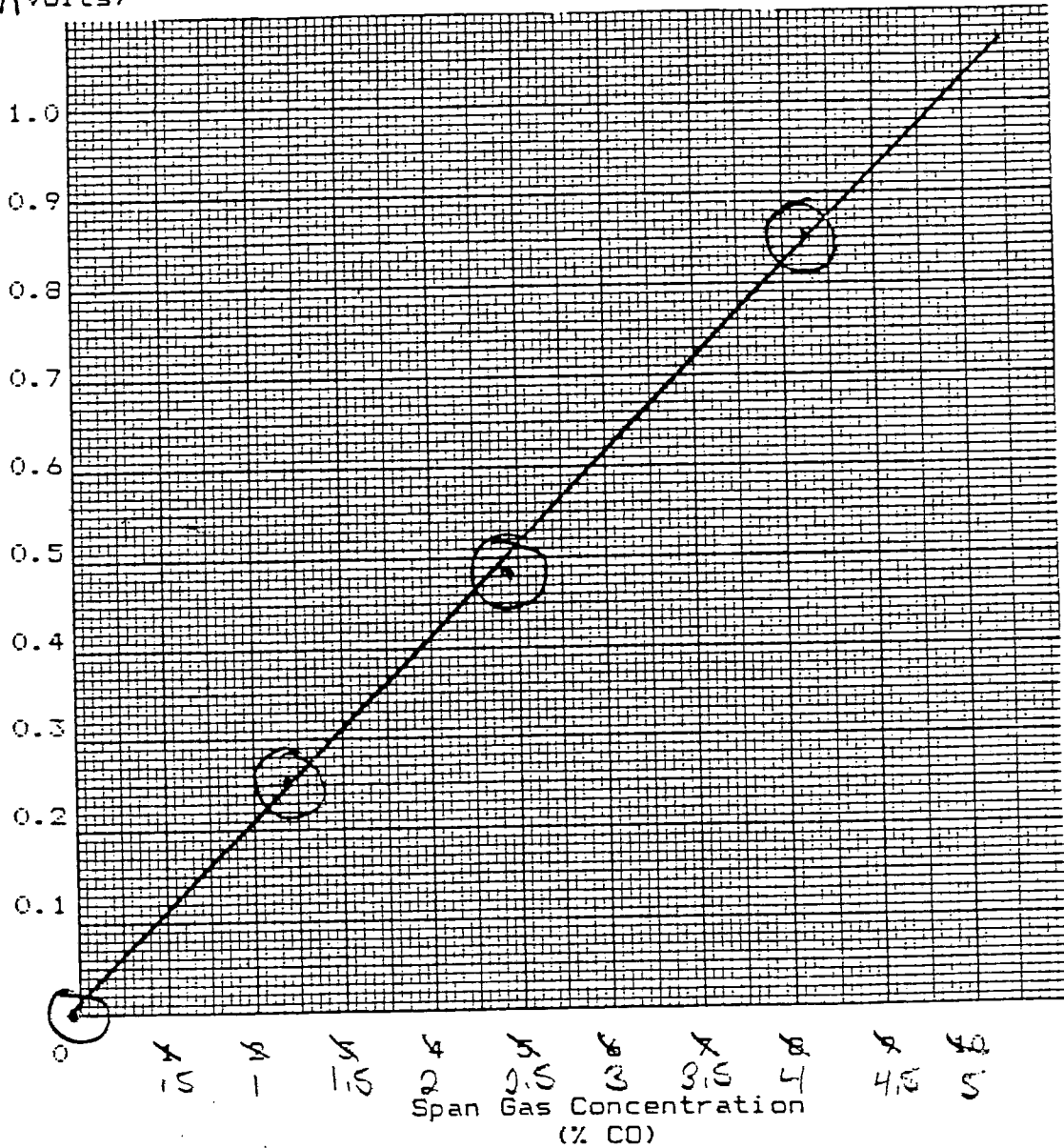
Slope (M) = $\frac{20.69379}{}$

Y Intercept (B) = $\frac{-1.7268}{}$

Correlation Coefficient (r) = 0.99933

Analyzer
Output
M(volts)

$\times 10^3$

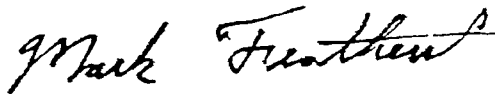


Comments

MALLINCKRODT**CERTIFICATE OF ANALYSIS**A Division of Mallinckrodt Baker, Inc.
222 Red School Lane • Phillipsburg, NJ 08865
Telephone: (908) 859-2151 • Fax: (908) 859-9318ITEM: ACETONE AR (ACS)
CODE: 2440
LOT : KTDC

TESTS	LIMITS	RESULTS
TITRATABLE ACID	0.0003 meq/g Max.	0.0002 meq/g
ALDEHYDE	0.002% Max.	0.002%
TITRATABLE BASE	0.0006 meq/g Max.	0.0004 meq/g
ISOPROPYL ALCOHOL	0.05% Max.	0.005%
METHANOL	0.05% Max.	0.005%
RESIDUE AFTER EVAPORATION	0.001% Max.	0.0002%
SOLUBILITY IN WATER	To Pass Test	Passes Test
SUBSTANCES REDUCING PERMANGANATE	To Pass Test	Passes Test
WATER	0.5% Max.	0.3%
COLOR	APHA 10 Max.	APHA 5
ASSAY	99.5% Min.	99.9%

It is hereby certified that the above is a true copy of the actual analysis of the lot indicated.

Mark Featherston
Manager, QA/QC
Mallinckrodt Baker, Inc
03/07/96 wwrAcetone Purchased 7/10/96
1st blank done 8/8/96

Stove QC

The Kuma Scott H-1 Noncatalytic Woodstove is a small to medium sized rectangularly shaped stove designed to be loaded either north-south or east-west with 16" wood. The firebox depth on the test unit was slightly longer (1/16") so the fuel load was placed in the unit in a North-South fashion.

The unit has a cast door, a fire brick baffle covered with a 1/2" ceramic blanket and 3 secondary air tubes.

The unit has several distinguishing features.

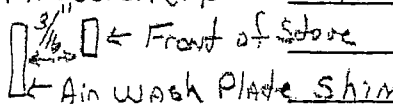
1. It is a step top stove.
2. It is a true outside air stove in that all of the air entering the unit has to go through the pedestal.
3. The unit is a very good consistent performer. Test starts were not a problem. The unit often did not lose gas balance after the primary air control was adjusted to the run setting at 5:00 into the test, which is unusual.

QUALITY CONTROL INSPECTION

MODEL KUMA Scott HT-1

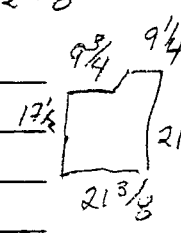
DATE 9/12/96 ATM

VERIFY MEASUREMENTS

HEIGHT [OVERALL] 32 1/2"
 WIDTH [OVERALL] 24"
 DEPTH [OVERALL] 25 1/4"
 HEIGHT FIREBOX See
 WIDTH FIREBOX drawings
 DEPTH FIREBOX _____
 FLUE COLLAR 6" x 2"
 ASH FENDER 19 3/4 x 3 3/4"
 GLASS _____
 Air Wash Gap 3/16"


VERIFY MEASUREMENTS

DOOR OPENING 14 1/4 x 9 1/2
 DRAFT-OPENING See drawings
 DRAFT-SECONDARY "
 DRAFT-3rd STAGE N/A
 BAFFLE PLATE N/A brick
 BASE (Pedestal) 22 1/4 x 22 1/4
 HEAT SHIELDS Pedestal Riser 8 7/8 x 12 1/8
 BACK _____
 SIDES _____
 BOTTOM N/A



MATERIAL

TOP 1/4"
 BACK 3/16"
 SIDES 3/16"
 BOTTOM 3/16"
 DOOR CAST
 BAFFLE Brick w/wood (Clay)
 HANDLE(S) door 1/2"
 BASE _____
 SHIELDS _____

BLOWER

TYPE & MODEL FASCO - No Visible ID
 CORD _____
 STRAIN RELIEF YES
 WIRING 3 wire 16 ga (?) grounded
 V.S.C. Yes
 FUSES N/A

DRAFT CONTROL Paddle Type See drawings

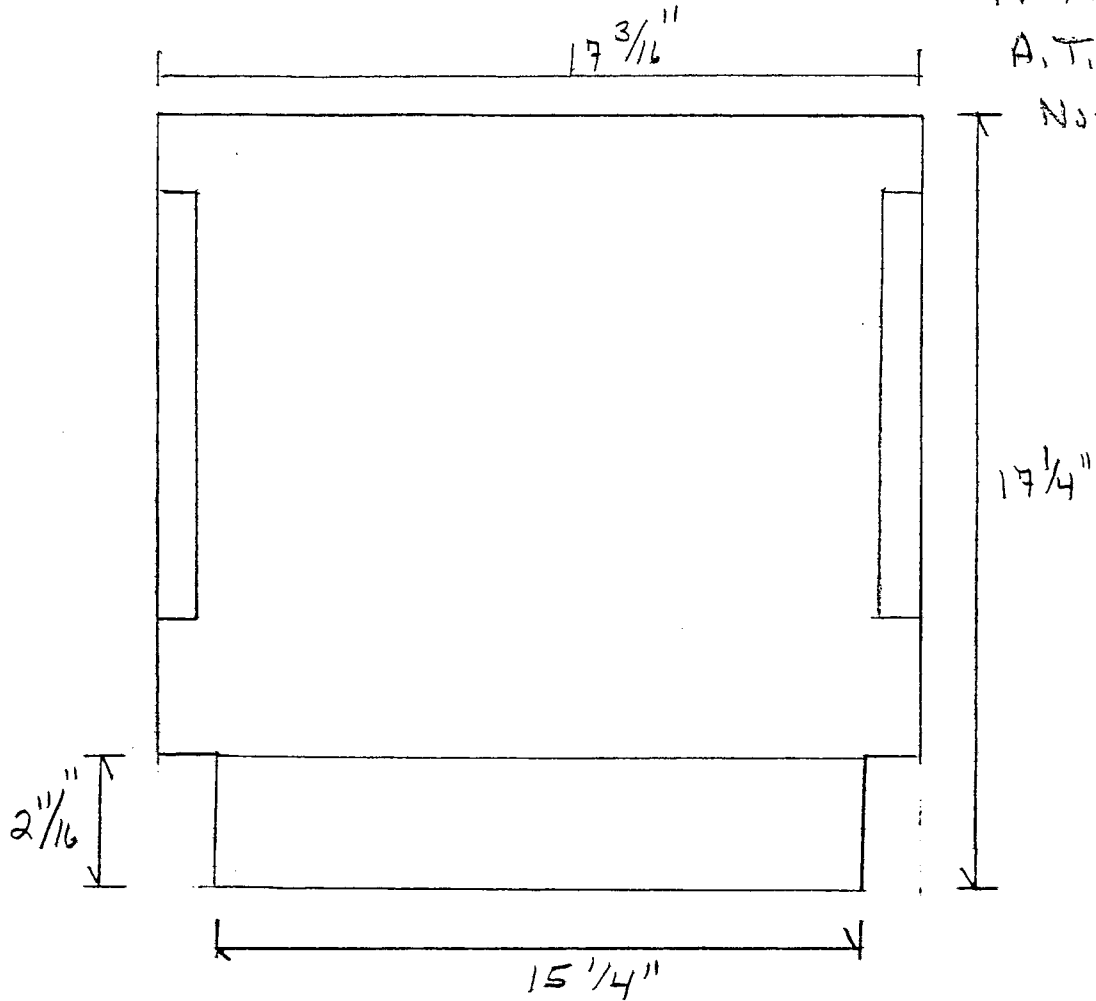
LABELING: CHECK OF RECORDS _____
 ANY IMPROPER USAGE FOUND _____
 SERIAL NO'S ON HAND _____

ADDITIONAL OBSERVATIONS: Step Top S-love, 3 1/8" Flue Collar
Hole in top below Flue Collar = 5 1/2"

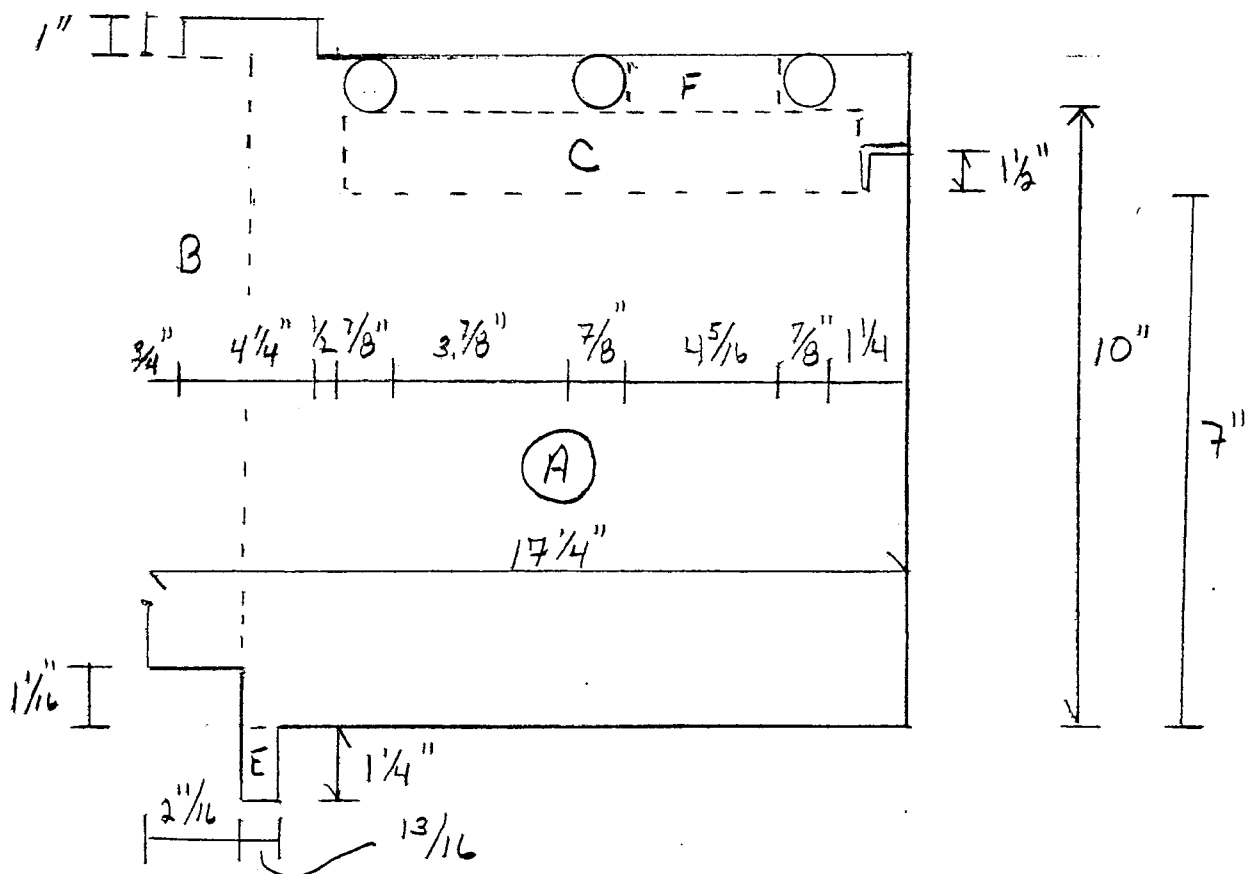
Kuma Scott HIT-1 USEABLE FIREBOX DIMENSIONS

P. 1 of 3

A. T. MYRUM
Not to Scale



USEABLE
DOOR
OPENING
HT.
 $9 \frac{1}{2}$ "



A.T. Myrow

USEABLE FIREBOX Volume Calculations:

$$A: 17.1875 \times (17.25 - 2\frac{1}{16}) \times 7 = 1752.051 \checkmark$$

$$B: 15.25 \times 2\frac{1}{16} \times 10 = 409.844 \checkmark$$

$$C: 16 \times (17.25 - 2\frac{1}{16}) \times 3 = 699.000 \checkmark$$

$$D: 15.25 \times 4.25 \times 1 = 64.813 \checkmark$$

$$E: 17.1875 \times 1.25 \times 13\frac{1}{16} = 17.456 \checkmark$$

$$F: 1 \times 4.3125 \times 16 = 69.000 \checkmark$$

$$\underline{3012.164 \text{ in}^3}$$

Less

$$G: 15.25 \times 1.0625 \times 2\frac{1}{16} = 43.5459$$

$$3012.164 \text{ in}^3 - 43.5459 \text{ in}^3 = 2968.618$$

$$2968.618 \text{ in}^3 \div 1728 \text{ in}^3/\text{ft}^3 = 1.7180 \text{ ft}^3$$

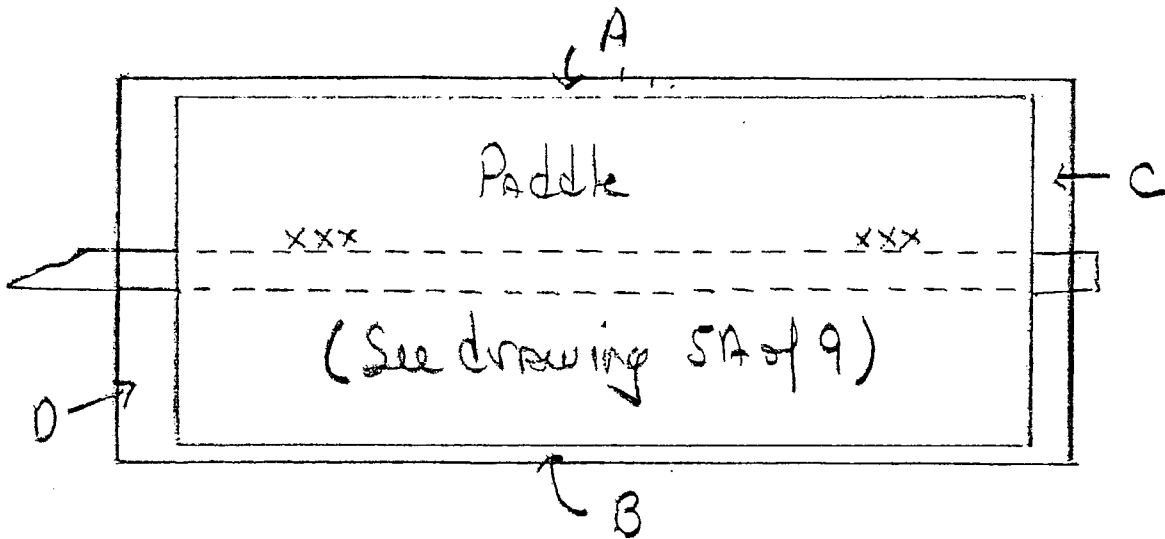
$$1.7180 \text{ ft}^3 \times 7 \text{ lbs}/\text{ft}^3 = 12.026 \text{ lbs. Ideal Fuel Load Wt.}$$

$$12.026 \text{ lbs} \pm 10\% = 13.229 - 10.823 \text{ lbs}$$

$$= 13.2 - 10.9 \text{ lbs, Fuel Load Wt. Range,}$$

Kumar Scott HT-1
 P. 3 of 3
 A. Timmy
 Not to Scale.

Primary air Control Gap
 Dimensions

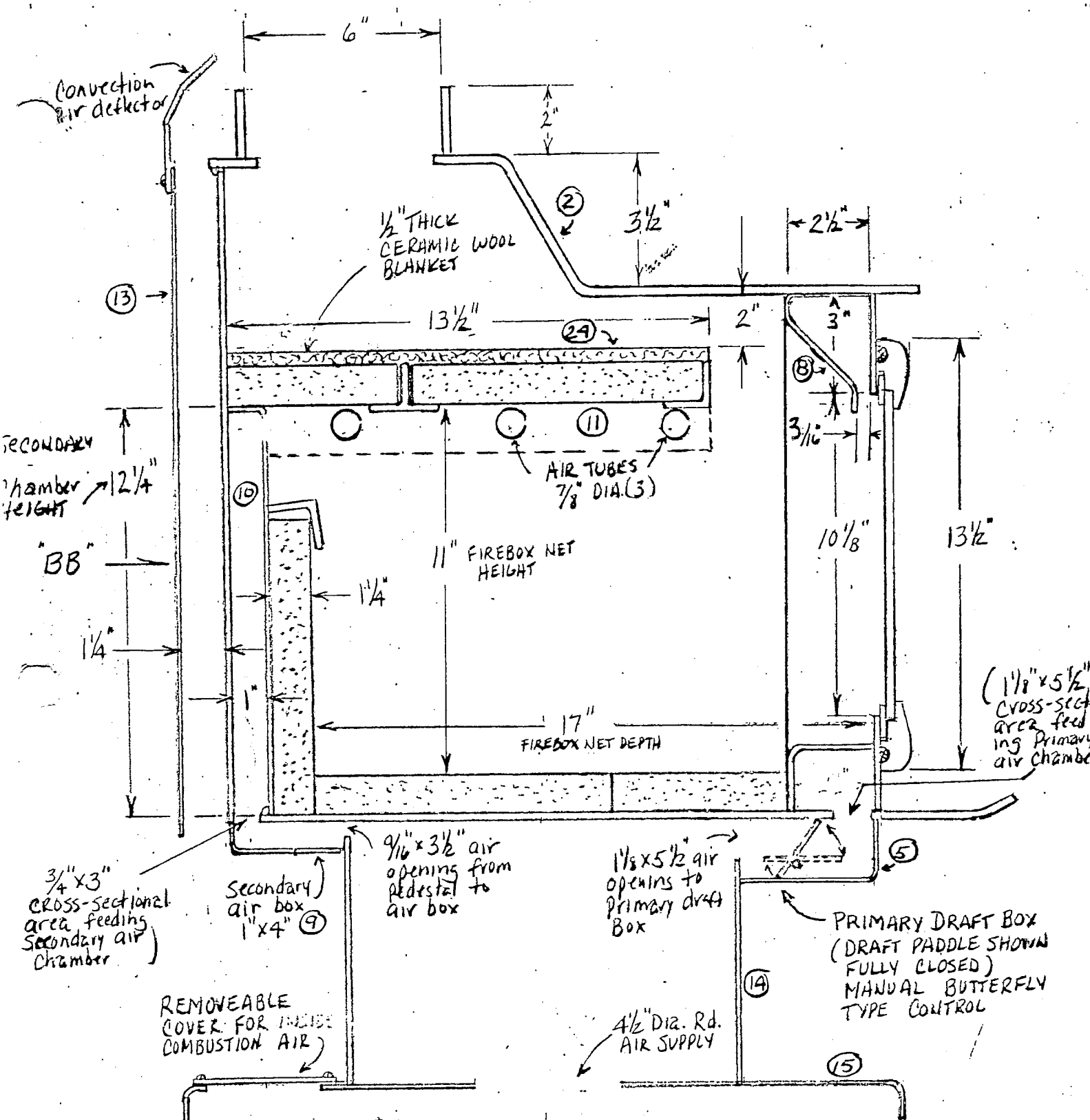


The gaps for the primary air control at the "stop" position ($3/8$ " on the arc from totally closed) are as follows:

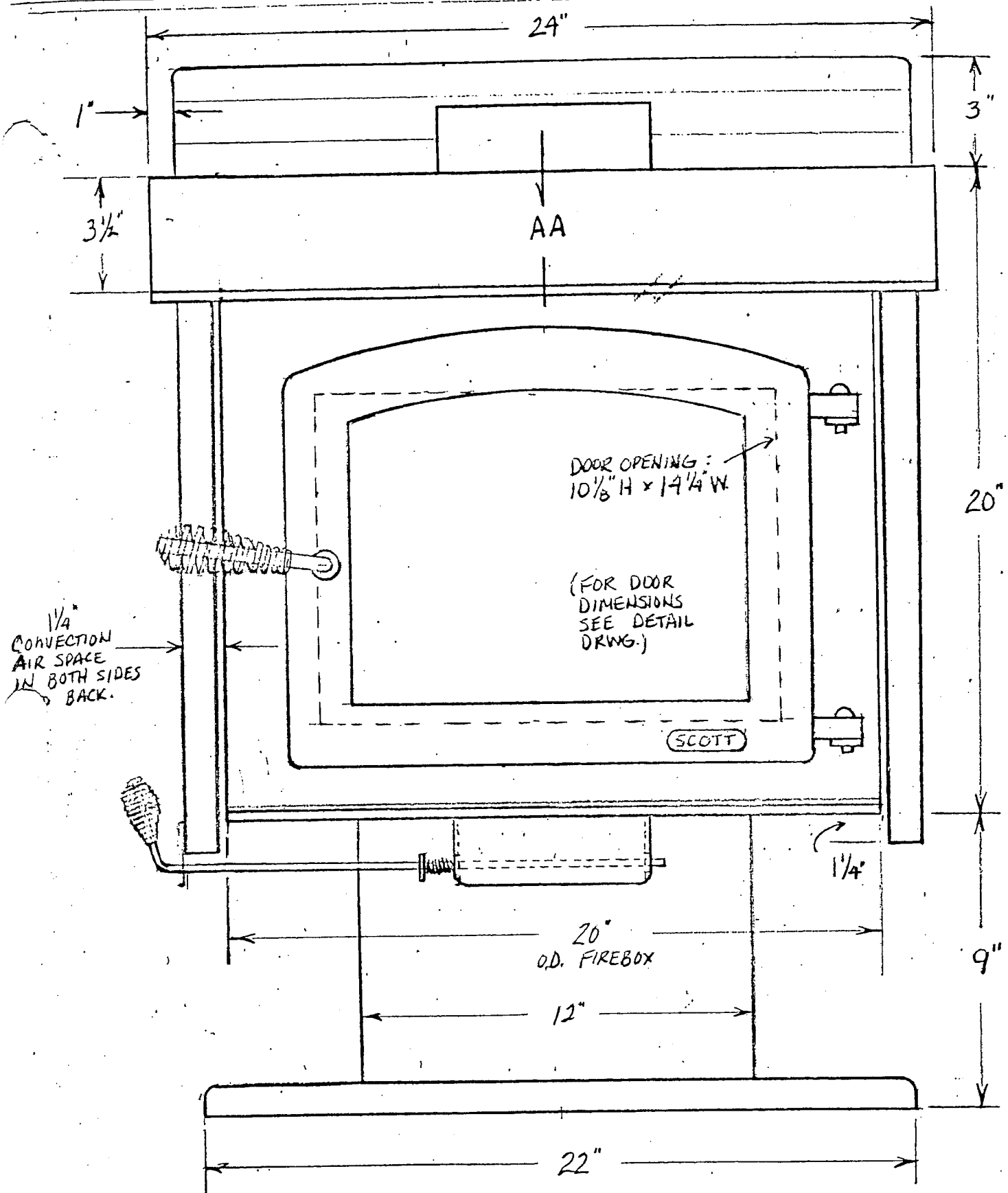
A	.0411	59	
B	.055	55	
C	.0785	47	
D	.1222	30 32	

\bar{X} of .1285 @ top and .1160 @ bottom

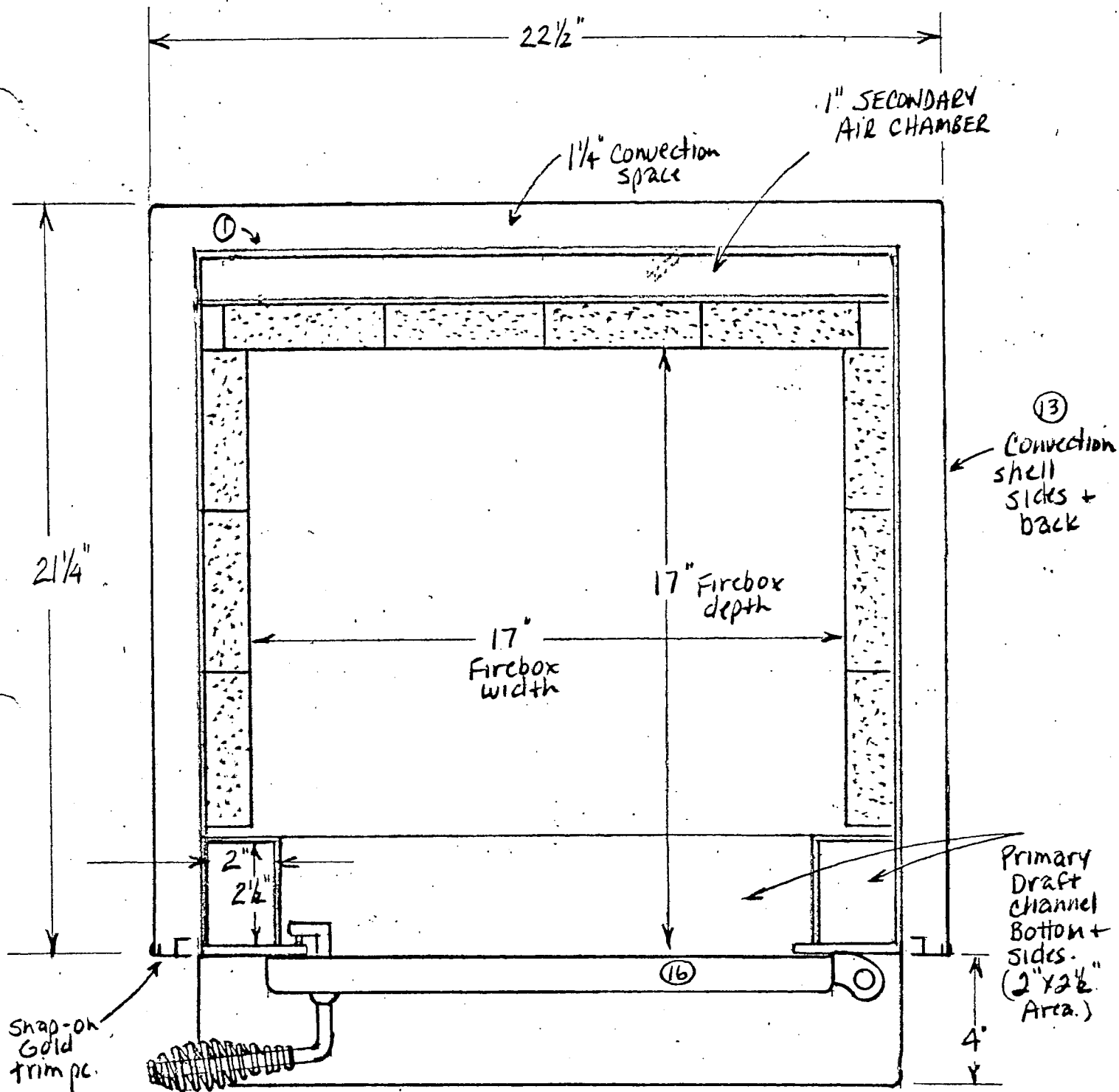
The manufacture intends to install a small shim inside the primary air control box to produce the desired gaps and thereby eliminate the stop on the heat shield that was used on the prototype.



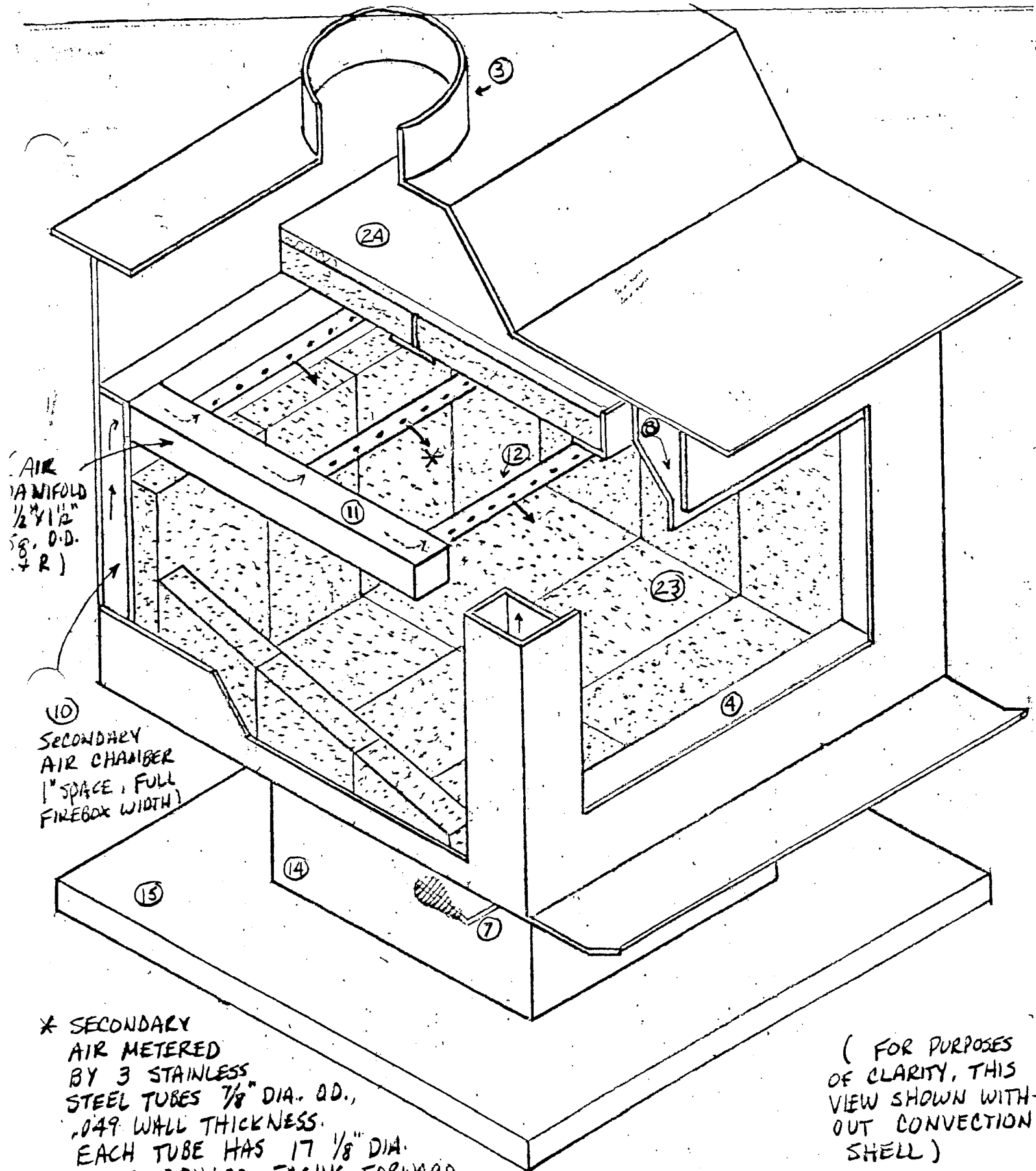
TITLE: KUMA SCOTT HT	DRAW. NO. 1 OF 9	DR. BY M.F.
VIEW: SIDE CROSS-SECTION A-A	DATE: 6-20-96	SCALE: 1/4" = 1"



TITLE: KUMA SCOTT HT	DRAW. NO. 2 OF 9	DR. BY M.F.
VIEW: FRONT	DATE: 6-20-96	



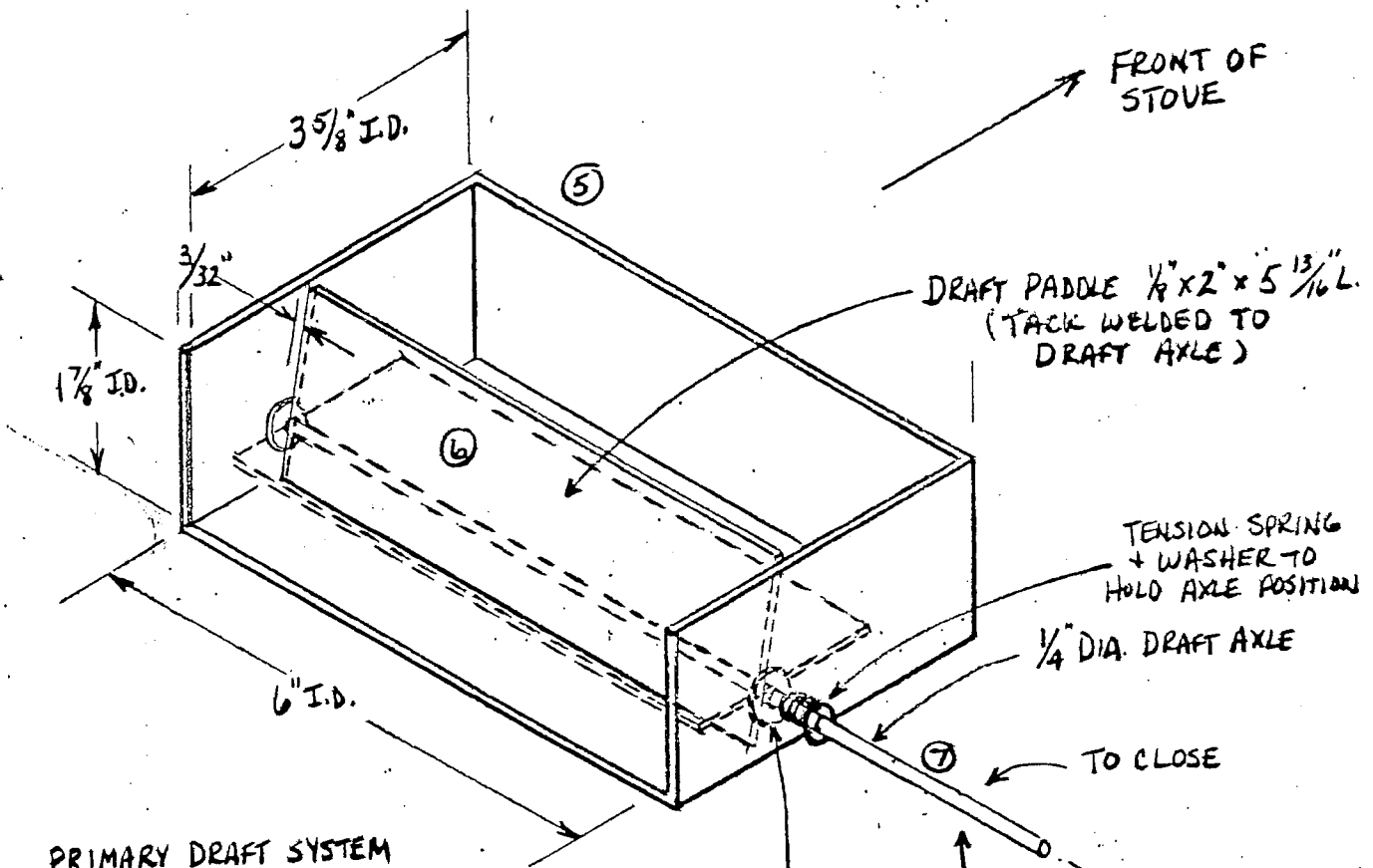
TITLE: KUMA SCOTT HT	DRAW. NO. 3 OF 9	DR. BY MF.
VIEW: TOP CROSS-SECTION B-B	DATE: 6-24-96	SCALE 1/4" = 1"



* SECONDARY
 AIR METERED
 BY 3 STAINLESS
 STEEL TUBES $\frac{7}{8}$ " DIA. O.D.,
 .049 WALL THICKNESS.
 EACH TUBE HAS 17 $\frac{1}{8}$ " DIA.
 HOLES DRILLED, FACING FORWARD.
 TOTAL SECONDARY AIR TO FIREBOX:
 (51, $\frac{1}{8}$ " HOLES
 .636 SQ IN
 TOTAL AREA.)

(FOR PURPOSES
 OF CLARITY, THIS
 VIEW SHOWN WITH-
 OUT CONVECTION
 SHELL)

TITLE: KUMA SCOTT HT	DRAW. NO. 4 OF 9	DR. BY MF.
VIEW: FIREBOX CUTAWAY PRIMARY/SECONDARY AIR	DATE: 6-26-96	SCALE 1 CM = 1"



PRIMARY DRAFT SYSTEM OPENINGS (AREA)

1. FROM PEDESTAL TO DRAFT BOX
($1\frac{1}{8} \times 5\frac{1}{2}$) = 6.188 sq. in.
2. DRAFT BOX AREA - (CLOSED POSITION)
($\frac{3}{16} \times 2$) = .374 sq. in.
3. DRAFT BOX AREA - (OPEN POSITION)
($1\frac{1}{2} \times 6$) = 9 sq. in.
4. FROM DRAFT BOX TO AIR CHANNEL: ($1\frac{1}{2} \times 5\frac{1}{2}$)
6.188 sq. in.
5. DRAFT CHANNEL AREA ($2 \times 2\frac{1}{2}$) = 5 sq. in.
6. TOP AIRWASH AREA: ($7\frac{1}{16} \times 15$)
= 6.56 sq. in.

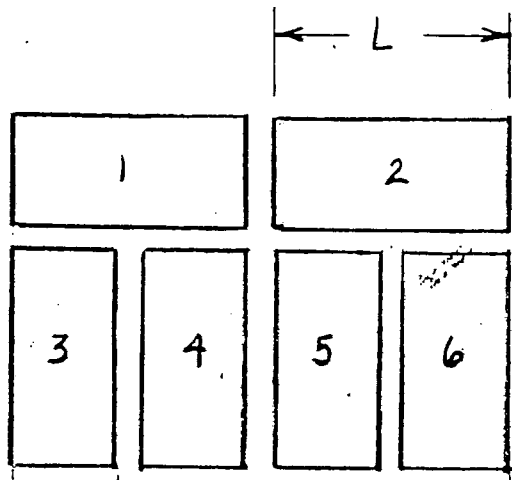
($\frac{1}{4}$ " DIA. \times $\frac{3}{32}$ " WASHER ON EACH END TO SPACE DRAFT PADDLE AWAY FROM BOX WALLS TO ALLOW SMALL AIR SUPPLY WHEN SHUT CLOSED.)

TO OPEN

TO CLOSE

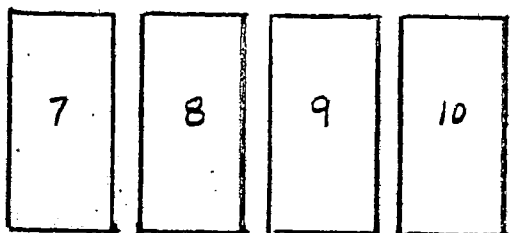
TO MANUALLY CONTROLLED SPRING HANDLE

TITLE: KUMA SCOTT HT	DRAW. NO. 5A OF 9	DR. BY M.F.
VIEW: PRIMARY DRAFT BOX DET.	DATE: 6/28/96	SCALE: $\frac{1}{2} = 1$ "



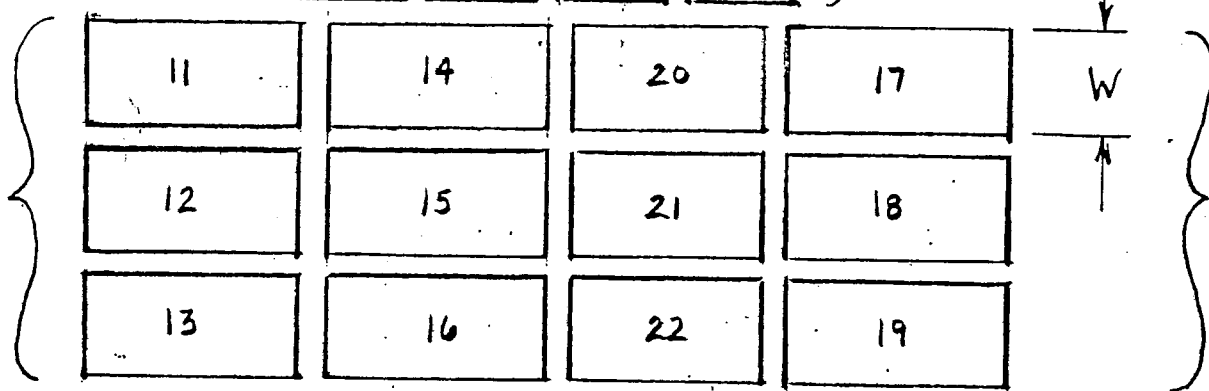
TOP VIEW OF
BAFFLE FIRE
BRICK LAYOUT
(6 pcs.)

(23)



FIREBOX BACK
(4 pcs.)

FIREBOX
LEFT
SIDE
(3 pcs)



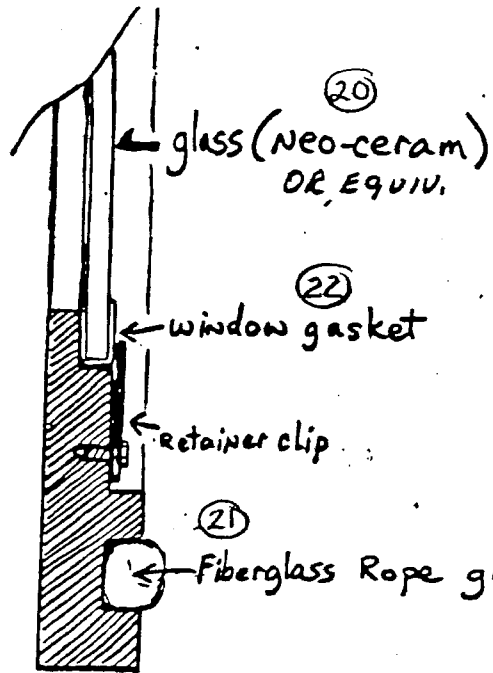
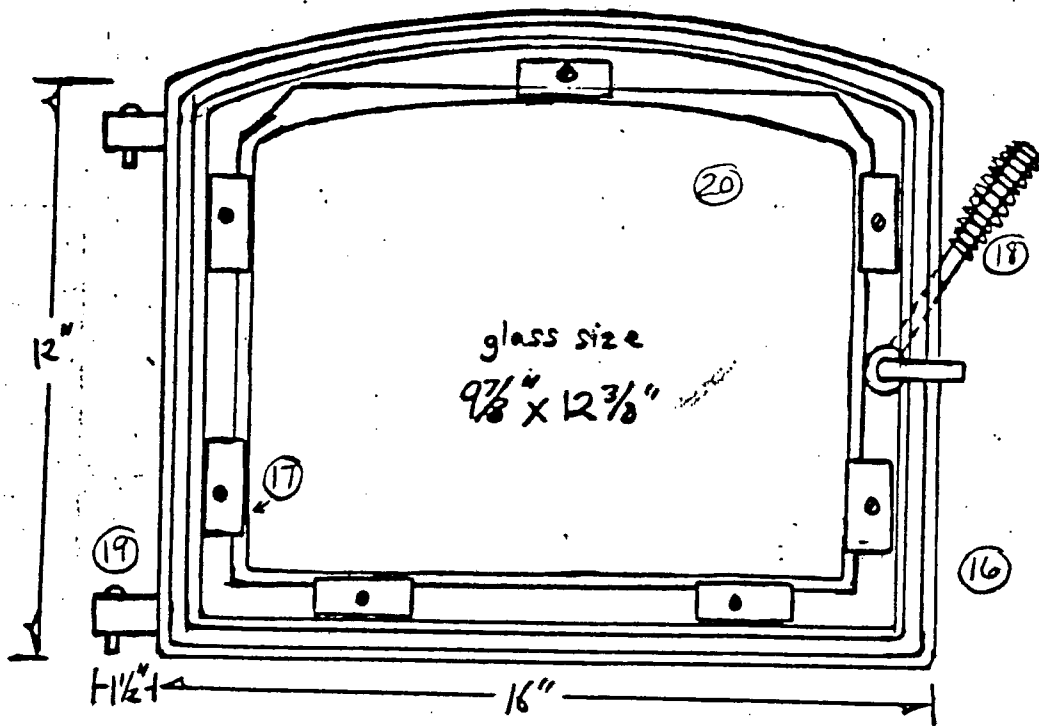
FIREBOX
RIGHT
SIDE
(3 pcs)

FIREBOX BOTTOM (6 pcs)

BRICK / LOCATION	L	W	THICKNESS
No. 1-19	9"	4½"	1¼"
No. 20-22	8"	4½"	1¼"

ALL REFRACTORY IS
LOW-DUTY FIREBRICK
MFG. BY MUTUAL
MATERIALS. CO. INC.,
81% FIRECLAY
19% SILICATED ALUMINA

TITLE: KUMA SCOTT HT	DRAW. NO. 6 OF 9	DR. BY MF
VIEW: REFRACTORY DETAIL	DATE: 7-5-96	

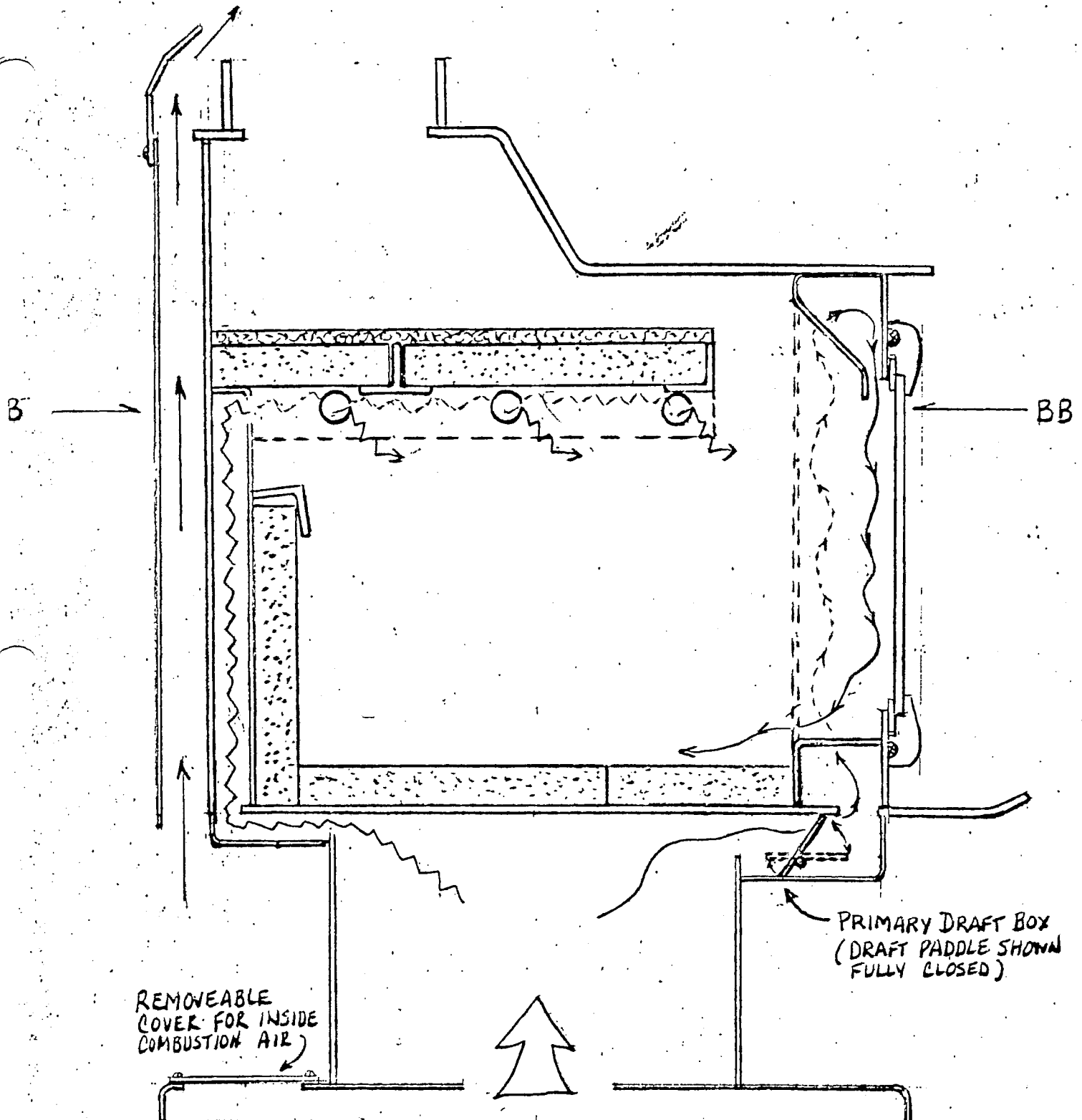





cutaway side view
(not to scale).

Note: The stove used for certification testing had a one piece glass retainer that went all the way around the glass except at the door handle.

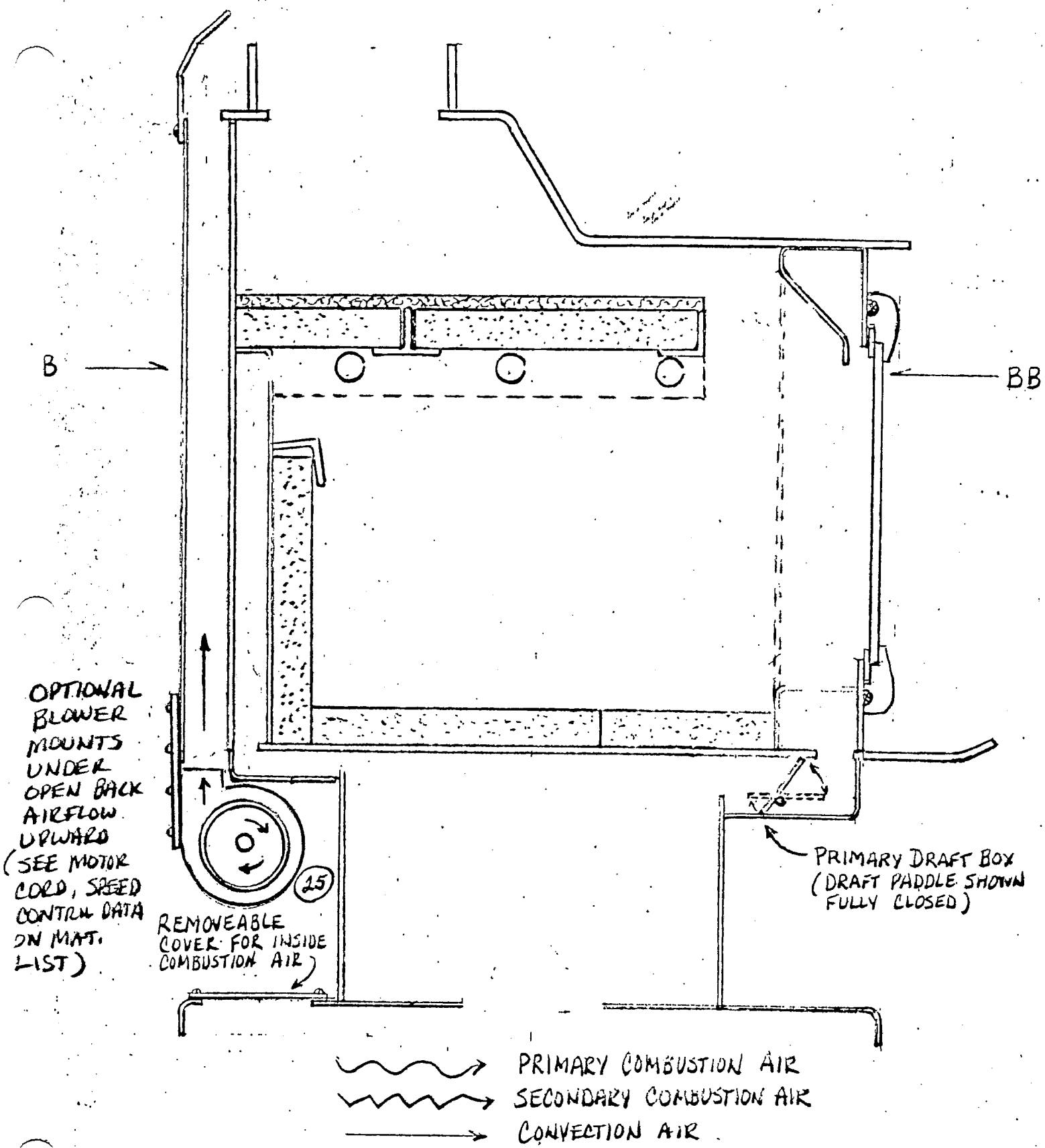
ATMyra
The screw locations were the same.

TITLE: KUMA SCOTT HT	DRAW. NO. 7 of 9	DR BY. S.C.
VIEW: DOOR BACK / CUTAWAY	DATE: 7-5-96	SCALE 1/4" = 1"



 PRIMARY COMBUSTION AIR
 SECONDARY COMBUSTION AIR
 CONVECTION AIR




TITLE: KUMA SCOTT HT	DRAW. NO. 8 OF 9	DR. BY M.F.
VIEW: SIDE CROSS-SECTION A-A COMBUSTION AIR PATTERNS	DATE: 6-20-96	SCALE: 1/4" = 1"



OPTIONAL
BLOWER
MOUNTS
UNDER
OPEN BACK
AIRFLOW
UPWARD
(SEE MOTOR
CORD, SPEED
CONTR. DATA
ON MAT.
LIST)

REMOVEABLE
COVER FOR INSIDE
COMBUSTION AIR

PRIMARY DRAFT BOX
(DRAFT PADDLE SHOWN
FULLY CLOSED)

 PRIMARY COMBUSTION AIR
 SECONDARY COMBUSTION AIR
 CONVECTION AIR

TITLE: KUMA SCOTT HT. BLOWER LOCATION	DRAW. NO. 9 OF 9	DR. BY M.F.
VIEW: SIDE CROSS-SECTION A-A	DATE: 6-20-96	SCALE: 1/4" = 1"

PART #	DESCRIPTION	DIMENSION	# OF PARTS	MATERIALS OF CONSTRUCTION MFG., MODEL ETC.
1	FIREBOX ASSLY	19 ⁵ / ₈ x 19 ⁵ / ₈ x 19 ⁵ / ₈	1	A-36 PLATE STEEL 3/16"
2	FIREBOX TOP	24" x 21 ³ / ₈	1	A-36 PLATE STEEL 1/4"
3	FLUE COLLAR	2" x 6" I.D.	1	MILD STEEL 3/16"
4	PRIMARY DRAFT CHANNEL	2" x 2 ¹ / ₂ "	3	MILD STEEL 10 ga.
5	" " BOX	2" x 6" x 3 ⁵ / ₈ "	1	" " 12 ga.
6	" " PADDLE	2" x 5 ¹³ / ₁₆ "	1	" " 1/8"
7	" " CONTROL	1/4" x 19"	1	1/4" C.R. ROUND
8	" " AIRWASH	2 ¹ / ₂ " x 3 ⁵ / ₈ " x 19 ¹ / ₂ "	1	MILD STEEL 10 ga.
9	SECONDARY DRAFT BOX	3 ⁵ / ₈ " x 3 ⁵ / ₈ " x 1"	1	" " 12 ga.
10	" " CHANNEL	12 ¹ / ₄ " x 19 ¹ / ₂ " x 1"	1	" " 10 ga.
11	" " MANIFOLDS	1 ¹ / ₂ " x 1 ¹ / ₂ " x 13 ¹ / ₂ "	2	" " 1/8"
12	" " TUBES	7/8" x 16 ¹ / ₂ "	3	STAINLESS STEEL .049
13	CONVECTION SHROUD	21 ¹ / ₄ " x 22 ¹ / ₂ " x 21"	1	MILD STEEL 14 ga.
14	PEDESTAL	12" x 12" x 8"	1	" " 12 ga.
15	PEDESTAL BASE	22" x 22" x 1"	1	" " 10 ga.
16	DOOR	13" x 16" x 1 ¹ / ₄ "	1	CAST IRON 14 lbs.
17	DOOR CLIPS (GLASS)	1" x 3"	7	MILD STEEL 1/8"
18	" HANDLE	1/2" x 7"	1	1/2" H.R. ROUND
19	" PINS	3/8" x 1 ¹ / ₂ "	2	STEEL RD. HD. RIVET
20	GLASS	10" x 12 ³ / ₈ "	1	SMA NED-CERAM
21	DOOR GASKET	5/8" DIA. x 60"	1	WOVEN FIBERGLASS
22	GLASS GASKET	3/4" x 1/8" x 45"	1	WOVEN FIBERGLASS WINDOW CHAM.
23	FIREBRICK	4 ¹ / ₂ " x 9"	22	(SEE REFRACTORY DRAW. # 6
24	BAFFLE BLANKET	14 ¹ / ₂ " x 19 ⁵ / ₈ "	1	1/2" CERAMIC FIBER BLANKET
		MFG. - HE-TEMP		PRODUCTS 1400°-2300° CONT.
25	BLOWER MOTOR	14" x 4" x 4 ¹ / ₂ "	1	MFG. BY FASCO INDUSTRIES
		SHAPE-POLE, 1.10 A, 115V.,		3200 R.P.M., 125 CFM MOD. A-125
26	BLOWER POWER CORD	5/16" x 8'	1	DAYTON SJT TYPE 18/3 w/GRD.
27	IN-LINE SPEED CONTROL	2 ¹ / ₂ " x 3 ¹ / ₂ " x 1 ¹ / ₂ "	1	WELLS TECH. MODEL JLS-3-8T, 3A.

TITLE: KUMA SCOTT HT	DRAW. NO.	DR. BY MF.
VIEW: PARTS/MATERIAL LIST	DATE: 7-5-96	

7/3/96

**Kuma Scott HT
Operating Instructions**

1. Primary Air Control Settings

Category 2 (≤ 1.0 Kg/hr) Stop - $1/8$ "

Category 2 ($> 1.0 \leq 1.25$ Kg/hr) Stop - $3/8$ "

Category 3 ($> 1.25 \leq 1.9$ Kg/hr) $1/4 - 1$ "

Category 4 Maximum Wide Open

Note: Measurements are from the stop and the movement is an arc. Measure at the top of the pointer.

Option (This can also vary with each burn category):
Leave the primary air control wide open for the full five minutes. Adjust to the run setting early if the burn rate appears to be too fast.. Crack the door open to enhance or assist ignition if necessary.

2. Blower

Category 2 and 3 - turn blower on High at 30 minutes

Category 4 - turn blower on high at 5 minutes.

KUMA2.doc

7-3-96

**Statements of Affirmation
KUMA SCOTT HT**

In direct relation to this application for certification of the Kuma model Scott HT, Kuma Stove and Iron Works affirms that:

1. Kuma Stove and Iron Works will conduct a Quality Assurance program (QA) on this model line.
2. Kuma Stove and Iron Works will notify the lab (Myron Consulting) that this model line has been certified within 30 days.
3. Kuma Stove and Iron Works will manufacture units pursuant to the certificate that will be similar in all material respects to the unit submitted for testing.
4. Kuma Stove and Iron Works will meet permanent and temporary labeling requirements.
5. Kuma Stove and Iron Works will execute record keeping and reporting according to requirements as set forth in Section 60.537.
6. Kuma Stove and Iron Works estimates annual production of this model line for the first two years: less than 2,500 per year.
7. Kuma Stove and Iron Works has entered into a contract agreement with Myron Consulting for Audit testing under the R.C.A. program.

KUMA STOVE AND IRON WORKS

MODEL: Scott HT Stove

INSTALLATION & OPERATING INSTRUCTIONS

— SAVE THESE INSTRUCTIONS —

THIS MANUAL DESCRIBES THE INSTALLATION AND OPERATION OF THE KUMA MODEL SCOTT HT WOOD HEATER. UNDER SPECIFIC TEST CONDITIONS, THIS HEATER HAS BEEN SHOWN TO MEET U.S. ENVIRONMENTAL PROTECTION AGENCIES EMISSION LIMITS FOR RESIDENTIAL WOOD HEATERS.

PLEASE READ THE FOLLOWING SAFETY PRECAUTIONS
AND THE ENTIRE INSTALLATION & OPERATING INSTRUCTIONS:

*****SAFETY PRECAUTIONS*****

1. If this stove is not properly installed, a house fire can occur. For your protection, follow the installation instructions provided. We recommend contacting local building or fire officials regarding restrictions and installation inspection requirements in your area.
2. **DO NOT CONNECT THIS UNIT TO A CHIMNEY FLUE SERVING ANOTHER APPLIANCE.**
3. Do not use gasoline, gasoline-type lantern fuel, kerosene, charcoal lighter fluid, or similar liquids to start or "freshen up" a fire in this heater. Keep all such liquids well away from the heater while it is in use.
4. Do not burn garbage.
5. Do not overfire. The stove is in an overfire condition if any part of the stove glows. If this should happen, immediately close air damper.
6. **WARNING: DO NOT INSTALL IN SLEEPING ROOM.**
7. Caution: The structural integrity of a mobile home floor, wall, & ceiling/roof must be maintained.
8. Do not use single wall pipe for exterior chimney or mobile home applications.
9. When installing into an existing metal or masonry chimney, examine chimney system carefully. If you have any question, seek professional advice. **DO NOT CONNECT THIS UNIT TO A CHIMNEY FLUE SERVING ANOTHER APPLIANCE.**
10. Note all minimum clearances to combustibles. Installation must comply with minimum clearances as listed in this manual.
11. **INSTALL AND USE IN ACCORDANCE WITH THE MANUFACTURERS INSTALLATION AND OPERATING INSTRUCTIONS ONLY.**
12. Safety Notice: If this heater is not properly installed, a house fire may result. For your safety, follow the installation directions.
13. Do not operate stove with firing door in an open position.

CODES & APPROVALS—The Kuma model Scott HT Stove is tested to UL, ULC, ICBO, HUD, and CSA standards, and listed with the Warnock Hersey International Test Lab (WHI).

MOBILE HOME INSTALLATION INSTRUCTIONS

Model: Kuma Scott HT

CAUTION: THE STRUCTURAL INTEGRITY OF A MOBILE HOME FLOOR, WALL, & CEILING/ROOF MUST BE MAINTAINED.

CAUTION: DO NOT INSTALL IN A SLEEPING ROOM.

BEFORE YOU START insure that there are no major obstructions. (i.e. floor joists, ceiling joists, electrical wires, heat ducts, plumbing, etc.)

Clearance—backwall 2 inches, corners 3 1/2 inches, sidewall 23 inches (using Class A Listed chimney and double wall connector). See figures 5 and 6. Consult your local building official and build your hearth pad to local building requirements.

Typical hearth pad (see Example: typical hearth pad on Page 3) -- 18" to front of unit, 6" to sides.

Material required for installation—6-inch outside air duct with screen, roof mate to seal roof flashing, assorted nails and screws, 8-gauge ground wire, 3/8 lag bolts to fasten stove to the floor (length will depend upon hearth thickness).

Tools required—saber saw, screw drivers, measuring tape, pencil, plumb line, electric drill and assorted bits, tin shears, knife, pliers, hammer.

1. After locating possible obstructions (joist, pipes, etc.) and taking into account the necessary combustible clearances (fig. 2), position the stove in the intended installation position. Use a plumb line to locate the position of the ceiling hole for the chimney. Size the chimney hole to the recommended manufacturers clearances for your chimney, mark the hole.
2. Mark a pencil outline around the base of the stove. Move the stove out of the way.
3. Mark with a pencil the holes to be drilled to fasten the stove to the floor, then mark with a pencil a 6-inch hole for the fresh air intake. This hole may be positioned anywhere under the stove.
4. If ceiling and floor are clear of all obstructions, cut out the holes.
5. In case of attic space use a plumb line to locate the hole in the roof. Cut out the opening, keeping in mind the chimney manufacturers recommended clearances.
6. Install the outside air duct to the floor using screws or nails. Ensure that your air duct has a screen or mesh to keep out predators. Air duct must be 6 inches.
7. Install a hearth pad 18" in front of unit -6" back, 6" to sides according to local building codes or manufacturers specs (see applicable figure —corner of straight wall).
8. Position the stove on the hearth and lag bolt the stove to the floor. Ensure that your lag bolts fasten securely to the floor of the mobile home.
9. Ground your stove to the mobile home frame with a min. 8-gauge wire. See figure 2 wiring diagram.
10. Install the first section of listed chimney pipe to the stove by carefully pushing it down on the flue collar, making sure it seats. Place the trim collar black side down over the first section of chimney pipe at this time. Ref. fig. 2 for parts list.
11. Check all chimney pipe for damage. Do not use any damaged pipe. Installation procedures may vary from manufacturer to manufacturer of listed chimney. Install the rest of the chimney up through the hole in the ceiling and roof.
12. After the chimney is perpendicular, fasten the trim collar to the ceiling.
13. In cases where there is an attic space, install a protective joist shield tube or box. Consult local building officials or chimney manufacturer.
14. Install the roof flashing, sealing water tight. Install the storm collar and seal water tight. Install chimney cap. Note: refer to chimney manufacturers specs. Chimney height see fig. 7. Minimum for mobile home 9 1/2' above stove.
15. Call for final inspection.
16. **INSTALL & USE IN ACCORDANCE WITH THE MANUFACTURES INSTALLATION AND OPERATING INSTRUCTIONS ONLY.**
17. **YOUR STOVE IS NOW READY FOR USE. REFER TO OPERATING INSTRUCTIONS.**

RESIDENTIAL INSTALLATION INSTRUCTIONS

Model: Scott HT

CAUTION —Always read instructions manual carefully before beginning the installation.

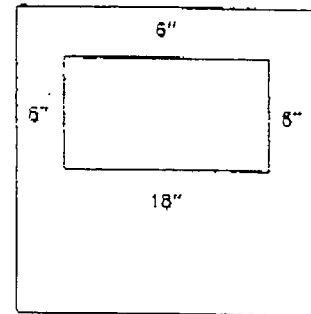
Check all listed factory built chimneys for concealed damage.

Exercise caution to insure that all necessary parts are installed correctly.

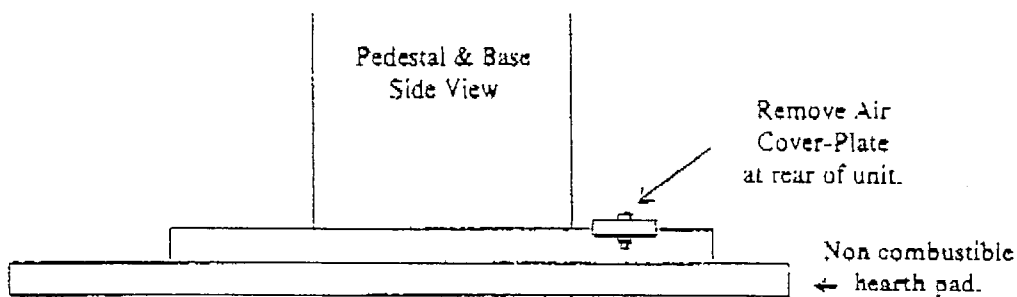
BEFORE YOU START insure that there are no major obstructions. (i.e. floor joists, ceiling joists, electrical wires, heat ducts, plumbing, etc.)

Clearance — backwall 2 inches, corners 3 1/2 inches, sidewall 21 inches. See figures 3 through 6. Consult your local building official and build your hearth pad to local building requirements.

Example: Typical hearth pad.



NOTE: For residential installation, in which outside air intake is not desired, remove cover-plate at rear of pedestal base by removing cover-plate before installing stove as shown below. In this application, hole through floor is not required.



INSTALLATION

1. After locating possible obstructions (joists, pipes, etc.) and taking into account the necessary combustible clearances (fig. 2), position the stove in the intended installation position. Use a plumb line to locate the position of the ceiling hole for the chimney. Size the chimney hole to the recommended manufacturers clearances for your chimney, mark the hole.
2. Mark a pencil outline around the base of the stove. Move the stove out of the way.
3. Mark with a pencil the holes to be drilled to fasten the stove to the floor, then mark with a pencil a 6-inch hole for the fresh air intake. This hole may be positioned anywhere under the stove, if fresh air is desired.
4. If ceiling and floor are clear of all obstructions, cut out the holes.
5. In case of attic space use a plumb line to locate the hole in the roof. Cut out the opening, keeping in mind the chimney manufacturers recommended clearances.
6. Install the outside air duct to the floor using screws or nails. Ensure that your air duct has a screen or mesh to keep out predators. Air duct must be 6 inches.
7. Install a hearth pad according to local building codes or manufacturers specs (see applicable figure).
8. Position the stove on the hearth and lag bolt the stove to the floor if desired.
9. Install the first section of listed chimney pipe to the stove by carefully pushing it down on the flue collar, making sure it seats. Place the trim collar black side down over the first section of chimney pipe at this time.
10. Check all chimney pipe for damage. Do not use any damaged pipe. Installation procedures may vary from manufacturer to manufacturer of listed chimney. Install the rest of the chimney up through the hole in the ceiling and roof.
11. After the chimney is perpendicular, fasten the trim collar to the ceiling.
12. In cases where there is an attic space, install a protective joist shield tube or box. Consult local building officials or chimney manufacturer.
13. Install the roof flashing, sealing water tight. Install the storm collar and seal water tight. Install chimney cap. Note: refer to chimney manufacturers specs. Chimney height see fig. 7.
14. Call for final inspection.
15. Read completely the Operating and Burning instructions.
16. Your stove is ready to burn.

WOOD BURNING OPERATING INSTRUCTIONS

Model: Scott HT

RECOMMENDATIONS ON BUILDING AND MAINTAINING A FIRE:

1. Open air control by rotating draft handle forward.
2. Start with tinder and small kindling. When starting a fire, stack wood in a "criss-cross" arrangement so as to allow the fuel plenty of air. Place smaller chunks of wood, on up to larger ones until desired fire size and heat level is achieved. Once the desired heat level in house is reached, rotating the air control handle back decreases the air to the firebox, and thus reduces heat produced. Use the following table as a general guideline for desired burn rates:

low burn	draft handle rotated back completely
med-low	draft handle full back to 1/4" forward
medium	draft handle 1/4" to 1/2" forward
med-high	draft handle 1/2" to 3/4" forward
high burn	draft handle rotated full forward

CAUTION: When building the first couple of fires be careful to build the fire small and increase heat slowly over 4-5 hour period. The paint on the stove "cures" with heat and needs to be done slowly. As the paint "cures" it gives off a smell of paint and even sometimes a visible "smoky" haze into the room. Make sure the area is well ventilated during the curing operation. The smell will disappear after a few hours of operation.

OPTIONAL BLOWER OPERATING INSTRUCTIONS: Install blower unit in back of stove as per instructions, and plug into nearest 115V grounded circuit. Turn the variable speed knob to 'click' onto high speed. As the knob is turned clock-wise, the blower speed decreases to your desired speed. The blower speed should match the desired burn rate on your stove: i.e., low burn rate-low blower speed; high blower rate-high blower speed and so forth.

DO NOT OPERATE THIS STOVE WITH THE DOOR OPEN. It may be necessary however to crack door during the first 5 or 10 minutes during the start-up stage. Contact your dealer if you have any questions or problems building or maintaining a fire.

CAUTION: DO NOT USE CHEMICALS OR FLUIDS TO START OR FRESHEN UP A FIRE. DO NOT BURN GARBAGE OF FLAMMABLE FLUIDS SUCH AS GASOLINE, NAPHTHA, OR ENGINE OIL.

1. The unit is designed to burn wood only. Build the fire directly on the hearth. Do not use grates. Your stove will burn better with about one inch of ash in the bottom, but never let the ash build up to the level of the combustion air inlet. Your stove is a very efficient "airtight" heater and if you use high quality wood, there will be very little ash residue.
2. Use only the best grade of dry wood available. It takes a full year to properly dry your split wood, so plan ahead. Burning wet or green wood greatly increases the chance of creosote build-up and produces less heat much less efficiently. Store your fuel in a dry location and be sure to maintain clearances from wood supply to your stove.
3. Small hot fires produce less creosote than long low smoldering fires. When you start your stove, open the draft fully and once or twice each day repeat this high burn cycle to reduce any creosote build-up. Just after starting the fire some smoke may occur until the chimney warms up to produce some draft. During normal operation adjust the draft to the position required. If properly set, it will assure longest burn times and the most even heat cycle.
4. Make routine inspections of your flue systems at least once every two months to ensure clean, safe operation.
5. Ensure an adequate supply of outside combustion air is available. Failure to provide adequate combustion air is dangerous. Fifteen (15) square inches is recommended.

WOOD BURNING OPERATING INSTRUCTIONS

continued

CREOSOTE FORMATION AND NEED FOR REMOVAL

6. When wood is burned slowly, it produces tar and other organic vapors which combine with expelled moisture to form creosote. The creosote vapors condense in the relatively cool chimney flue of a slow burning fire. As a result, creosote residue accumulates on the flue lining. When ignited, this creosote makes an extremely hot fire. If creosote has accumulated, it should be removed to reduce the risk of a chimney fire.

DISPOSAL OF ASHES

7. Ashes should be placed in a metal container with a tight-fitting lid. The closed container of ashes should be placed on a non-combustible floor or on the ground, well away from all combustible materials, pending final disposal. If the ashes are disposed of by burial in soil or otherwise locally dispersed, they should be retained in the closed container until all cinders have thoroughly cooled.
8. Maintain door seals, etc., to ensure airtight fit. Operate only with the fire door closed. Open door only to fuel fire.
9. Resist the temptation to refuel too soon. Let the fire burn down to just glowing coals before you open the door. This will be the most efficient operation and there will be less smoking. Do not overfire.
10. Contact your local or provincial fire authority for information on how to handle a chimney fire.
11. For further information on using your heater safely, obtain a copy of the National Fire Protection Association publication: "Using Coal and Wood Stoves Safely." NFPA No. HS-8-1974. The address of NFPA is: 470 Atlantic Ave., Boston, Ma. 02210.

GLASS DOOR

1. Never clean hot glass.
2. Clean with an approved cleaner. Never use an abrasive.
3. Excessive mechanical stress will crack or break the glass. Should breakage occur see your dealer or carefully remove retainer clip screws to release glass. Dispose of broken glass in a safe place. Replace glass only with 5mm neoceram available from your dealer. Always replace the gasket with a glass replacement. Check glass after heater has been fired to ensure a tight seal. Tighten clip just enough to provide the air tight seal. Uneven pressure from over tightened screws will break the ceramic (glass). See Figure 1.
4. Never build the fire up against the glass and ensure the glass wash secondary air draft slot is open.
5. When closing door, do not allow logs to protrude against glass.

A WORD ABOUT DRAFT

The principle of draft is that warm air rises. Your chimney provides draft which sucks the smoke up the chimney. The stove does not "push" out the smoke. Your Scott HT Stove has been designed and approved for use under normal conditions. Unacceptable smoking usually indicates poor draft in your chimney system. CHECK THAT YOU HAVE PROVIDED FOR ADEQUATE OUTSIDE AIR FOR COMBUSTION.

PROBABLE CAUSE FOR SMOKING ARE:

1. Insufficient chimney height above nearby obstructions.
2. Clogged or obstructed chimney system.
3. Downdrafts caused by nearby trees, hills, building, etc.

Figure 1

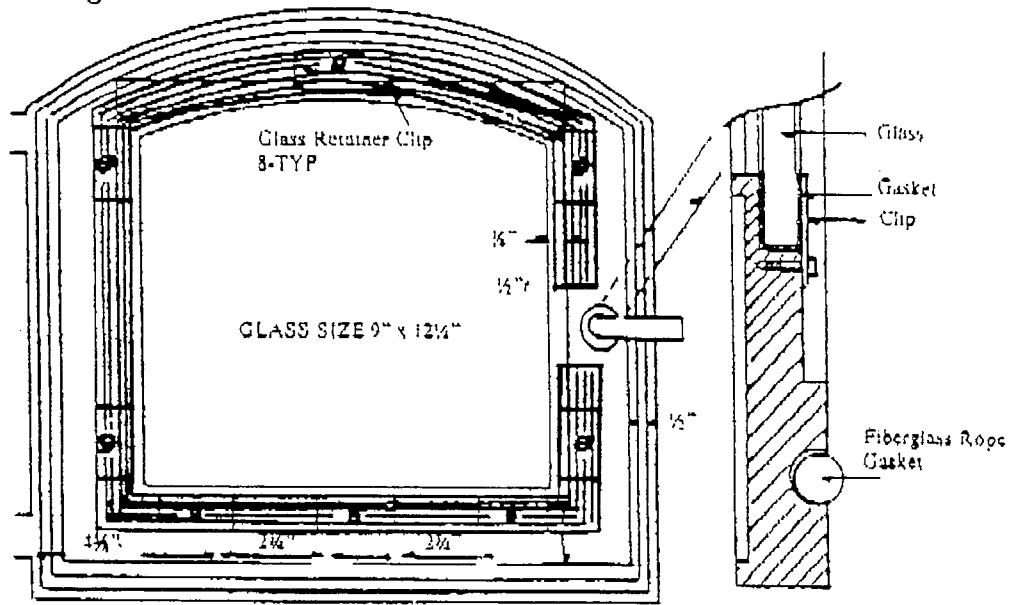
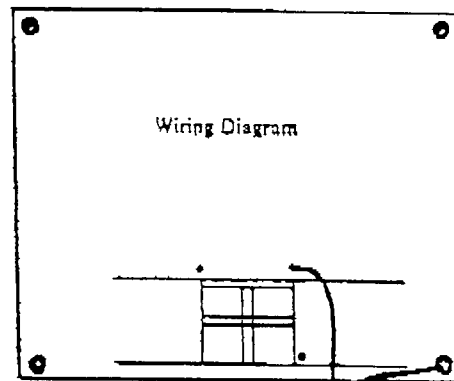
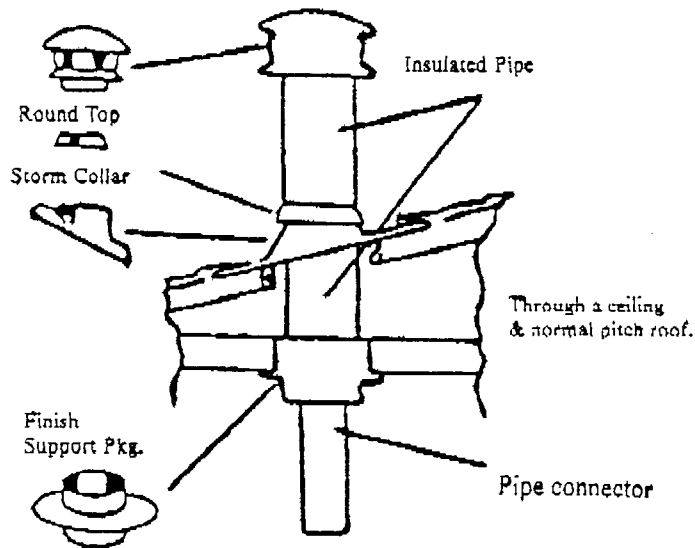


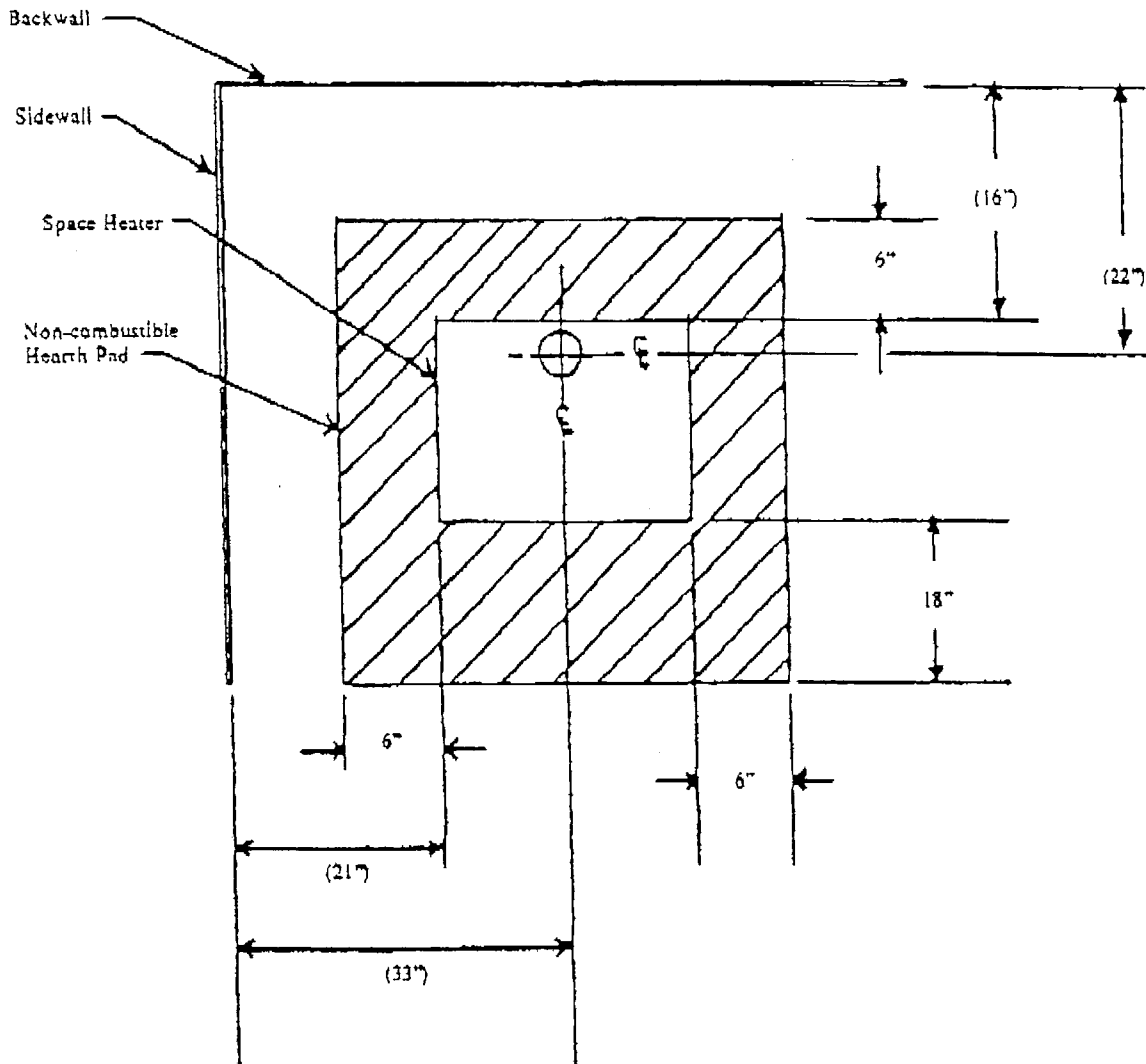
Figure 2



Ground wire to Mobile Home Frame. #8GA Wire & Approved Terminal.

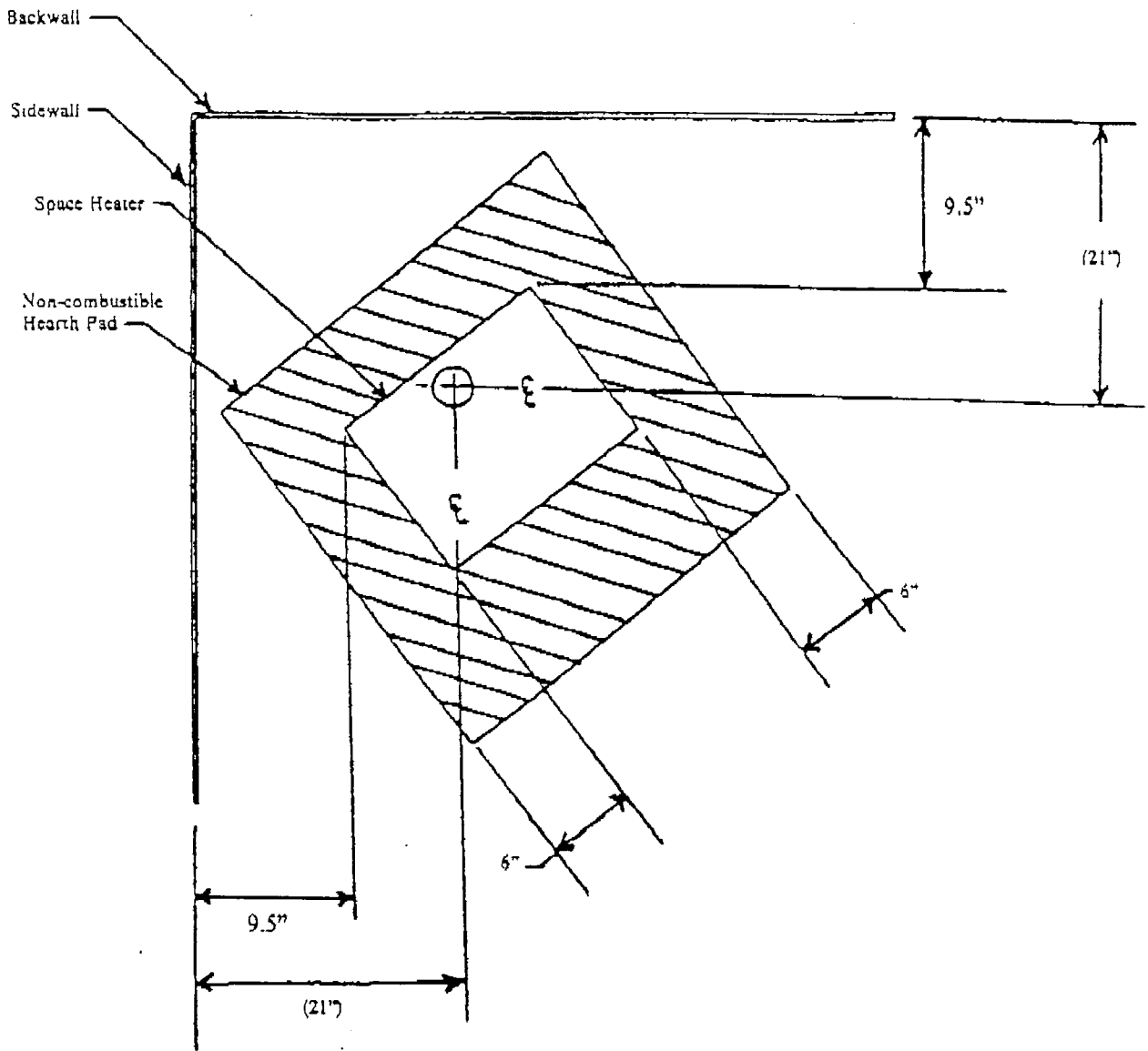
Use only 6" diameter listed chimney system parts that have been tested and found to be compliant with all applicable U.L. standards. Clearances to combustibles must be maintained as per manufacturers instructions on chimney pipe, and stove pipe connectors. Use only double-wall connector in mobile home applications.

Figure 3



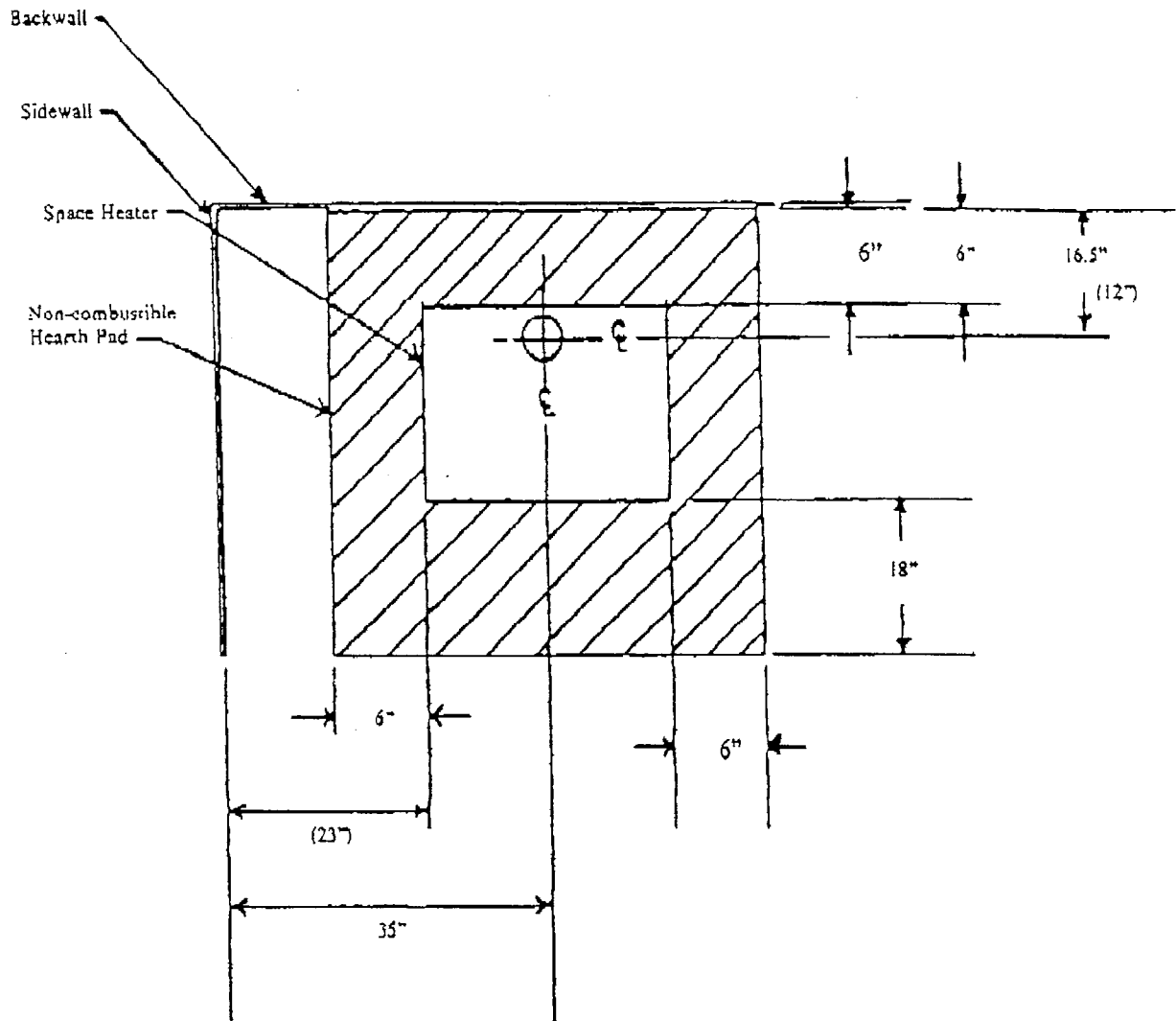
**MINIMUM CLEARANCES TO COMBUSTIBLES — STRAIGHT WALL
CLASS C SINGLE WALL CHIMNEY CONNECTOR**

Figure 4



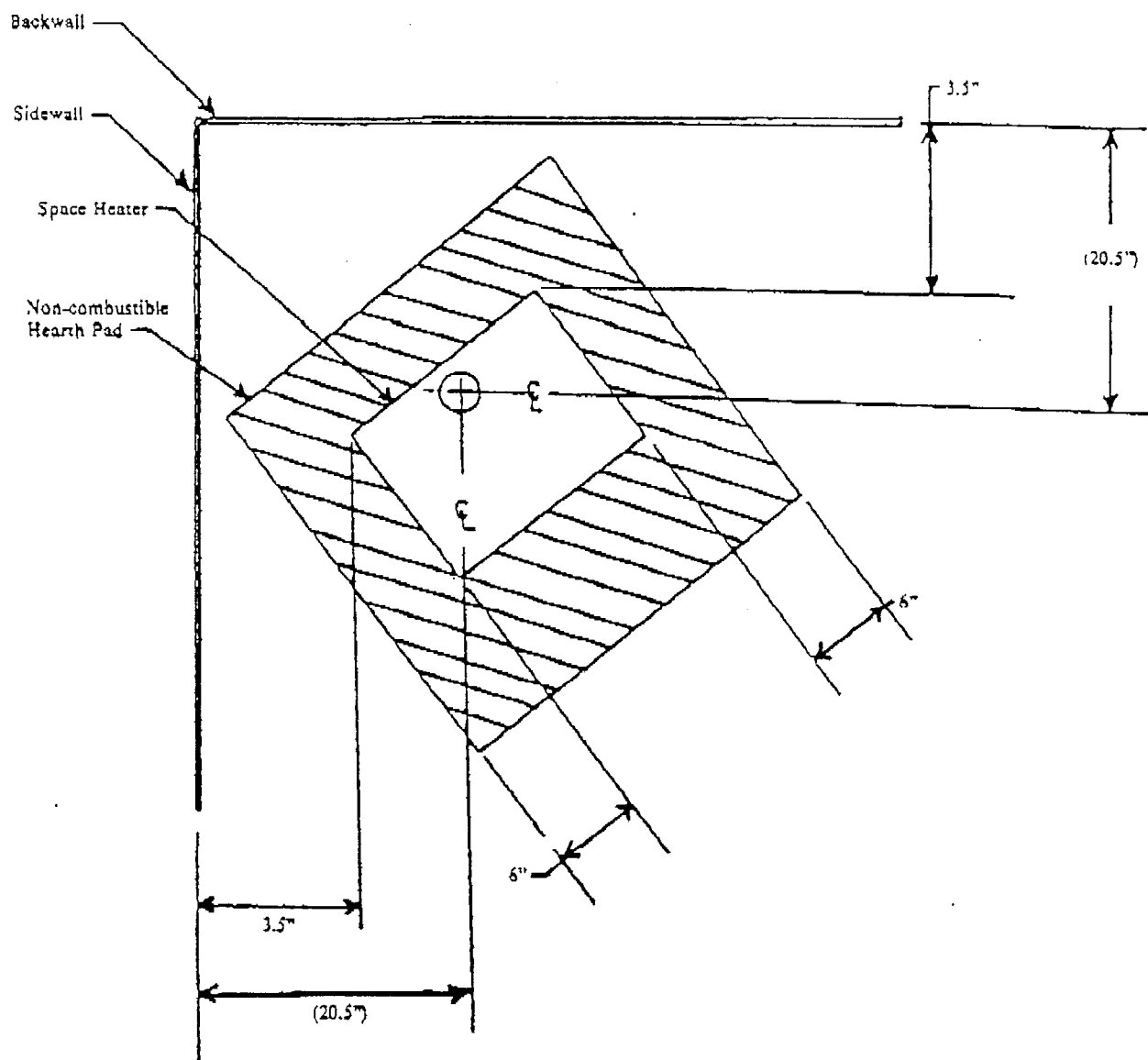
MINIMUM CLEARANCES TO COMBUSTIBLES — CORNER
CLASS C SINGLE WALL CHIMNEY CONNECTOR

Figure 5



**MINIMUM CLEARANCES TO COMBUSTIBLE — STRAIGHT WALL
CLASS A LISTED CHIMNEYS USING APPROVED DOUBLE-WALL CONNECTOR**

Figure 6

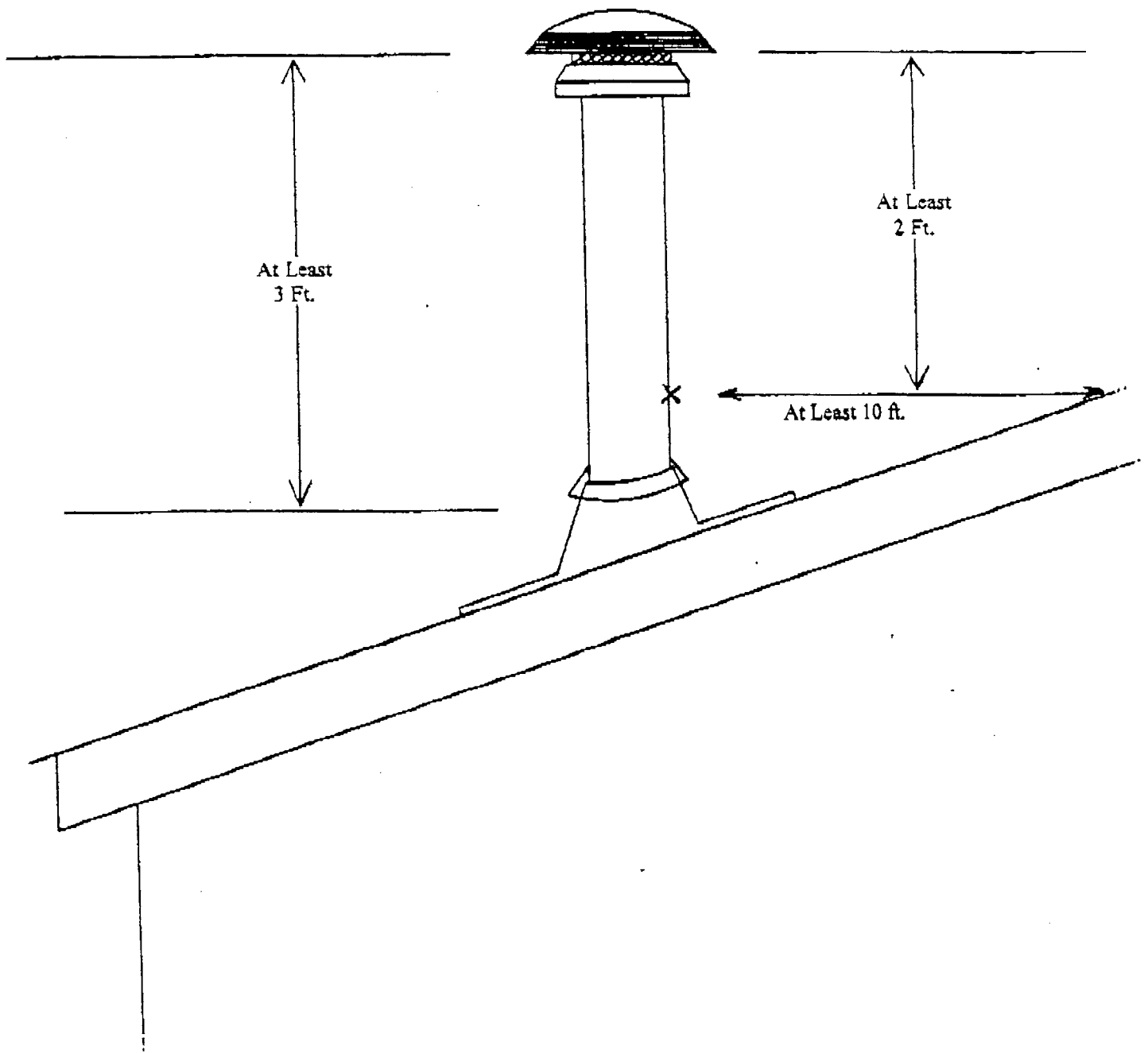


MINIMUM CLEARANCES TO COMBUSTIBLES . CORNER
CLASS A LISTED CHIMNEYS USING APPROVED DOUBLE-WALL CONNECTOR

HEIGHT REQUIREMENTS

A chimney must be the required height above the roof or other obstruction for safety and for proper draft operation. The requirement is that the chimney must be at least 3 feet higher than the highest point where it passes through the roof and at least 2 feet higher than the highest part of the roof or structure that is within 10 feet of the chimney, measured horizontally (FIGURE 7).

Figure 7



WOODSTOVE DATA SHEET #30
STOVE STORAGE

The Kuma Scott HT-1 Noncatalytic Woodstove

tested by Myren Consulting is being held in custody by Kuma Stove
and Iron Works and is being stored

at:

Kuma Stove and Iron Works Contact Person

450 Old Highway 95

Mark Freeman

Rathdrum, Id 83858

Phone

(208) 762-8002

A. Temporary storage at Myren Consulting until certification is granted.

A single strap of steel banding is placed around the stove so that the banding crosses the door horizontally, making it impossible to open the door on the unit. If it is necessary to break the banding to check some internal dimension or component, the banding is immediately replaced after the work on the unit has been completed.

The unit is identified by having the unit's certification tracking name written on a tag, label or piece of tape which is attached to the unit.

B. Permanent storage after certification has been granted.

The following measures have been taken to seal the unit against tampering: several lengths of steel banding have been placed around the stove in a manner which prevents the door from being opened. At least two (2) of these lengths cross at 90° angles. At each 90° crossing point on the top of the stove, a Myren Consulting address label has been placed over the crossing point and the label is then taped to the stove with 2" clear packing tape. The stove is then loaded onto a pallet and strapped to the pallet with several lengths of metal banding. A shipping carton (box) is then placed over the stove and attached to the pallet with staples and/or nails. The name of the unit is written on a Myren Consulting address label which is affixed to the outside of the box.

C. The stored unit is identified as follows:

The Myren Consulting address label(s) on top of the stove has (have) the name of the stove written on them. The box has warning labels affixed to the sides and top of the box which clearly identify the stove as a test stove being stored pursuant to 40 CFR Part 60. These labels have the name of the stove clearly written on them. (A sample warning label follows on the next page.)

D. The unit was returned to the manufacturer via manufacturer's
and lab's pickup trucks

W A R N I N G

SEALED EPA TEST STOVE

DO NOT OPEN OR TAMPER WITH THE SEALS AND PACKAGING ON THIS STOVE.

TO DO SO WILL VOID THE CERTIFICATION ON THIS STOVE.

W A R N I N G

SEALED EPA TEST STOVE

DO NOT OPEN OR TAMPER WITH THE SEALS AND PACKAGING ON THIS STOVE.

TO DO SO WILL VOID THE CERTIFICATION ON THIS STOVE.

